

UNITED STATES DEPARTMENT OF THE INTERIOR GEOLOGICAL SURVEY

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JUN 2 1 1982 OIL SHALE

RESULTS OF CORE DRILLING IN 1978 FOR OIL SHALE IN

THE EOCENE GREEN RIVER FORMATION, PICEANCE CREEK

AREA OF WESTERN COLORADO

Ву

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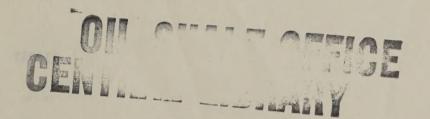
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RESULTS OF CORE DRILLING IN 1978 FOR OIL SHALE IN THE EOCENE GREEN RIVER FORMATION, PICEANCE CREEK AREA OF WESTERN COLORADO

Ву

M. C. Smith and R. B. O'Sullivan

INTRODUCTION

In 1978, the U.S. Geological Survey drilled 15 core holes in the Piceance Creek area of western Colorado. This preliminary report presents the basic data gathered during the drilling program. The general location of all the core holes is shown on figure 1; a more precise location is shown on figures 2-14. A summary of core holes data is given in table 1. The wells were drilled with a truck-mounted rig, and the recovered cores were examined at the drill site. A lithologic description of each of the core holes accompanies this report. The purpose of the drilling was to obtain information to aid in the evaluation of the oil-shale resources of the Piceance Creek area. Cores from the drill holes were assayed for oil yield by the Natural Resource Laboratory, Inc. of Lakewood, Colorado, and Laramie Energy Technology Center, Laramie, Wyoming. Histograms showing oil yield and tables giving the analytical results for each core hole accompany this report.

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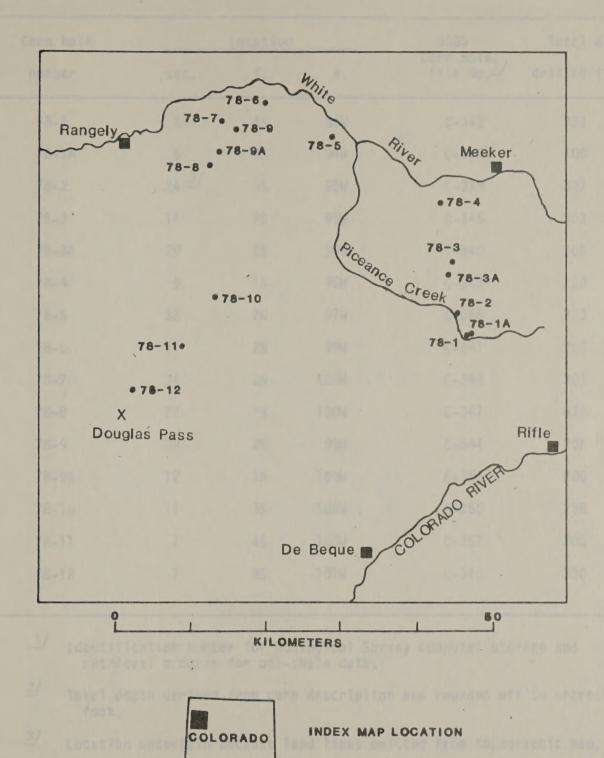
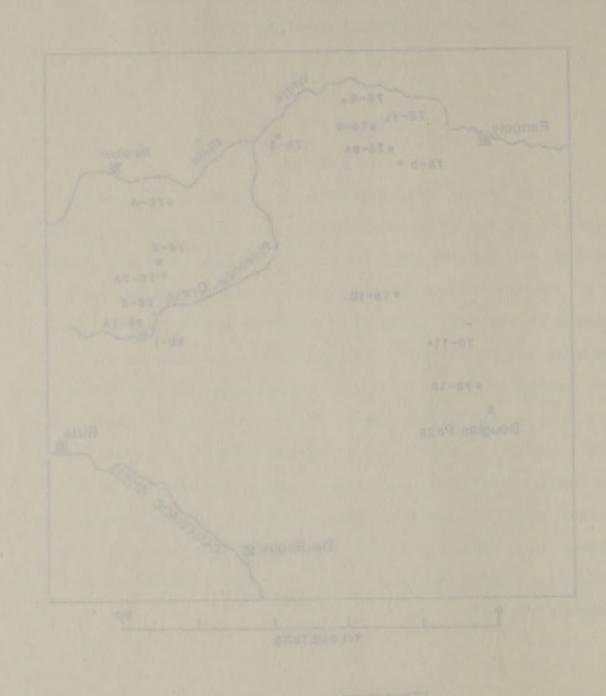


Figure 1.--Index map showing location of core holes drilled in 1978.



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Table 1.--Core holes drilled in 1978 in Piceance Creek basin area.

Core hole		Location		USGS	Total depth	
number	sec.	т.	R.	Core hole /	drilled (feet) ^{2/}	
78-1	6	48	94W	C-342	232	
78-1A	6	45	94W	C-338	100	
78-2	24 3/	3S	95W	C-339	307	
78-3	14	2S	95W	C-345	303	
78-3A	26	25	95W	C-340	. 300	
78-4	9	15	95W	C-343	220	
78-5	32	2N	97W	C-358	323	
78-6	11	2N	99W	C-341	205	
78-7	24	2N	100W	C-346	304	
78-8	22	1N	100W	C-347	630	
78-9	29	2N	99W	C-344	205	
78-9A	12	1N	100W	C-356	200	
78-10	11	3S	100W	C-355	298	
78-11	7	45	100W	C-357	202	
78-12	7	5S	101W	C-348	330	

Identification number for Geological Survey computer storage and retrieval program for oil-shale data.

 $[\]frac{2}{}$ Total depth derived from core description and rounded off to nearest foot.

^{3/} Location uncertain because land lines omitted from topographic map.

Table 1,-- Core tolles spilling to 1976 to Sicource Creek cools longs

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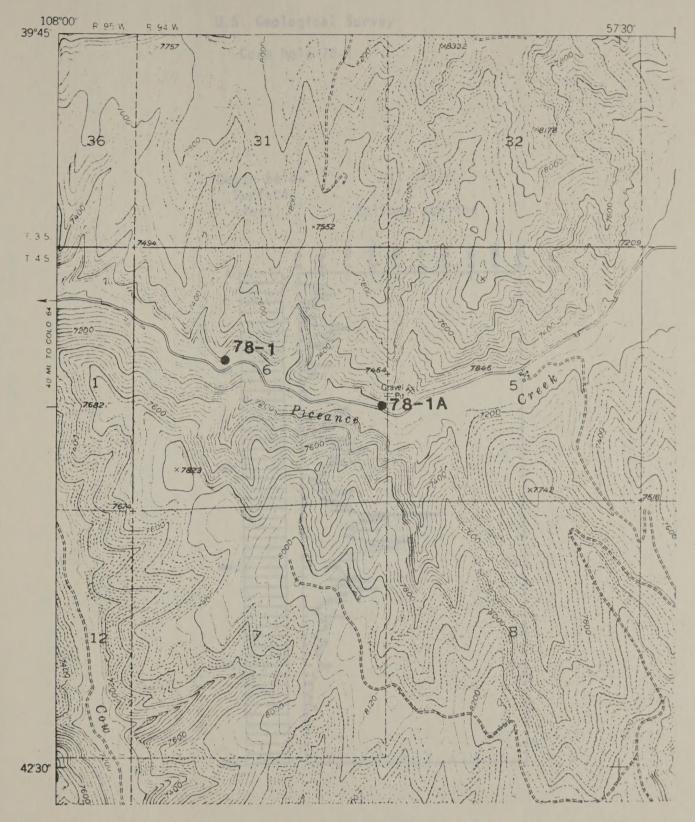


Figure 2.--Map showing location of core holes 78-1 and 78-1A. Base from Rio Blanco Quadrangle (1952). Scale 1:24,000.

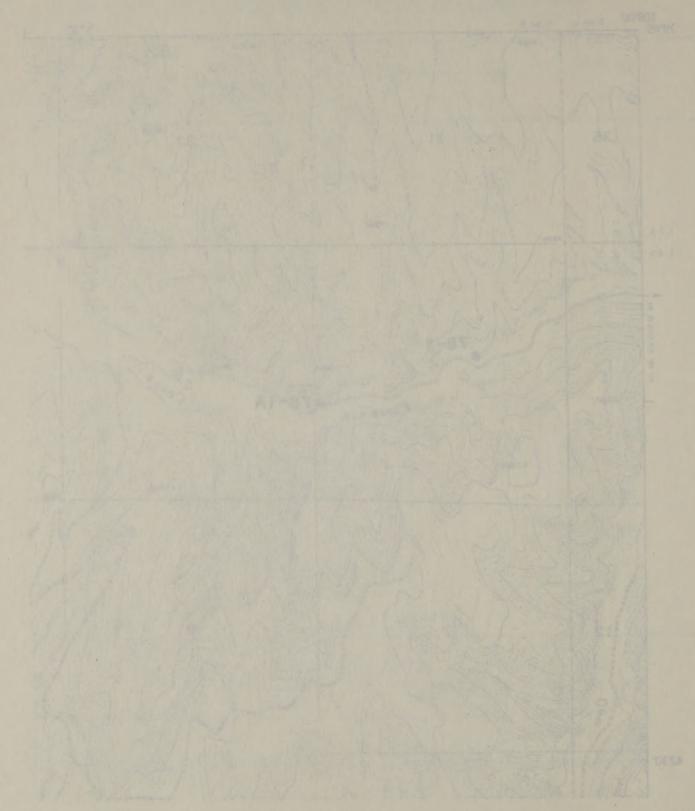
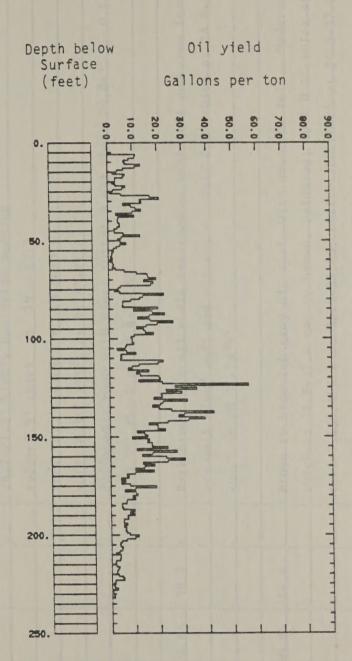


Figure 2.--Map showing Totalion of core hales 28-1 and 70-1A. Sees from fits Blanco Quadrangle (1992). Seets 1:24.600.

U.S. Geological Survey

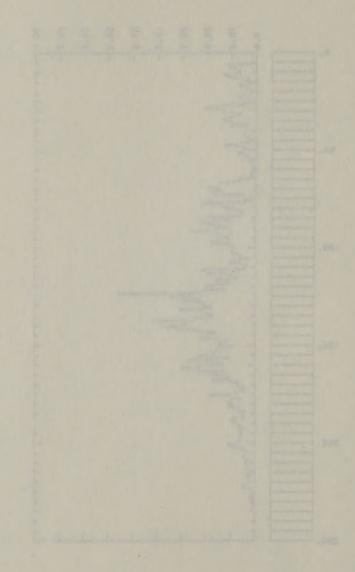
Core hole 78-1



U.S. Geological Survey Core hole 28-1

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Corehole 78-1 Logged by Kurt Hollocher

FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION
6.0	26.65		Brown to brownish gray oil shale with winer tuff. Little turbation with thin
			_bedding. Moderately rich.
			tuff~0.15' thick at 14.85-15.0
			tuff 0.15' thick at 15.6-15.75
			18.7-21.5' highly contorted hedding
			tuff = 0.2' thick at 19.0-19.3
		1	tuff 0.3' thick at 20.2-20.5
			tuff 0.35' thick at 21.05-21.4
			Tuffaceous zone with minor turbated oil shale 24.8-25.2, 0.4' thick tuff
			0.25' thick at 26.4-26.65
26.65	30-2		Dark brown rich oil shale interbedded with tuff and some leaner oil shale. Parts are well mixed tuff and oil shale. Tuff 0.2' thick at 28.6-28.8'; tuff 0.4'
			thick at 28.9'-29.3'
30.2	46.4		Brown to brownish gray oil shale with abundant tuff. Moderately rich. Tuff 0.5' thick at 31.9-32.4 tan to brown, oxidized; tuff 0.1' thick at 32.8-32.9';
		,	zone 38.5-40.9' 2.4' thick, homogenized.
1			

9

Corchele 18-1

FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION
46.4	113.1		Dark brown to brown rich oil shale with abundant intermixed tuff. Green and blu material in some fractures and in beds, some folding, but generally even bedding
			tuff 0.4'thick at 49.05-49.45
			tuff 0.1' thick at 58.0'
			tuff 0.1' thick at 64.0
			tuff 0.15' thick at 65.3-65.45
			tuff 0.2' thick at 73.2-73.4
			tuff 0.25' thick at 73.7 - 73.95
			tuff at 0.25' thick at 74.05-74.3
			tuff 0.1' thick at 74.5'
			Sequence of thick tuffs with thin even layers of oil shale between them from
			74.8-77.2. 2.4' thick white tuff 0.15' thick at 77.2-77.35
			Very dark brown to black oil shale with some tuffs.
			77.35-78.1
			Sequence of thick and thin tuffs of different textures with thin interhedded
			dark rich oil shale, 80.9'-86.5', 5.6' thick tuff 0.1' thick at 89.3'
			Tuff 0.2' thick at 92.0-92.2
			Tuff 0.1' thick at 92.8
,			Tuff 0.25' thick at 95.0-95.25 Tuff 0.15' thick at 95.85 - 96.0
			Tuff 0.2' thick at 99.2-99.4 contorted

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FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION
			Tuff 0.3' thick at 99.9' - 100.2'
			Tuff 0.2' thick at 103.1' - 103.3'
			Tuff 0.4' thick at 103.4' - 103.8'
			Tuff 0.4' thick at 104.4' - 104.8'
			Tuffaceous section ~70 percent massive thick to thin tuffs
A			with interhedded moderately rich to rich oil shale
			105.2'-111.0', 5.8' thick total
113.1	122.6	9.5'	Highly tuffaceous section with 70 percent tuff interhedded with brown to very dark brown rich oil shale. Some turbation. Individual tuffs not described
122.6	143.0		Dark brown rich oil shale interhedded with tuff. Little turbation.
		-	tuff 0.1' thick at 124.6'
			Shallow dipping bedding plane slickensides at 124.9', 125.05, 125.2'
			Tuff 0.1' thick at 126.7'
			Tuff 0.15' thick at 130.1'-130.3'
			Tuff 0.12' thick at 130.6'
			Tuff 0.1' thick at 130.6'
			Tuff 0.1' thick at 130.7'
			Tuff 0.1' thick at 132.3'
			Tuff 0.1' thick at 133.8'

 ∞

FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION
			Slickensides in bedding plane at 136.9', 137.05', 138.2', 138.3', 139.6', 139.8'
1			139.95', 140.2' 140.7' 141.4', 142.4',
			Tuff 0.1' thick at 138.1
			Tuff 0.5' thick at 140.2'-140.7'
			Tuff 0.1' thick at 141.0'
			Tuff 0.1' thick at 142.0'
			Tuff 0.1' thick at 146.0'
143.0	204.2		Brown to gray brown moderately rich oil shale with several units of rich dark
			brown oil shale, much tuff or silt intermixed with shale, bedding is thin and
			even with little turbation 470 percent tuff with mixed and discrete oil shale
			layers from 147.5-147.9', 0.4' thick.
			Bedded massive tuff with very thin shale layers from 149.9' - 150.3', 0.4' thick
			Tuff_0.1' thick at 152.3'
			Tuff 0.75' thick at 156.05-156.8 with minor shale
			Tuff 0.1' thick at 158.1'
			Tuff 0.8' thick at 158.7-159.5
-			Tuff 0.7' thick at 162.6-163.3 with minor shale
			Tuff 0.1' thick at 166.1'
			Tuff 0.2' thick at 168.3' - 168.5' with minor shale
			Tuff 0.5' thick at 171.6-172.1
			Tuff 0.1' thick at 172.5'

•		-1,0					1	4	-	-57/7	1	-	-	-	-	+ 1	16.1
V																	

FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION
			Tuff 0.1' thick at 172.8'
1			Tuff 0.1' thick at 174.0'
			Tuff 0.1' thick at 175.5'
			Tuff 0.1' thick at 175.8'
			Tuff 0.35' thick at 177.35-177.7
			Tuff 0.45' thick at 178.75' -179.2'
			Tuff 0.4' thick at 181.6-182.0'
			Highly tuffaceous section with shale mixed with tuff
			and/or silt - 183.9'-187.4', 3.5' thick
			Tuff 0.9' thick at 187.8' 188.7'
			Tuff 0.1' thick at 189.7'
			Tuff 0.15' thick at 194.95-195.1
			Tuff 0.3' thick at 195.3-195.6
			Tuff 0.15' thick at 197.0-197.15
			THE PROPERTY OF THE PROPERTY O
04.2	232.0		Zone of gray siltstone with minor oil shale and probably abundant tuff. The
OTTOM	OF HOLE		rock retains water in this unit. Thin pyrite rich layers common.
			Tuff 0.1' thick at 207.5'
			Tuff 0.2' thick at 217.4-217.6

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OIL-SHALE ASSAYS BY MODIFIED FISCHER RETORT METHOD

Samples from the U.S. Geological Survey's Corehole 78-1 drilled in sec. 6, T 4 S, R 94 W, Rio Blanco County, Colorado

				Yield o	f prode			
30.0	23.0	-	Weight	percent	· proge	The second secon		Specific
Dept	th	-		Spent	Gas +	Gal pe	er con	gravity
From	To	Oil	Water	shale	loss	0i11/	11	of oil at
6.0	7.0	4.5	1.8	92.5	1.2	11.4	Water	60°/60° F
7.0	8.0	4.3	1.6	93.0	1.1	11.0	4.3	0.939
8.0	9.0	3.4	1.5	93.9	1.2		3.8	.938
9.0	10.0	2.6	1.2	95.6		8.6	. 3.6	.941
10.0	11.0	2.7		95.5	.6	6.6	2.9	.934
11.0	12.0	5.2	1.6		. 6	7.1	2.9	.926
12.0	13.0	4.3	1.5	91.9	1.3	13.4	3.8	.932
13.0	14.0	2.4		92.7	1.5	11.1	3.6	.933
14.0	15.0		1.2	95.7	.7.	6.3	2.9	.926
15.0	16.0	1.5	1.1	97.0	.4	3.8a	2.6	
16.0	17.0	. 8	1.0	97.6	.6	2.1a	2.4	
17.0		2.7	1.1	95.3	.9	7.0	2.6	.931
18.0	18.0	2.4	1.3	95.4	.9	6.2	3.1	.930
19.0	19.0	1.2	1.5	96.7	.6	3.0a	3.6	
	20.0	1.1	1.0	97.2	.7	3.0a	2.4	
20.0	21.0	.7	1.0	97.7	.6	1.8a	2.4	1
21.0	22.0	1.2	1.3	96.7	.8	3.1a	3.1	
22.0	23.0	2.8	1.5	94.6	1.1	7.2	3.6	.927
23.0	24.0	2.3	1.6	94.8	1.3	5.9	3.8	.925
24.0	25.0	. 8	1.0	97.4	. 8	2.1a	2.4	
25.0	26.0	.4	1.9	97.2	.5	1.0a	4.6	
26.0	27.0	2.1	1.2	95.3	1.4	5.4	2.9	.927
27.0	28.0	6.6	1.6	90.4	1.4	17.1	3.8	.930
28.0	29.0	8.0	1.6	38.7	1.7	20.8	3.8	.922
29.0	30.0	5.0	1.7	92.1	1.2 .	12.9	4.1	
30.0	31.0	5.3	1.2	92.0	1.5	13.7	2.9	.928
31.0	32.0	2.3	.9	96.1	.7	6.1	2.2	.925
32.0	33.0	3.6	1.4	93.8	1.2	9.4	3.4	.925
33.0	34.0	4.3	. 9	93.6	1.2	11.2		.925
34.0	35.0	5.2	.7	93.0	1.1	13.5	2.2	.924
35.0	36.0	3.8	1.2	93.4		9.9	1.7	.916
36.0	37.0	1.2	0.7	97.3	0.8	3.1a	2.9	.919
37.0	38.0	4.2	1.4	92.9	1.5		1.7	0.000
38.0	39.0	1.6	1.4	96.4		10.7	3.4	0.928
39.0	40.0	1.4	1.1	97.0	.6	4.1a	3.4	
40.0	41.0	1.5	1.1	96.5		3.8a	2.6	
41.0	42.0	1.8	1.4		.9	4.0a	2.6	
42.0	43.0	1.9	1.3		.5	4.6a	3.4	
43.0	44.0	1.4		95.8	1.0	4.8a	3.1	4
44.0	45.0		1.4	96.5	.7	3.7a	3.4	
45.0	46.0	.9	1.0	97.6	.5	2.4a	2.4	1
0.0	40.0	1.0	1.0	97.5	.5	2.6a	2.4	

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Samples from the U.S. Geological Survey's Corehole 78-1 (Continued)

		-		Yield o	of produ	C.	7 A COST	
			Weight	percent		Gal pe	T TOD	Specific
Det	th			Spent	Gas +		T EUII	gravity
Prom	To	Oil	Water	shale	loss	013-1/	Water	of oil at 60°/60° F
46.0	47.0	2.4	1.1	95.8	.7	6.2	2.6	.927
47.0	48.0	5.0	1.3	92.3	1.4	13.0	3.1	.925
48.0	49.0	2.1	1.0	96.3	.6	5.4	2.4	.927
49.0	50.0	1.5	1.0	96.9	.6	3.9a	2.4	. 721
50.0	51.0	1.9	1.4	96.1	.6	4.9a	3.4	
51.0	52.0	2.8	1.3	95.0	.9	7.3	3.1	.926
52.0	53.0	1.8	1.0	96.4	. 8	4.7a	2.4	. 720
53.0	54.0	1.3	1.1	96.9	.7	3.3a	2.6	
54.0	55.0	.8	1.7	97.1	.4	2.0a	4.1	
55.0	56.0	. 8	2.0	96.7	.5	2.1a	4.8	
56.0	57.0	. 6	1.9	97.0	.5	1.5a	4.6	
57.0	58.0	.6	1.9	97.1	.4	1.4a	4.6	
58.0	59.0	.4	1.7	97.3	.6	1.0a	4.1	
59.0	60.0	.6	2.0	96.7	.7	1.6a	4.8	
60.0	61.0	.4	1.9	97.2	.5	.9a	4.6	
61.0	62.0	.7	1.7	97.2	.4	1.8a	4.1	
62.0	63.0	.8	1.6	97.1	.5	2.1a	3.8	
63.0	64.0	.6	1.1	97.6	.7	1.6a	2.6	
64.0	65.0	1.1	.9	97.7	.3	2.8a	2.2	
65.0	66.0	2.4	1.1	95.7	.8	6.5		003
66.0	67.0	4.3	1.3	93.2	1.2	11.4	2.6	.903
67.0	68.0	5.9	1.4	91.2	1.5	15.7		0.906
68.0	69.0	6.0	1.4	91.2	1.4		3.4	.901
69.0	70.0	7.2	1.6	89.4	1.8	16.0	3.4	.904
70.0	71.0	5.4	1.7	91.5		19.2	. 3.8	.903
71.0	72.0	6.9	1.9		1.4	14.3	4.1	.906
72.0				89.5	1.7	18.1	4.6	.911
	73.0	6.5	1.9	89.6	2.0	17.0	4.6	910
73.0	74.0	1.8	1.6	95.8	.8	4.7a	3.8	
74.0	75.0	1.5	1.7	.95.3	1.5	3. 8a	4.1	
75.0	76.0	. 8	2.2	96.3	.7	2.2a	5.3	
76.0	77.0	1.7	2.4	95.1	. 8	4.5a	5.8	
77.0	78.0	8.5	2.8	86.4	2.3	22.3	6.7	.910
78.0	79.0	5.3	1.3	92.3	1.1	13.7	3.1	.917
79.0	80.0		7 .7	93.1	1.5	12.5	1.7	.908
80.0	81.0	3.3	1,3	94.5		8.8	3.1	.906
81.0	82.0	2.1	1.7	95.4		5.6	4.1	.915
82.0	83.0	2.1	2.4	95.0	.5	5.6	5.8	.931
83.0	84.0	2.1	2.9	94.5		5.4	7.0	.920
84.0	85.0	7.7	1.2	89.7	1.4	19.9	2.9	.920
85.0	86.0	3.8	1.5	93.9	.8	9.9	3.6	.915
86.0	87.0	6.7	1.7	90.4	1.2	17.5	4.1	.912
87.0	88.0	8.6	1.6	87.9	1.9	22.6	3.8	.912
88.0	89.0	6.3	1.8	90.6	1.3	16.3	4.3	.919
89.0	90.0	4.5	1.8	92.3	1.4	11.6	4.3	.924
90.0	91.0	6.4	1.7	90.8	1.1		4.1	.922
91.0	92.0	. 9.9	1.7	86.1	2.3	26.0	4.1	.915
92.0	93.0	7.4	1.7	89.4	1.5	19.5	4.1	.913.
93.0	94.0	5.7	1.6	91.5	1.2	15.0	3.8	.917
94.0	95.0	4.3	1.6	93.1	1.0	11.1	3.8	.919
95.0	96.0	5.3	1.8	91.5	1.4	14.0	4.3	.917

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Semples from the Mr. S. Santagent Survey's favorate

OLL-SHALE ASSAYS BY MODIFIED FISCHER RETORT METHOD

Samples from the U.S. Geological Survey's Corehole 78-1 (Continued)

		-		Yield o	of produ	100		
			Weight	percent	or produ	Gal pe	7 700	Specific
De				Spent	Gas +		- LOII	gravity
From	To	011	Water	shale	loss	011-/	Water	of oil at 60°/60° F
04.0								
96.0	97.0	5.6	1.8	91.4	1.2	14.7	4.3	0.914
97.0	98.0	6.9	1.7	89.8	1.6	18.0	4.1	.916
98.0	99.0	3.8	1.0	94.1	1.1	10.1	2.4	.916
99.0	100.0	3.4	2.5	93.1	1.0	8.8	6.0	.925
100.0	101.0	3.5	1.2	94.5	. 8	9.3	2.9	.915
101.0	102.0	3.5	.7	94.9	.9	9.2	1.7	.909
102.0	103.0	3.8	1.5	93.7	1.0	9.9	3.6	.916
103.0	104.0	2.7	3.0	93.4	.9	6.9	7.2	.922
104.0	105.0	2.5	1.6	95.2	. 7	6.5	3.8	.918
105.0	106.0	1.2	. 7	96.8	1.3	3.1a	1.7	
106.0	107.0	2.6	.7	96.2	.5	6.9	1.7	.912
107.0	108.0	4.1	1.2	93.9	. 8	10.8	2.9	.915
108.0	109.0	1.7	.9	96.8	.6	4.5a	2.2	
109.0	110.0	1.9	1.9	95.7	.5	5.0a	4.6	
110.0	111.0	1.7	1.7	96.0	. 6	4.4a	4.1	
111.0	112.0	8.3	1.7	88.1	1.9	21.8	4.1	.915
112.0	113.0	7.4	1.5	89.8	1.3	19.7	3.6	.906
113.0	114.0	4.5	1.4	92.9	1.2	11.9	3.4	.909
114.0	115.0	3.5	1.3	94.5	. 7	9.1	3.1	.910
115.0	116.0	. 2.8	1.3	95.2	. 7	7.5	3.1	.909
116.0	117.0	6.1	1.4	91.3	1.2	16.0	3.4	.908
117.0	113.0	4.2	1.6	93.1	1.1	10.9	3.8	.914
118.0	119.0	4.8	1.6	92.5	1.1	12.5	3.8	.917
119.0	120.0	7.7	1.5	89.4	1.4	20.0	3.6	.917
120.0	121.0	7.8	1.2	88.8	2.2	20.6	2.9	.914
121.0	122.0	4.5	1.5	92.8	1.2	11.7	3.6	.915
122.0	123.0	8.1	1.7	88.4	1.8	21.4	4.1	.909
123.0	124.0	21.3	1.9	72.7	4.1	56.2	4.6	.907
124.0	125.0	10.1	1.3	86.4	2.2	26.4	3.1	.914
125.0	126.0	13.4	.9	83.1	2.6	35.4	2.2	.907
126.0	127.0	8.6	1.4	88.1	1.9	22.7	3.4	0.913
127.0	128.0	11.3	1.3	84.7	2.7	29.3	3.1	.926
128.0	129.0	8.0	1.4	88.7	1.9	20.7	3.4	.925
129.0	130.0	8.2	1.2	88.6	2.0	21.4	2.9	.922
130.0	131.0	6.8	1.0	90.7	1.5	17.9	2.4	.915
131.0	132.0	12.1	1.0	84.5	2.4	31.5	2.4	.919
132.0	133.0	8.3	1.2	88.4	2.1	21.5	2.9	.927
133.0	134.0	7.9	.9	89.5	1.7	20.5	2.2	.921
134.0	135.0	6.6	1.0	91.0	1.4	17.2	2.4	.922
135.0	136.0	7.7	1.1	89.6	1.6	20.0	2.6	.918
136.0	137.0	9.5	.9	87.7	1.9	25.1	2.2	.911
137.0	138.0	16.1	1.0	79.6	3.3	42.2	2.4	.916
138.0	139.0	11.5	1.0	85.2	2.3	30.1	2.4	.914
139.0	140.0	10.6	.9	86.4	2.1	27.9	2.2	.906
140.0	141.0	14.5	.9	81.2	3.4	38.7	2.2	. 899

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Samples from the U.S. Confessed Survey's Envances

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OIL-SHALE ASSAYS BY MODIFIED FISCHER RETORT METHOD

DIRTHARD ASSAULT NOTE | THE PARTY NAMED IN COLUMN

Samples from the U.S. Geological Survey's Corehole 78-1 (Continued)

				Yield o	of produ	CL		Specific
Tree.		-	Weight	percent		Gal pe	er ton	gravity
	pth			Spent	Gas +			of oil at
From	To	011	Water	shale	loss	0i11/	Water	60°/60° F
1/1 0	1420:	11 0	-	0/ 0	2 1	51.0		0.0.0
141.0	142.0	11.9	. 7	84.3	3.1	31.9	1.7	. 897
142.0	143.0	8.8	.5	89.1	1.6	23.5	1.2	.893
143.0	144.0	5.9	. 4	92.3	1.4	15.8	1.0	. 888
144.0	145.0	7.2	. 4	91.3	1.1	19.4	1.0	.885
145.0	146.0	. 7.2	.6	91.0	1.2	19.3	1.4	.900
146.0	147.0	8.5	.9	89.0	1.6	22.4	2.2	.911
147.0	148.0	4.2	1.1	93.4	1.3	10.9	2.6	.917
148.0	149.0	5.3	1.0	92.2	1.5	14.0	2.4	.908
149.0	150.0	5.8	1.3	91.7	1.2	15.2	3.1	.908
150.0	151.0	3.4	1.3	94.6	.7	8.9	3.1	.921
151.0	152.0	6.1	1.1	91.3	1.5	15.9	2.6	.921
152.0	153.0	5.7	1.0	91.9	1.4	15.0	2.4	.916
153.0	154.0	6.4	1.0	91.2	1.4	17.0	2.4	.911
154.0	155.0	6.4	.9	91.4	1.3	16.9	2.2	.908
155.0	156.0	8.8	1.0	88.5	1.7	23.4	2.4	.902
156.0	157.0	4.1	0.8	94.0	1.1	10.8	1.9	0.903
157.0	158.0	10.2	.9	86.8	2.1	27.1	2.2	.902
158.0	159.0	6.4		91.4	1.3	17.1	2.2	.901
159.0	160.0	4.8	.9	93.0	1.3	12.9	2.2	.903
160.0	161.0	8.7	1.0	88.5	1.8	22.8	2.4	.911
161.0	162.0	11.4	.9	85.7	2.0	30.3	2.2	.898
162.0	163.0	. 8.8	1.0	88.6	1.6	23.3	2.4	.901
163.0	164.0	5.0	.9	93.2	.9	13.2	. 2.2	.902
164.0	165.0	6.8	1.0	90.8	1.4	17.9	2.4	.913
165.0	166.0	5.3	1.0	92.4	1.3	13.8	2.4	.919
166.0	167.0	3.9	. 8	94.3	1.0	10.1	1.9	.922
167.0	168.0	6.7	1.0	91.0	1.3	17.6	2.4	.914
168.0	169.0	. 3.9	1.0	93.8	1.3	10.0	2.4	.919
169.0	170.0	2.5	.7	96.1	.7.	6.6	100	.923
170.0	171.0	2.8	. 8	95.7	. 7	7.4	1.9	.922
171.0	172.0	1.6	1.0	96.8	.6	4.2a	2.4	* / ** **
172.0	173.0	2.3	.8	96.1	.8	6.0	1.9	.925
173.0		1.7	.6	97.1	.6	4.3a	1.4	• > 2 3
174.0	174.0	3.0	.5	95.8	.7	7.9	1.2	.911
175.0	175.0	7.0	1.4	90.3	1.3	18.6	3.4	.904
176.0	176.0	3.8	1.5	93.9	.8	10.0	3.6	.901
177.0	177.0	2.1	2.5	94.1	1.3	5.6		.906
178.0	178.0	3.9	1.0	94.5	.6	10.2	2.4	.915
179.0	179.0		.6	94.5			1.4	.913
180.0	180.0	4.1			. 8	10.9	1.2	
	181.0	3.4	.5	95.4	. 7	8.8		.909
181.0	182.0	3.8	. 8	94.8	.6	9.9	1.9	.913
182.0	183.0	2.5	.6	96.4	.5	6.4	1.4	.921
183.0	184.0	2.4	.6	96.3	. 7	6.3	1.4	.926
184.0	185.0	1.7	.7	96.9	.7	4.4a	1.7	
185.0	186.0	1.7	1.1	96.4	.8	4.4a	2.6	

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OLL-SHALE ASSAYS BY MODIFIED FISCHER RETORT MITHOD

Samples from the U.S. Geological Survey's Corehole 78-1 (Continued)

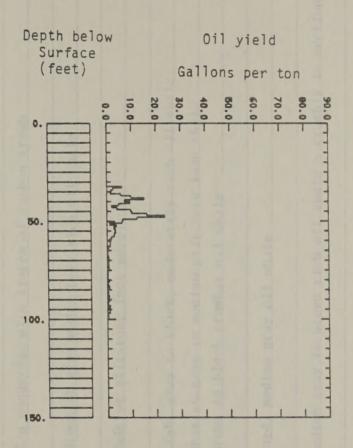
			Weight		of produ	The second secon		Specific
De	pth	-	Mengin	THE RESERVE THE PERSON NAMED IN		Gal pe	T ton	gravity
Fron	To	011	Water	Spent	Gas +	1/		of oil at
		021	MULCI	shale	loss	013-1/	Water	60°/60° F
186.0	187.0	1.9	1.0	96.5	0.6	4.9a	2.4	
187.0	188.0	3.7	1.7	92.7	.9	9.6	4.1	0.920
188.0	189.0	2.9	2.7	93.5	.9	7.7	6.5	.919
189.0	190.0	3.7	. 8	94.4	1.1	9.6	1.9	.920
190.0	191.0	2.6	.4	96.5	.5	6.7	1.0	.923
191.0	192.0	2.7	.7 .	96.1	.5	7.0	1.7	.926
192.0	193.0	2.0	1.2	96.2	.6	5.1a	2.9	
193.0	194.0	1.9	1.5	95.7	.9	.5.1a	3.6	
194.0	195.0	2.6	1.0	,95.7	.7.	6.6	2.4	.935
195.0	196.0	2.0	1.1	96.0	.9	5.2	2.6	.929
196.0	197.0	2.4	. 8	96.1	.7	6.1 *	1.9	.928
197.0	198.0	2.2	1.1	95.6	1.1	5.8	2.6	.926
198.0	199.0	2.5	1.1	95.5	.9	6.4	2.6	.925
199.0	200.0	2.9	1.3	94.8	1.0	7.5	3.1	.928
200.0	201.0	4.3	1.0	93.2	1.5	11.2	2.4	.914
201.0	202.0	3.7	1.1	93.9	1.3	9.7	2.6	.916
202.0	203.0	2.4	1.0	95.7	.9	6.3	2.4	.916
203.0	204.0	1.6	. 4	97.4	.6	4.2a	1.0	. 510
204.0	205.0	1.3	.2	98.0	. 5	3.4a	.5	
205.0	206.0	1.4	.5	97.5	.6	3.7a	1.2	
206.0	207.0	1.8	.3	97.3	.6	4.6a	.7	
207.0	208.0	1.6	.1	97.7	.6	4.3a	. 2	
208.0	209.0	1.2	.4	97.8	.6	3.2a		
209.0	210.0	.6	.4	98.5	.5		1.0	
210.0	211.0	1.4	.3	97.8	.5 .	1.7a	1.0	
211.0	212.0	1.4	.3	97.8	.5	3.7a	. 7	
212.0	213.0	1.3	.2	97.9	.6	3.7a	. 7	
213.0	214.0	.7	.1	98.6		3.4a	. 5	
214.0	215.0	.5	.2	98.7	.6	1.7a	. 2	
215.0	216.0	.7	.2		.6	1.4a	. 5	
216.0	217.0			98.7	0.4	1.9a	.5	
217.0		1.2	0.3	97.7	0.8	3.1a	0.7	
218.0	218.0	1.0	.2	98.3	.5	2.6a	.5	
219.0	219.0	. 8	.1	98.6	.5	2.1a	. 2	
220.0	220.0	. 8	.4	98.2	.6	2.0a	1.0	
221.0	221.0	1.1	.6	97.8	.5	2.8a	1.4	4 7
	222.0	1.8	1.2	96.2	. 8	4.6a	2.9	
222.0	223.0	1.9	.6	96.7	. 8	5.1a	1.4	
223.0	224.0	.5	.3	98.8	.4	1.4a	. 7	
224.0	225.0	.5	. 2	98.7	.6	1.2a	. 5	
225.0	226.0	. 4	. 2	99.2	. 2	.9a	. 5	
226.0	227.0	.5	.3	98.7	.5	1.2a	.7	
227.0	228.0	. 9	. 3	98.2	.6	2.4a	.7	
. 228.0	229.0	. 2	. 3	99.3	. 2	.4a	.7	
229.0	230.0	. 2	. 2	99.3	.3	.4a	.5	
230.0	231.0	.4	. 4	98.9	.3	1.0a	1.0	
231.0	232.0	.4	.4	98.8	:4	1.1a	1.0	

^{1/ &}quot;a"--indicates specific gravity estimated as 0.92.

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U.S. Geological Survey
Core hole 78-1A



FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION
32.2	37.0		Light gray very low grade shale
37.0	39.0		Medium gray moderately rich oil shale
39.0	39.2		Tan sandstone with traces of carbon trash
39.2	39.4		Brownish gray moderately rich oil shale
39.4	39.6		Tuff or siltstone (not sure)
39.6	41.3		Light gray to black, moderately rich oil shale
41-1	43.5		Whitish gray to medium gray very lean shale
43.5	46.5		Brown to black crumbly oil shale
			remainsted took didwers with montraining right and whater
46.5	48.7		Hard, medium gray oll shale
18.7	50.9		Medium gray to brown rich oil shale - crumbly in sections
20.9	51.3		Light brown shale marbled with coarse grain silt
51.3	52.0		ight gray lean oil shale - hard
52.0	52.4		ouff = numerous dingy white layers of ecorse grained material.

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FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION
52.4	62.5		Hard, light gray, lean oil shale
62.5	62.7		Tuff - dingy white coarse grained layer
62.7	72.4		Hard, light gray, lean oil shale
72.4	77.8		Hard, more heavily banded, light gray oil shale (lean)
77.8	80.0		Tuff
80.0	90.4	*	Light gray moderately rich oil shale with intermittent zones of crumbly water
חוו. ט	90.4	-	absorbent shale.
90.4	93.0		Intermingled tuff layers with moderately rich oil shale
93.0	100.2		Gray, lean oil shale.
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OLL-SHALL ASSAYS BY MODIFIED FISCHER REPORT METHOD

Samples from the U.S. Geological Survey's Corchole 78-1A drilled in sec. 6, T 4.S, R. 94 W., Rio Blanco County, Colorado

				Yield o	f prod	uct		Specific
De	pth		Weight	percent		Gal pe	er ton	rravity
		0:1		Spent	Gus +	1/		of nil at
From	То	Oil	Water	shale	loss	0111/	Water	60°/60° F
32.2	2-33.0	2 2	2 5	02 5				
	-34.0	2.3	2.5	93.5	1.7	6.1	6.0	0.923
	-35.0	1.0	2.1	96.1	. 8	2.5a	5.0	
	-36.0	.7	1.3	96.8	1.2	1.8a	3.1	
	-37.0	.6	1.5	97.5	. 4	1.5a	3.6	
	-38.0	2.2	2.2	94.7	.9	5.7	5.3	.913
	-39.0	3.8	2.6	92.3	1.3	9.8	6.2	.916
	1-40.0	5.8	3.6	.88.8	1.8	15.2	8.6	.912
	-41.0	2.7	4.7	91.6	1.0	7.1	11.3	.916
		3.6	2.7	, 92.5	1.2	9.4	6.5	.923
	0-42.0 0-43.0	1.8	2.3	95.3	.6	4.8a	5.5	
		.8	2.6	96.1	.5	2.0a	6.2	
	1-44.0	1.6	4.2	93.1	1.1	4.1a	10.1	
	1-45.0	3.7	5.5	89.6	1.2	9.7	13.2	.907
	1-46.0	3.8	5.5	89.4	1.3	10.2	13.2	.907
	1-47.0	6.1	3.3	88.8	1.8	16.3	7.9	.903
	1-48.0	8.9	3.1	85.8	2.2	23.6	7.4	.907
	1-49.0	4.7	2.9	90.9	1.5	12.2	7.0	.924
	-50.0	2.5	2.8	93.6	1.1	6.4	6.7	.922
50.0	-51.0	2.3	2.6	94.2	.9	6.1	6.2	.915
51.0	-52.0	.5	1.6	97.4	.5	1.2a	3.8	
52.0	-53.0	1.5	2.1	95.9	.5	3.8a	5.0	
53.0	-54.0	1.1	1.9	96.5	.5	2.8a	4.6	
54.0	-55.0	1.3	2.4	95.6	.7	3. 3a	5.8	
55.0	-56.0	1.3	2.8	95.1	.8	3.5a	6.7	
	-57.0	1.1	3.0	95.2				
	-58.0				.7.	3.0a	7.2	
	-59.0	1.1	2.9	94.9	1.1	2.8a	7.0	
	-60.0	.7	3.0	95.2	1.1	1.8a	7.2	
)-61.0	.5	2.8	96.1	. 7	1.2a	6.7	
	0-62.0	.5	2.9	96.1	.5	1.3a	7.0	
		.5	3.0	96.0	.5	1.3a	7.2	
	0-63.0	0.5	1.6	97.5	0.4	1.2a	3.8	
	0-64.0	.0	2.1	97.4	.5	.la	5.0	
)-65.0	.2	2.2	97.3	. 3	.5a	5.3	
	0-66.0	.0	2.1	97.4	.5	Trace	5.1	
	0-67.0	.1	2.3	97.0	.6	. 2a	5.5	
	0-68.0	.1	1.9	97.3	.7	. 3a	4.6	
68.0)-69.0	. 2	1.9	97.4	.5	.6а	4.6	
69.0	0-70.0	.1	2.1	2011	1.1	.4a	5.0	
70.0	71.0	. 2	2.1	96.9	. 8	.6a	5.0	
71.0	72.0	.2	2.0	97.0	. 8	.5a	4.8	
	73.0	.2	2.2	96.9	.7	.6a	5.3	
	0-74.0	. 2	2.3	96.8	.7	.6a	5.5	
	75.0	. 2	2.4	97.0	.4	.4a	5.8	
	0-76.0	.1	2.6	96.8	.5	. 3a	6.2	
	0-77.0	.1	2.1	97.4	-4	. 2a	5.0	
	78.0	.1	2.1	97.2	.6	. 2a	5.0	
11.0	, , , , ,	**		2112				

Samples from the U.S. Sautogical Sarato, a farming to the United in

OIL-SHALE ASSAYS BY MODIFIED FISCHER RETORT MITHOD

Samples from the U.S. Geological Survey's Corehole 78-1A (Continued)

	No.		Yield (of produ	ıcı		Specific
		Weight	percent			er ton	gravity
Depth From To	011	Water	Spent shale	Gas + loss	0i1 ¹ /	Water	of oil at
78.0-79.0	.0	2.3	06 9	0		F F	
79.0-80.0			96.8	.9	Trace	5.5	
80.0-81.0	.1	1.9	97.0	1.0	. 3a	4.6	
	. 3	2.2	96.9	.6	.7a	5.3	
81.0-82.0	0	2.2	96.8	1.0	Trace	5.2	
82.0-83.0	.1	2.7	96.7	. 5	. 3a	6.5	
83.0-84.0	. 3	2.7	96.5	.5	.8a	6.5	
84.0-85.0	. 2	2.9	96.4	.5	.4a	7.0	
85.0-86.0	.0	2.8	96.5	.7	Trace	6.6	
86.0-87.0	.1	2.9	96.4	.6	.4a	7.0	
87.0-88.0	.0	2.8	96.7	.5	Trace	6.6	
88.0-89.0	. 3	2.8	96.6	. 3	. 8a	6.7	
89.0-90.0	.1	2.7	96.6	.6	.4a	6.5	
90.0-91.0	.3	2.6	96.3	. 8	.7a	6.2	
91.0-92.0	.1	2.9	96.6	.4	. 3a	7.0	
92.0-93.0	0.1	2.7	96.6	0.6	0.3a	6.5	
93.0-94.0	. 4	3.3	95.8	. 5	1.la	7.9	
94.0-95.0	.3	3.5	95.4	.8	.7a	8.4	
95.0-96.0	.4	3.1	96.0	.5	1.0a	7.4	
96.0-97.0	.4	3.3	95.7	.6	1.0a	7.9	
97.0-98.0		2.6	96.8	.6		6.2	The state of the s
98.0-99.0	.0				.la		
99.0-100.2	.1	2.5	96.5	.9	.4a	6.0	
33.0-100.2	.0	3.0	96.4	.6	.la	7.2	

[&]quot;--indicates specific gravity estimated as 0.92.

ASSESSMENT AND ADDRESS OF PERSONS ASSESSMENT AND PROPERTY OF PERSONS ASSESSMENT AND PARTY OF PERSONS ASSESSMENT ASSESSMENT

design from the U.S. (Scotlengt) server's Corenal-

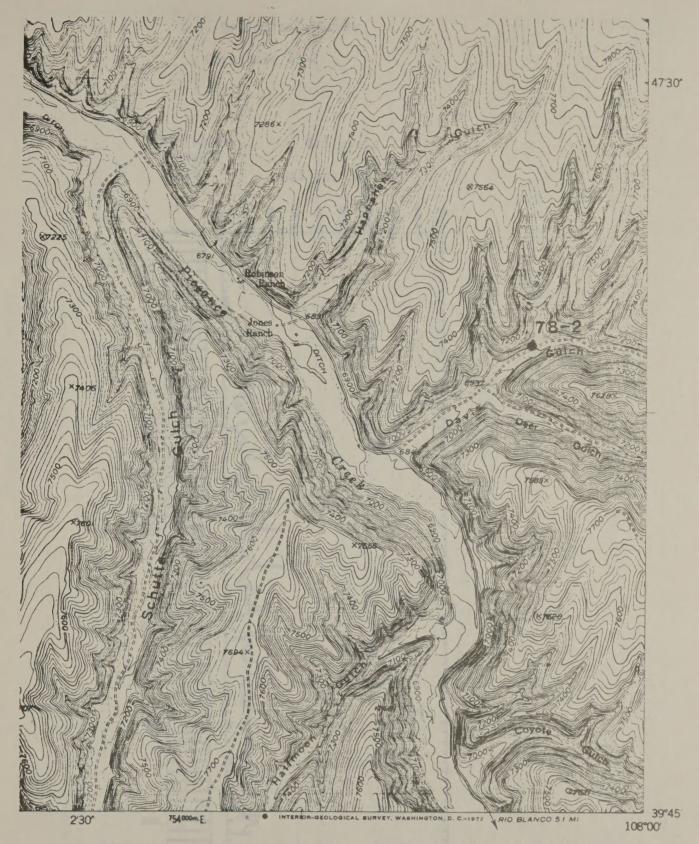
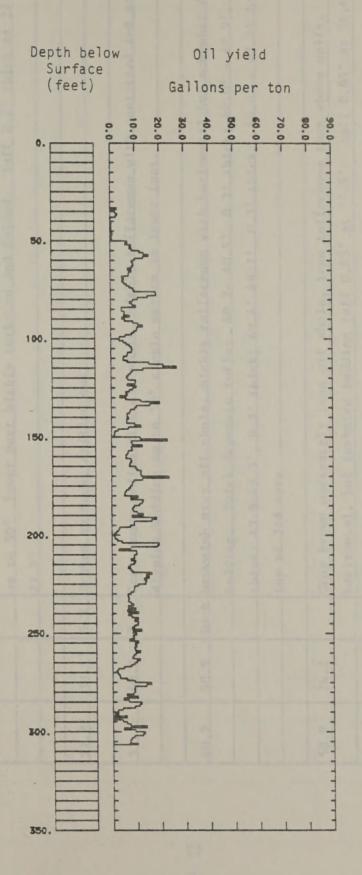


Figure 3.--Map showing location of core hole 78-2. Base from No Name Ridge Quadrangle (1952). Scale 1:24,000.



U.S. Geological Survey

Core hole 78-2



FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION
23.4	27.8	4.4	Lean medium gray partly weathered oil shale, upper part thinly bedded with dips of
			up to 50°, lower part highly turbated and folded. Tuff 0.2' thick at 27.5' to
			27.7'
27.8'	33.1'	5.3	Broken up rock, drilled out
33.1	-40-2	7.1	Gray brown medium rich oil shale, highly tuffaceous with contorted and steeply
			dipping hedding up to 50° ripple markes in lower foot.
40_2	50.9	Dark	brownish gray oil shale, highly tuffaceous with horizontal but somewhat disturbed
			bedding. Thick descrete tuffs: 40.2-40.5', 0.3' thick; 42.0' - 42.9', 0.9'
			thick; 43.0-43.3', 0.3' thick; 49.4' 49.7', 0.3' thick; 46.4' - 47.25 lost at
			top of 3rd core
50.9	76.2		Gray brown moderately lean oil shale, less tuffaceous than above units. Even,
			horizontal, but turbated bedding tuff 0.05' at 53.8'; tuff 0.05' at 56.6'
*			Rich brown oil shale from 56.8' - 59.7'
76.2	79.1		Dark brownish gray moderately rich oil shale, interbedded with minor tuff. Tuff
			0.05' thick at 77.4'
79.1	115.1		Same as interval 50.9-76.2' - tuff 0.05' thick at 88.1'
	anamaig. metrodille houself & r. h.		

FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION
115.1	117.0		Rich oil shale with tuff, thinly bedded, little turbation tuff 0.05' thick at 118.1. Some leaner oil shale mixed in.
117.0	150.7		Same as interval 50.9 76.2'. Tuff 0.05' thick at 119.2; Rich oil shale dark brown 0.1' thick at 132.7'; rich oil shale 132.3 - 133.6 interhedded with moderately rich oil shale and tuff. Tuff 0.05' thick at 135.0'. Rich oil shale 143.6' - 144.4' with tuff.
150.7-	151.5		Rich dark brown thinly bedded oil shale.
151.5	156.4		Medium rich oil shale thinly bedded with moderate turbation. Tuff 0.05' thick at 153.3'. Tuff, turbated 0.05' thick at 154.2'. Tuff turbated 0.05' thick at 156.0'.
156.4	170.2		Same as interval 50.9'-76.2' medium grade oil shale. Tuff with minor oil shale 0.1' thick at 158.3'. Tuff with minor oil shale 0.4' thick 159.8=160.2'. Tuff, turbated 0.05' thick at 160.9', Tuff 0.5' thick at 164.6' and 164.7' and 165.9' and 168.3' and 170.2'.
170.2	171.7		Dark brown rich oil shale with abundant tuff Tuff 0.15' thick at 170.9-171.05'
171.7-	191.3		Medium rich oil shale, thinly bedded with little turbation./Tuffs common thick 179.3-179.5; tuff 0.1' thick at 181.2; tuff 0.1' thick at 181.3; tuff 0.2' thick at 185.0-185.2; tuff 0.3' thick at 187.3-187.6.

FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION
191.3	192.5		Rich dark brown oil shale interbedded with pink and gray tuff. Tuff 0.05'
			thick at 192,2'
192.5	208.1		Medium rich brown to gray brown oil shale, thinly bedded with little turbation.
			Tuffs very common. Tuff 0.07' thick at 195.3; tuff with minor oil shale 0.2'
			thick at 196.1- 196.3. Tuff 0.06' thick at 196.9'; tuff 0.05' thick at 197.5;
			tuff 0.05' thick at 197.6; Tuff 0.15' thick from 198.0-198.15; tuff 0.05' thick
			at 198.3; ruff 0.05' thick at 198.4; tuff 0.05' thick at 198.5; tuff 0.1' thick
			at 199.0; tuff 0.2' thick at 199.2'- 199.4'; rich oil shale, dark brown interbedded
			with tuff 204.2'-205.5'. Tuff 0.15' thick 205.05-205.2; tuff 0.06' thick at
			207.0; thick tuff with minor oil shale toward top 0.8' thick from 207.3-208.1'
208.1	217.1		Dark brown rich oil shale thinly bedded with little turbation. Tuff 0.05' thick
			at 212.7' tuff 0.07' thick at 213.5'; tuff 0.05' thick at 215.5'; tuff 0.08'
			thick at 216.3; tuff 0.1' thick at 217.0.
217.1	256.4		Brown, dark gray brown, moderately rich oil shale with turbation in parts.
			Horizontal thin bedding with abundant tuff. Tuff 0.05' thick at 217.6; tuff 0.1
			thick at 218.8'; tuff 0.2' thick at 219.1-219.3'; tuff 0.4' thick at 220.6-220.9
			Turbated tuff 0.1' thick at 227.0' tuff 0.07' thick at 230.0'; turbate! tuff
	in an automorphism for the second sec		0.2' thick at 230.8-231.0; tuff 0.15' thick at 231.2-231.35; tuff 0.08' thick at
And the second second			232.3'; tuff 0.08' thick at 232.8'; tuff 0.06' thick at 232.9'; tuff 0.1' thick at
an en			233.4'; tuff 0.15' thick at 233.5 to 233.65'; tuff 0.05' thick at 233.7; tuff
	1.000		0.09' at 234.0; tuff 0.07 thick at 234.5; tuff 0.05' thick at 234.9'; tuff 0.08'

		2										
											1	

FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION
264.7	278.2		Brown to gray brown moderately rich oil shale, thinly bedded with little
			turbation. Tuffs abundant. Tuff 0.07' thick at 265.5'; tuff 0.12' thick at
			266 8': tuff 0.08' thick at 268.4'; 50 percent thin tuffs from 268.6-270.9;
			buff 0.06' thick at 273.2'; tuff 0.1' thick at 274.2'; 275.3'-276.7' rich brown
			oil shale interbedded with tuff and leaner oil shale. Tuff 0.15' thick at
			277.45-277.6' with minor shale.
278.2	306.6		Brown to dark brown oil shale, rich, thinly bedded with generally little
-	OF HOLE		Abundant tuff, some leaner oil shale; tuff 0.05' thick at 2/9.4;
BOTTON	OT HOUSE		tuff 0.05' thick at 280.9'; tuff 0.3' thick at 281.6-281.9'; tuff 0.15 tiller
			282 7 - 282 85'; tuff 0.1' thick at 283.0-283.1; tulf 0.2; thick at
			202 15 203 35. tuff 0.3' thick at 283.4-283.7; tuff 0.55' thick at 283.93-204.3,
			tuff 0.15' thick at 283.6-283.75; 50 percent numerous tuffs interbedded with an
			turbated with oil shale 284.8 - 287.3'; Tuff 287.5-292.3' with minor oil shale
			upper foot 4.8' thick total; tuff 0.2' thick with minor shale, turbated from
			292.5=292.7; tuff 292.85 = 294.5, 1.65' thick; 470-percent-tuff, 30-percent oil
			295-0-296-7-1-7' thicki
gat a garantello spirint dell'anni denne material dell'il e			297 5. tuff 0.75' thick at 298.35-299.1; tuff 0.45 thick at 299.5-299.65;
		-	tuff 0.08' thick at 300.05-300.13; tuff 0.1' thick at 301.0' pinkish tan color,
			no gray; tuff 0.5' thick at 301.8-302.3'.
		-	

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Samples from the U.S. Geological Survey's Corchole 78-2 drilled in sec. 24, T. 3 S., R. 95 W., Rio Blanco County, Colorado

	-		Yield e	of prod	uct		Sounds
Depth		Weight	percent		Gal pe	r ton	Specific gravity
ocp til			Spent	Gus +			of nil at
From. To	Oil	Water	shale	loss	0111/	Water	60°/60° F
33.1-34.0	1.0	1.2	97.1	0.7	2.7a	2.9	0.920
34.0-35.0	. 2	3.2	96.1	.5	.5a	7.7	.920
35.0-36.0	. 8	1.4	97.2	.6	2.0a	. 3.4	.920
36.0-37.0	1.1	1.8	96.1	1.0	2.9a	4.3	.920
37.0-38.0	.8	1.8	96.6	.8	2.2a	4.3	.920
38.0-39.0	.0	1.9	97.6	5			
39.0-40.0	.0	1.8	97.7		.1a	4.6	920
40.0-41.0				.5	Trace	4.3	.920
41.0-42.0	.1	2.7	96.6	.6	.2a	6.5	.920
	. 2	1.9	96.3	1.6	.5a	4.6	.920
42.0-43.0	.1	2.5	96.9	.5	.2a	6.0	. 920
43.0-44.0	. 2	1.6	97.7	.5	.4a	3.8	.920
44.0-45.0	. 2	1.3	97.1	1.4	.4a	3.1	.920
45.0-46.0	. 2	2.0	97.1	.7	.6a	4.8	.920
46.0-47.0	.4	2.2	96.7	. 7	.9a	5.3	.920
47.0-48.0	.3	1.6	97.5	.6	.7a	3.8	.920
48.0-49.0	. 2	1.8	97.5	.5	.6a	4.3	.920
49.0-50.0	. 3	2.9	96.2	.6	.7a	7.0	.920
50.0-51.0	2.7	2.6	93.7	1.0	7.0	6.2	.926
51.0-52.0	2.4	2.5	94.3	. 8	6.2	6.0	.926
52.0-53.0	3.3	2.1	93.5	1.1	8.5	5.0	.931
53.0-54.0	3.0	2.2	93.4	1.4	7.8	5.3	.928
54.0-55.0	3.3	2.7	92.9	1.1	8.7	6.5	.920
55.0-56.0	4.5	2.6	91.6	1.3	11.9	6.2	.919
56.0-57.0	5.2	2.6	90.6	1.6	13.6	6.2	
57.0-58.0	6.0	2.6			15.5		.920
58.0-59.0			. 89.6	1.8		6.2	.923
	5.1	2.3	91.2	1.4	13.3	5.5	.924
59.0-60.0	3.8	2.3	92.4	1.5	9.9	5.5	.929
60.0-61.0	3.3	2.7	92.8	1.2	8.6	6.5	.927
61.0-62.0	3.6	2.3	93.0	1.1	9.2	5.5	.925
62.0-63.0	3.6	2.1	93.1	1.2	. 9.4	5.0	.922
63.0-64.0	3.3	1.3	94.4	1.0	8.7	3.1	0.921
64.0-65.0	2.7	. 8	95.6	.9	7.1	1.9	.917
65.0-66.0	3.3	.8	94.6	1.3	8.5	1.9	.920
66.0-67.0	2.9	1.3	94.9	.9	7.5	3.1	.924
67.0-68.0	2.9	2.0	94.4	.7	7.4	4.8	.931
68.0-69.0	1.8	1.9	95.8	.5	4.6a	4.6	.920
69.0-70.0	2.1	1.9	95.3	.7	5.5	4.6	.927
70.0-71.0	1.8	1.9	95.7	.6	4.7a	4.6	.920
71.0-72.0	2.1	2.1	95.1	.7	5.5	5.0	.925
72.0-73.0	2.5	1.8	94.9	.8	6.6	4.3	.923
73.0-74.0	3.0	2.1	93.9	1.0	7.8	5.0	.922
74.0-75.0	3.5	2.0	93.2	1.3	9.2	4.8	.924
75.0-76.0	3.6	2.0	93.1	1.3	9.5	4.8	.921
76.0-77.0	7.1	2.1	89.4	1.4	18.4	5.0	.925
77.0-78.0	7.2	1.8	89.2	1.8	18.6	4.3	.926
78.0-79.0	5.8	1.4	91.6	1.2	15.0	3.4	.920
79.0-80.0	4.2	2.1	92.4	1.3	10.9	5.0	.924

OLL-SHALE ASSAYS BY MODITIED FISCHER RETORT MUTHOD

Semples from the U.S. Geological Survey's Corehole 78-2 (Continued)

			Yield	of pro	ouct		5
Danah	-	Weight	percen	1	The second secon	er ton	Specific
Pepth From To	012		Spent	Gas 4			of oil at
210111	011	Water	shale	loss	011-1	Water.	60°/60°
80.0-81.0	2 5		94,5				0.000
81.0-82.0	3.5	1.7	93.5	1.3	9.0	4.1	.920
82.0-83.0	3.0	1.5	94.5	1.0	7.8	3.6	.924
83.0-84.0	. 3.4	3.0	92.2	1.4	8.8	7.2	.930
84.0-85.0	3.9	2.9	91.9	1.3	10.2	7.0	.928
85.0-86.0	1.7	1.7	96.0	.6	. 4.4a	4.1	.920
86.0-87.0	1.7	1.6	96.1	.6	4.4a	3.8	. 920
87.0-88.0	2.2	1.9	95.4	. 5	5.6	4.6	.926
	2.1	1.8	95.6	.5	5.4	4.3	.933
88.0-89.0	3.0	1.7	94.7	.6	7.8	4.1	.931
89.0-90.0	1.8	1.5	96.1	.6	4.6a	3.6	.920
90.0-91.0	2.2	1.7	95.6	.5	5.7	4.1	.931
91.0-92.0	3.5	2.3	93.3	.9	9.1	5.5	.932
92.0-93.0	4.3	2.5	92.0	1.2	11.1	6.0	.932
93.0-94.0	5.0	2.2	91.6	1.2	13.0	5.3	0.928
94.0-95.0	4.1	2.0	92.7	1.2	10.7	4.8	.925
95.0-96.0	4.0	1.8	93.1	1.1	10.5	4.3	.920
96.0-97.0	3.6	1.9	93.5	1.0	9.5	4.6	.916
97.0-98.0	3.2	2.0	93.7	1.1	8.5	4.8	.914
98.0-99.0	2.2	2.1	94.9	. 8	5.8	5.0	.916
99.0-100.0	1.3	2.6	95.6	.5	3.4a	6.2	.920
100.0-101.0	1.3	2.6	95.6	.5	3.4a	6.2	.920
101.0-102.0	2.0	2.5	94.8	.7	5.1a	6.0	.920
102.0-103.0	2.4	2.5	94.4	.7	6.3	6.0	.928
103.0-104.0	2.9	2.1	94.0	1.0	7.6	5.0	.921
104.0-105.0	3.2	2.1	93.5	1.2	8.4	5.0	.917
105.0-106.0	3.4	2.1	93.2	1.3	8.7	5.0	.919
106.0-107.0	3.2	2.5	93.1	1.2	8.4	6.0	.921
107.0-108.0	2.6	2.4	94.0	1.0	6.8	5.8	.920
108.0-109.0	2.6	2.1	94.6	.7	6.6	5.0	
109.0-110.0	2.0	1.7	95.5	.8	5.1	4.1	.926
110.0-111.0	1.9	1.6	95.8				.931
111.0-112.0	2.6			. 7	4.9a	3.8	.920
112.0-113.0	. 5.9	1.8	94.7	-9	6.7	4.3	.926
113.0-114.0		1.7	91.0	1.4	15.5	4.1	.919
114.0-115.0	8.2	1.9	87.5	2.4	21.3	4.6	.923
115.0-116.0	10.2	1.7	85.5		26.7	4.1	.917
116.0-117.0	5.0	1.7	92.1	1.2	13.0	4.1	.918
117.0-118.0	3.3	1.9	93.8		8.6	4.6	.922
	3.1	2.1	93.9	.9	7.9	5.0	.925
118.0-119.0	2.7	2.2	94.3	.8	7.0	5.3	.923
119.0-120.0	2.4	2.6	94.3	. 7	6.2	6.2	.922
120.0-121.0	2.6	2.2	94.3	.9	6.8	5.3	.919
121.0-122.0		1.6	93.5	1.1	10.0	3.8	.919
122.0-123.0	3.7	1.8	93.3	. 1.2	9.8	4.3	.918

-LANCE REPORT DESCRIPTION OF STREET BEAUTIFUL

descript from the M.S. Control Largest Largest of the Park and American

. 0.16-0.08				
0.24-0.15				

OLL-SHALE ASSAYS BY MODIFIED FISCHER RETORT MITHOD

Bemples from the U.S. Geological Survey's Corehole 78-2 (Continued)

	-		Yield	of prod	1101		
		Weight	percent	ar bron	THE RESERVE AND ADDRESS OF THE PARTY OF THE	er ton	Specific
Depth	-		Spent	Gas +		er ton	gravity
From To	011	Water	shale	loss	0i1-1/	Water.	of oil at 60°/60° F
123.0-124.0	2.5	1.8	94.5	1.2	6.6	4.3	0.922
124.0-125.0	4.0	2.0	92.6	1.4	10.3	4.8	.918
125.0-126.0	3.4	2.0	92.7	1.9	8.8	4.8	.923
126.0-127.0	2.9	2.5	93.6	1.0	7.4	6.0	.924
127.0-128.0	2.3	2.7	93.9	1.1	5.9	6.5	.924
128.0-129.0	2.5	2.3	94.2	1.0	6.6	5.5	.930
129.0-130.0	. 1.3	1.7	96.4	.6	3.5a	4.1	
130.0-131.0	2.3	1.6	95.3			3.8	.920
131.0-132.0				.8	6.0		.922
132.0-133.0	4.6	1.8	92.3	1.3	12.1	4.3	.916
133.0-134.0	7.6	1.7	88.5		19.7	4.1	.922
	6.0	2.1	90.4	1.5	15.7	5.0	.921
134.0-135.0	4.0	1.8	93.1	1.1	10.2	4.3	.929
135.0-136.0	3.7	1.9	93.3	1.1	9.5	4.6	.934
136.0-137.0	3.1	2.0	94.0	.9.	7.8	7.0	.941
137.0-138.0	2.9	2.4	93.3	1.4	7.4	5.8	.939
138.0-139.0	2.5	2.4	94.3	. 8	6.4	5.8	.939
139.0-140.0	2.5	2.3	94.1	1.1	6.4	5.5	. 9 36
140.0-141.0	2.7	2.0	94.2	1.1	7.0	4.8	.935
141.0-142.0	2.4	1.6	94.9	1.1	6.2	3.8	.935
142.0-143.0	2.4	1.6	94.9	1.1	6.3	3.8	.928
143.0-144.0	3.7	2.1	92.7	1.5	9.5	5.0	.920
144.0-145.0	4.6	2.2	91.4	1.8	12.0	5.3	.921
145.0-146.0	2.6	,1.9	94.3	1.2	6.9	4.6	.914
146.0-147.0	1.0	1.6	96.6	. 8	2.7a	3.8	.920
147.0-148.0	.5	1.6	97.1	.8	1.4a	3.8	.920
148.0-149.0	.5	1.6	97.1	. 8	1.3a	3.8	.920
149.0-150.0	. 4	1.5	97.4	.7	1.0a	3.6	.920
150.0-151.0	4.5	2.1	91.6	1.8	11.7	5.0	.923
151.0-152.0	8.9	2.0	87.0	2.1	22.8	4.8	.936
152.0-153.0	3.1	2.3	93.4	1.2	8.0	5.5	.933
153.0-154.0	3.3	2.7	92.8	1.2	8.4	6.5	0.935
154.0-155.0	4.9	2.0	91.5		12.6	4.8	. 9 36
155.0-156.0		2.0		1.4		4.8	.932
156.0-157.0		1.9			8.5		.932
157.0-158.0	2.6	1.5	94.8	1.1	6.8	3.6	.928
158.0-159.0	2.5	1.3	95.1	1.1	6.5		
159.0-160.0	. 2.2	1.4			0 2	2 1.	.927
160.0-161.0	2 2		95.2		5.8	3.4	.927
161.0-162.0	2.3	1.6	95.1				.927
162.0-163.0	3.1	1.6	94.1		7.9	3.8	.929
163.0-164.0	3.2	2.2	93.4		8.2	5.3	.928
	2.9	2.1	93.8		7.5		.924
164.0-165.0	2.8	1.8	94.2		7.3	4.3	.916
165.0-166.0	3.7	1.8	92.9		9.8	4.3	.914
166.0-167.0	4.0	1.8	92.6		10.3		.916
167.0-168.0	4.6	2.6	91.1	1.7		6.2	.915
168.0-169.0	4.5	1.9	92.0	1.6	11.7	4.6	.921
169.0-170.0	4.6	1.9	91.6	1.9	12.1	4.6	.918

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Oll-SHALE ASSAYS BY MODIFIED FISCHER RETORT METHOD Samples from the U.S. Geological Survey's Corehole

. 78-2 (Continued)

			Yield	of produ	ict		5
		Weight	percent		Ga) pe	T POR	Specific
Depth	1 199		Spent	Gas +		LUI	gravity
From To	0:1	Water	shale	loss	0il-/	Water.	of oil at 60°/60° F
170.0-171.0	9.0	2.2	86.3	2.5	23.4	5.3	.921
171.0-172.0	4.9	2.2	90.8	2.1	12.6	5.3	
172.0-173.0	3.5	1.2	94.1	1.2	9.0	2.9	.929
173.0-174.0		1.2			8.4		.932
174.0-175.0	3.2		94.5	1.1		2.9	.927
175.0-176.0	3.2	1.2	94.5	1.1	8.3	2.9	.931
	3.0	.1.5	94.2	1.3	7.6	3.6	.937
176.0-177.0	2.7	1.9	94.0	1.4	7.0	4.6	.937
177.0-178.0	2.3	1.4	95.4	.9	5.9	3.4	.931
178.0-179.0	2.1	1.5	95.6	. 8	5.4	3.6	.926
179.0-180.0	2.0	1.4	95.8	. 8	5.2a	3.4	.030
180.0-181.0	4.1	1.4	93.1	1.4	10.7	3.4	.927
181.0-182.0	3.0	1.7	94.1	1.2	7.7	4.1	.922
182.0-183.0	4.9	2.1	91.4	1.6	12.8	5.0	.923
183.0-184.0	4.8	1.9	91.8	1.5	12.4	4.6	.929
184.0-185.0	4.4	2.0	92.3	1.3	11.3	4.8	.931
185.0-186.0	3.6	2.1	93.3	1.0	9.1	5.0	.936
186.0-187.0	3.3	2.2	93.6	.9		5.3	.934
187.0-188.0	3.4	2.2	93.4	1.0	8.8	5.3	.933
188.0-189.0	4.1	1.7 .		1.1	10.5	4.1	.923
189.0-190.0	4.9	1.3	.92.4	1.4	12.9	3.1	.918
190.0-191.0	3.2	1.5	94.4	.9	. 8.3	3.6	.918
191.0-192.0	7.0	1.8	. 89.6	1.6	18.2	4.3	.920
192.0-193.0	6.3	1.5	90.7	1.5	16.3	3.6	.919
193.0-194.0	3.5	1.0	94.4	1.1	9.0	2.4	.917
194.0-195.0	3.5	1.0	94.3	1.2	9.2	2.4	.917
195.0-196.0	2.8	1.0	95.1	1.1	7.5	2.4	.914
196.0-197.0	1.2	. 8	97.1	.9	3.1a	1.9	.920
197.0-198.0	1.1	1.0	97.0	.9	2.8a	2.4	.920
198.0-199.0	. 7	.9	97.6	.8	1.9a	2.2	.920
199.0-200.0	. 4	.8	98.2	.6	1.1a	1.9	.920
200.0-201.0	.4	.9	97.7	1.0	1.1a	2.2	.920
201.0-202.0	.5	1.0	97.5	1.0	1.3a	2.4	.920
202.0-203.0	. 8	1.1	97.3	.8	2.2a	2.6	. 920
203.0-204.0	1.6	1.4	96.1	.9	4.2a	3.4	. 920
204.0-205.0	7.5	1.8	88.7	2.0	19.3	4.3	.927
205.0-206.0	7.3	2.2	88.4	2.1	18.7	5.3	.930
206.0-207.0	3.0	2.4	93.4	1.2	7.8	5.8	.931
207.0-208.0	1.1	1.7	96.4	.8.	2.7a	4.1	.930
208.0-209.0	3.9		92.8	1.2	10.0	5.0	.926
209.0-210.0	3.9	2.3	92.4	1.4	10.1	5.5	.929
210.0-211.0	3.5	2.3	93.0	1.2	8.9	5.5	.931
211.0-212.0	3.5	2.0	93.3	1.2	9.2	4.8	.926
	3.0	1.7	94.2	1.1	7.7	4.1	.927
212.0-213.0	3.0	7.1	34.4	1.1	, . ,	4.7	. 121

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Samples from the U.S. Geologics: Survey's Corehole 78-2 (Continued)

	-	Madazz	Yaeld o			Specific	
Sanak.	-	Merkut	percent		Gal D	er ton	gravity
Prom To	011	Water	Spent	Gas +	013-1/	11-4	of oil at
1100	0.1	MULEI	anale.	1088	013-	Water.	60.140. £
213.0-214.0	3.7	1.7	93.3	1.3	9.6	4.1	0.928
214.0-215.0	3.5	1.5	93.7	1.3	9.0	3.6	.925
215.0-216.0	2.9	1.2	95.0	9	7.4	2.9	.923
216.0-217.0	2.6	1.1	94.9	1.4	6.6	2.6	.925
217.0-218.0	3.0	2.1	94.0	.9	7.6	5.0	.932
218.0-219.0	3.2	2.0	93.9	.9	8.3	4.8	.930
219.0-220.0	. 6.3	2.2	90.1	1.4	16.2	5.3	.935
220.0-221.0	5.4	2.9	90.4	1.3	13.9	. 7.0	.937
221.0-222.0	5.9	2.0	90.8	1.3	15.1	4.8	.932
222.0-223.0	5.1	2.2	91.5		13.1	5.3	.936
223.0-224.0	5.5	2.1	91.1	1.3	14.0	5.0	.938
224.0-225.0	5.3	1.6	91.8	1.3	13.6	3.8	.933
. 225.0-226.0	4.1	1.5	93.0	1.4	10.6	3.6	.934
226.0-227.0	3.6	1.6	93.8	1.0.	9.1	3.8	.940
227.0-228.0	3.5	1.5	94.0	1.0	9.0	3.6	.938
228.0-229.0	3.4	1.1	94.7	.8	8.7	2.6	.935
229.0-230.0	3.0	1.2	95.1	.7	7.6	2.9	.936
230.0-231.0		2.0	94.8	.7	6.4	4.8	.940
	2.5	.9	95.8	.7	6.6	. 2.2	.927
231.0-232.0	2.6			.7	6.9	1.9	.925
232.0-233.0	2.7	.8	95.8			1.9	.927
233.0-234.0	2.5	.8	95.8	.9	6.5	2.2	.927
234.0-235.0	2.9	.9	95.3	.9	7.6		.931
235.0-236.0	3.4	.1.4	94.4	. 8	8.7	3.4	.928
236.0-237.0	2.5	1.3	95.5	.7	6.5	3.1	.923
237-0-238.0	3.7	1.3	94.0	1.0	6.2	6.0	.930
238.0-239.0	2.4	2.5	94.1	1.0		9.1	.942
239.0-240.0	4.2	3.8	91.2	. 8	10.7	10.8	.948
240.0-241.0	2.6	4.5	92.4	.5	6.5	4.8	.937
241.0-242.0	3.1	2.0	94.0	.9	7.9	4.3	.935
242.0-243.0	4.1	1.8	92.9	1.2	10.6	4.6	0.939
243.0-244.0	3.6	1.9			10.6	4.3	.943
244.0-245.0	4.2	1.8	92.9	1.1	10.4	4.6	.941
245.0-246.0	4.1	1.9	93.0	1.0		4.1	.936
246.0-247.0	3.5	1.7	94.2	.6	9.0	3.6	.937
247.0-248.0	3.1	1.5	94.4	1.0	8.0	2.9	.933
248.0-249.0	4.6		92.9.		11.9		.928.
249.0-250.0	3.2	1.3	94.6	.9	8.3	3.1	.936
250.0-251.0	3.8	1.9	93.3	1.0	.9.8	4.6	
251.0-252.0	3.3	1.0	,94.8	.9.		2.4	.933
252.0-253.0	3.4	.9	94.7	1.0	8.9	2.2	.927
253.0-254.0	2.7	.9	95.5	.9	7.0	2.2	.928
254.0-255.0	4.1	1.2	93.6	1.1	10.6	2.9	.931
255.0-256.0	3.6	1.3	94.3	. 8	9.2	3.1	.934
256.0-257.0	3.9	1.5	93.6	1.0	9.9	3.6	.935
257.0-258.0	3.5	1.7	94.0	.8	9.0	4.1	.933
258.0-259.0	3.7	1.3	93.9	1.1	9.4	3.1	.930
259.0-260.0	4.4	2.5	92.1	1.0	11.4	6.0	.933

Sumples from the U.S. Sealington Sover's Consider

			E.E.	
			0.0	
				257.0-250.0

OIL-SHALF ASSAYS BY MODITIED FISCHER RETORT METHOD

Samples from the U.S. Geological Survey's Corehole 78-2 (Continued)

			10-2				
		None	Yield c			Specific	
Depth	Contraction of the last of the	Weight	The second name of the second		الا [الم	er ton	gravity
Pron To	011	Water	Spent	Gas +	0111/	Water.	of oil at 60°/60° F
260.0-261.0	3.7	1 0	02.5	1.0			
261.0-262.0		1.8	93.5	1.0	9.5	4.3	.934
262.0-263.0	3.4	1.2	94.2	1.2	8.6	2.9	.932
263.0-264.0	3.1	1.2	94.7	1.0	8.1	2.9	.928
264.0-265.0	4.3	1.1	93.0	1.6	11.2	2.6	.929
265.0-266.0	3.9	1.1	93.9	1.1	10.0	2.6	.930
266.0-267.0	3.5	1.2	94.3	1.0	9.0	2.9	.931
267.0-268.0	3.0	1.6	94.6	. 8	7.7	3.8	.931
268.0-269.0	1.8	. 8	96.7	.7 .		1.9	. 920
	.9	.9	97.7	.5	2.3a	2.2	.920
269.0-270.0	.6	.9	98.0	.5	1.6a	2.2	.920
270.0-271.0	. 9	1.2	97.4	.5	2.3a	2.9	:920
271.0-272.0	1.1	1.3	97.0	.6	2.9a	3.1	.920
272.0-273.0	1.2	1.3	96.9	.6	3.1a	3.1	.920
273.0-274.0	2.3	1.9	95.0	0.8	5.9	4.6	0.923
274.0-275.0	3.5	1.6	93.9	1.0	9.1	3.8	.928
275.0-276.0	6.1	1.8	90.4	1.7	15.8	4.3	.924
276.0-277.0	5.3	1.6	91.6	1.5	13.8	3.8	.924
277.0-278.0	3.5	1.2	94.2	1.1	9.1	2.9	.925
278.0-279.0	3.4	1.6	93.8	1.2	8.9	3.8	.929
279.0-280.0	3.5	1.6	93.7	1.2	9.2	3.8	.926.
280.0-281.0	3.3	1.8	93.7	1.2	.8.6	4.3	.925
281.0-282.0	2.2	1.8	.95.9	.9.	5.7	4.3	.926
282.0-283.0	4.0	1.7	93.2	1.1	10.3	4.1	.925
283.0-284.0	1.7	2.7	94.8	. 8	4.4a	6.5	.920
284.0-285.0	2.5	1.9	94.3	1.3	6.6	4.6	.921
285.0-286.0	4.5	1.9	92.3	1.3	11.7	4.6	.919
286.0-287.0	4.2	2.0	92.5	1.3	10.9	4.8	.923
287.0-288.0	3.4	2.8	92.7	1.1	8.9	6.7	.925
288.0-289.0	1.6	3.8	93.8	. 8	4.1a	9.1	.920
289.0-290.0	. 8	4.3	94.2	.7	2.1a	10.3	.920
290.0-291.0	.9	4.3	93.9	.9	2.3a	10.3	.920
291.0-292.0	.3	4.4	94.6	.7	.9a	10.5	.920
292.0-293.0	2.2	3.3	93.5	1.0	5.7	7.9	.933
293.0-294.0	.2	3.7	95.7	. 4	.5a	8.9	.920
294.0-295.0	1.6	3.1	94.6	.7	4.2a	7.4	. 920
295.0-296.0	2.3	3.1	93.7	.9	5.7	7.4	.941
296.0-297.0	2.8	2.3	93.8	1.1	7.2	5.5	.943
297.0-298.0	5.4	1.5	92.0		13.8	3.6	.938
298.0-299.0	1.7	3.0	94.8	.5	4.4a	7.2	.920
299.0-300.0	3.6	1.2	94.2	1.0	9.1	2.9	.932
300.0-301.0	5.1	1.4	92.3	1.2	13.1	3.4	.928
301.0-302.0	4.8	1.5	92.6	1.1	12.3	3.6	.926
302.0-303.0	3.4	1.8	93.9	.9	8.7	4.3	.935
302.0-303.0	3.4	1.0	23.7	• >	0.7	7.3	1723

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200.0-200.0 200.0					
281,0-281,0					
280.0-281.0 281.0-281.0 282.0-281.0 283.0 283.0-281.0 283.0-281.0 283.0-281.0 283.0-281.0 283.0-281.0 283.0-281.0 283.0-281.0 283.0-281.0 283.0-281.0 283.0-281.0 283.0-281.0 283.0-281.0 283.0-281.0 283.0-281.0 283.0-281.0 283.0-281.0					
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					0.000-0.085

Semples from the U.S. Geological Survey's Corehole 78-2 (Continued)

			Yzeld c	of procu	cı		Specific
		Weight	percent		Cai) pe	r ton	gravity
Prom To	011	Water	Spent	Gas + loss	013-1/	Water.	of oil at 60°/60°
303.0-304.0	3.0	1.5	94.8	0.7	7.6	3.6	0.934
304.0-305.0	2.7	1.2	95.5	.6	7.0	2.9	.932
305.0-306.0	2.7	1.2	95.5	.6	7.0	2.9	.927
306.0-306.6	3.9	1.1	94.2	. 8	10.1	2.6	.929

^{1/ &}quot;a"--indicates specific gravity estimated as 0.92.

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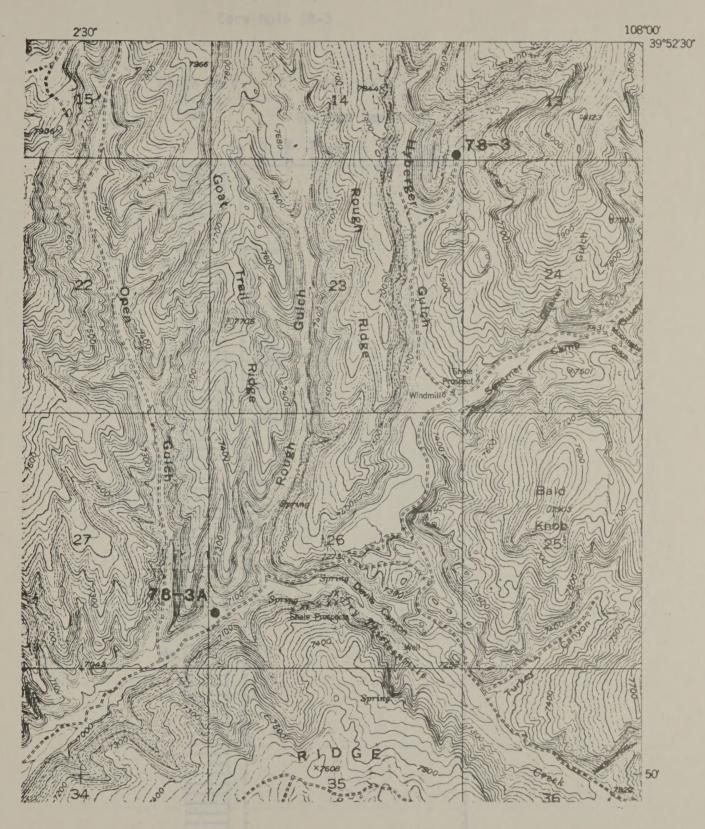
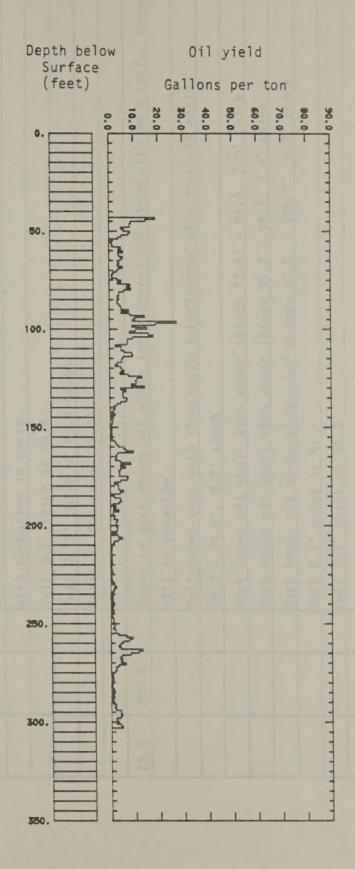


Figure 4.--Map showing location of core holes 78-3 and 78-3A. Base from No Name Ridge Quadrangle (1952). Scale 1:24,000.



U.S. Geological Survey

Core hole 78-3



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Corehole 78-3 Logged by Kurt Hollocher

FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION
3.0	77.7		Moderately rich oil shale with much admixed tuff or silt. Color is brown to
			brownish gray. Thin, even bedding
			with turbation in parts.
			Tuff 0.1' thick at 45.8'
			Tuff 0.75' thick at 63.9-64.65
			Vertical fractures 72-74'
77.7	220.0		Brown to dark brown oil shale interlayered and mixed with much tuff. Abundant
			silt is possible
			Tuffaceous zone with thin tuffs interlayered with rich oil shale.
			78.3 - 79.0', 0.7' thick
			Dark brown oil shale with other things 92.6' - 94.6, 2.0' thick
			Dark brown oil shale with other things 95.7 - 98.5, 2.8' thick
			Dark brown oil shale with other things 97.8 - 106.5' 8.7' thick
			Tuff 0.1' thick at 92.6'
			Tuff 0.1' thick at 95.2
		,	Zone weathered to plastic mud 0.07' thick at 100.6'
			Zone ←50percent massive gray tuff 108.4-109.8; 1.4' thick
			Very dark brown oil shale 109.8-109.9, 0.1' thick
			Dark brown oil shale interlayered with tuff and leaner oil
			Shale 112.3' - 113.9' - 1.6' thick
			Tuff 0.1' thick at 116.1
			ruff 0.2' thick at 118.6 - 118.8'
			ruff 0.2' thick at 126.2 - 126.4

FROM	TO	THICK- NESS	LITHOLOGIC DESCRIPTION
			Tuff 0.2' thick at 128.2- 128.4
			Tuff 0.1' thick at 129.9
			Tuff 0.2' thick at 130.3- 130.5
			Tuff 0.15' thick at 130.7-130.85
			Fractures: 128' - 130'
			134.5 - 140' highly fractured
			Tuff 0.15' thick at 144.9 - 145.05
			Tuff 0.25' thick at 147.0 - 147.25
			Tuff 0.3' thick at 155.3 - 155.6 with some oil shale
			Tuff 0.1' thick at 156.4
			Tuff 0.5' thick at 157.6-158.1 turbated with oil shale
			Tuff 0.1' thick at 163.2'
			Tuff 0.1' thick at 164.7'
			Tan tuff 0.5' thick at 169.3-169.8 with some oil shale
	1		Dark brown rich oil shale interhedded with leaner oil shale and tuff 160,3-162,8,
			2.5' thick
			168.6-170.5, 1.9' thick
	na danas de dendado e Malado de Pere		ruff 0.1' thick at 174.4
			ruff 0.3' thick at 176.7- 177'
			ruff 0.15' thick at 177.4 - 177.55
			ruff 0.1' thick at 177.7 - 177.8
			ruff 0.1' thick at 178.2'
			ruff 0.2' thick at 186.5-186.7 with mixed oil shale
			fulf 0.3' thick at 187.0-187.3 with mixed off shale

FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION
			Dark brown rich oil shale with tuff 186.8 - 187.6, 0.8'
			Tuff 2.25' thick at 187.6-189.85 with minor mixed shale
			Tuff 0.1' thick at 189.9
			60 percent massive tuff zone 190.1-191.3, 1.2' thick with 40 percent dark
			brown oil shale
			Tuff 0.15' thick at 191.85'-192.0
			Tuff 0.15' thick at 192,2-192.35'
			Tuff 0.2' thick at 193.5 - 193.7'
			Tuff 0.15' thick at 197.8-197.95
			Tuff 0.25' thick at 199.85-200.1' with minor shale
			Tuff 0.15' thick at 203.15 - 203.3' 204.0-205.5' highly fractured
			Tuff 0.15' thick at 205.6-205.75'
			Tuff 0.1' thick at 206.2
			Tuff 0.1' thick at 206.7
			ruff 0.18' thick at 210.0'210.18'
			ruff 0.2' thick at 210.9-211.1
			Tuff 0.1! thick at 215.3'
			Tuff 0.1' thick at 215.5'
	-		ruff 0.45' thick at 216.6-217.05 with mixed shale
			ruff 0.4' thick at 218.0-218.4 with mixed shale
			ruff 0.1' thick at 218.9'
			ruff 0.2' thick at 220.0' - 220.2'

|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|

FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION
220.0	255.5		Gray to brown oil shale mixed and hedded with much silt or/and tuff. Oil Shale
			is lean to moderate. Generally evenly bedded with little turbation
			Tuff 0.2' thick at 234.2'-234.4'
			Tuff 1.0' thick at 235.2-236.2'
			Tuff 0.1' thick at 238.3
			Tuff 0.1' thick at 240.9'
			Tuff 0.15' thick at 242.05-242
			Tuff 0.15' thick at 245.1-245.25
			Tuff 0.2' thick at 245.4-245.6'
			Tuff 0.3' thick at 252.6-252.9 with some shale
			Tuff 0.15' thick at 254.5'
255.5	273.4		Gray brown to brown oil shale moderately lean with less silt than above unit.
			Shale is somewhat fissile.
			Some parts brown to dark brown oil shale with interlayered tuff.
			Dark brown oil shale with abundant thin tuff layers near base, 256.7-258.4
			Tuff 0.1' thick at 264.3'
273.4	302.9		Similar to interval 220.0 - 255.5'
			ruff 0.1' thick at 276.5'
			ruff 0.1' thick at 289.6'
A-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1			

FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION		
			Tuff 0.1' thick at 291.5'		
			Tuff 0.1' thick at 292.1'		
			Tuff 0.1' thick at 292.5'		
			Tuff 0.15' thick at 292.7-292.9'		
			Tuff 0.1' thick at 300.1'		
			AND		
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	and the second s				-
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Samples from the U.S. Geological Survey's Corolole 78-3 drilled in sec. 14, T. 2 S., R 95 W, Rio Blanco County. Colorado

		* *************************************						
					of produ	ict		Specific
Dep	th		Weight	percent		Gal p	er ton	gravity
		0:1	11	Spent	Gus +	0111/	:	of oil at
From	To	 Oil	Water	shale	loss	011=	Water	60°/60° F
43.0	44.0	7.1	3.0	88.0	1.9	18.9	7.2	0.897
44.0	45.0	5.6	3.1	89.8	1.5	14.8	7.4	.908
45.0	46.0	3.4	3.1	92.3	1.2	8.8	7.4	.916
46.0	47.0	3.2	2.6	93.2	1.0	8.4	6.2	.911
47.0	48.0	3.2	2.2	93.4	1.2	8.4	5.3	.914
48.0	49.0	1.9	2.0	95.3	. 8	4.8a	4.8	
49.0	50.0	2.3	1.8	95.1	3.	5.9	4.3	.916
50.0	51.0	3.3	1.7	93.6	1.4	8.6	4.1	.914
51.0	52.0	3.0	2.3	93.6	1.1	7.8	5.5	.913
52.0	53.0	1.9	1.9	95.2	1.0	5.0a	4.6	.,,,
53.0	54.0	1.4	1.8	96.0	.8	3.7a	4.3	
54.0	55.0	.2	1.6	97.7	.5	.5a	3.8	
55.0	56.0	. 3	1.4	97.7	.6	.8a	3.4	
56.0	57.0	.5	1.6	97.4	.5	1.2a	3.8	
57.0	58.0	.5	1.6	96.7	1.2	1.3a	3.8	
58.0	59.0	1.8	2.6	94.8	.8	4.8a		
59.0	60.0	1.4	2.3	95.6	. 7		6.2	
60.0	61.0	2.1	2.3	93.8	1.8	3.7a	5.5	0.2.6
61.0	62.0	1.4	1.9	96.0		5.6	5.5	.916
62.0	63.0	1.5	2.3	95.5	. 7	3.6a	4.6	
63.0		2.1	3.0		.7	4.0a	5.5	1000
64.0	64.0	1.3	4.6	94.1	.8	5.5	7.2	.919
65.0	66.0	1.3	1.3	92.5	1.1	4.8a	11.0	
66.0	67.0	1.6	1.7	96.0	- 8	3.4a	4.3	
67.0	38.0	1.3	1.9		. 7	4.1a	4.1	
68.0		2.1	1.9	96.1	. 7	3.3a	4.6	
69.0	69.0			95.2	. 8	5.4	4.6	.912
	70.0	1.4	1.3	96.3	1.0	3.7a	3.1	
70.0	71.0	1.2	1.4	96.8	.6	3.0a	3.4	
71.0	72.0	. 7	1.2	97.6	. 5	1.7z	2.9	
72.0	73.0	0.4	1.3	97.9	. 4	1.0a	3.1	
73.0	74.0	0.4	1.3	97.8	0.5	1.la	3.1	
74.0	75.0	1.2	1.6	96.5	.7	3.2a	3.8	
75.0	76.0	1.8	1.9	95.2	1.1	4.8a	4.6	
76.0	77.0	1.3	2.0	96.0	. 7	3.4a	4.8	
77.0	78.0	3.3	2.2	93.4	1.1	8.5	5.3	0.920
78.0	79.0	2.7	2.0	93.6	1.7	7.0	4.8	.920
79.0	80.0	3.3	2.2	93.4	1.1	8.8	5.3	.908
80.0	81.0	2.2	1.8	94.8	1.2	5.9	4.3	.904
81.0	82.0	1.5	1.7	95.9	.9	3.9a	4.1	
82.0	83.0	1.5		96.5	.3	3.9a	4.1	
83.0	84.0	1.2	2.1	96.2	.5	3.1a	5.0	
84.0	85.0	1.5	2.0	96.1	.4	3.9a	4.8	
85.0	86.0	1.2	2.4	96.0	. 4	3.2a	5.8	
86.0	87.0	1.2	1.9	96.1	. 8	3.1a	4.6	
87.0	88.0	1.5	2.0	96.1	. 4	3.9a	4.8	
88.0	89.0	1.8	2.1	95.7	. 4	4.6a	5.0	
89.0	90.0	1.8	2.1	95.7	. 4	4.8a	5.0	

NAME AND ADDRESS OF TAXABLE PARTY AND PERSON OF TAXABLE PARTY.

DESCRIPTION OF PERSONS ASSESSED BY THE PARTY OF THE PARTY

Samples from the U.S. Geological Survey's Corehole 78-3 (Continued)

					With the same of		
	Weight percen Spent 0-91.0 3.0 2.2 93.7 .0-92.0 1.8 1.8 95.2 .0-93.0 3.2 2.4 93.3 .0-94.0 5.6 2.6 90.4 .0-95.0 3.9 2.0 92.9 .0-96.0 3.6 2.0 93.3 .0-97.0 10.4 2.4 84.9 .0-98.0 7.1 2.5 88.7 .0-99.0 3.5 2.2 92.8 .0-100.0 5.8 1.9 90.8 .0-101.0 4.0 2.1 92.7 .0-102.0 3.1 1.2 94.1 .0-103.0 6.1 1.8 90.6 .0-104.0 6.7 2.8 86.8 .0-105.0 3.6 2.5 92.8 .0-106.0 2.7 2.2 94.0 .0-107.0 2.8 1.9 94.3 .0-108.0 2.7 2.1 94.1 <th>Yield</th> <th>of proc</th> <th>duct</th> <th></th> <th>Spanist</th>	Yield	of proc	duct		Spanist	
Prop To		Weight	percent		The second secon	er ton	Specific gravity
Depth			Spent	Gas +			of oil at
From To	Oil	Water	shale	loss	0i1 ¹ /	Water	60°/60° F
90 0-91 0	3.0	2 2	03 7	7 7			
				1.1	7.9	5.3	.909
				1.2	4.8a	4.3	33.6
				1.1	8.4	5.8	.913
				1.4	14.4	6.2	.926
				1.2	10.3	4.8	.919
				1.1	9.4	4.8	.915
				2.3	27.4	5.8	.910
				1.7	18.8	6.0	.904
98.0-99.0				1.5	9.2	5.3	.920
99.0-100.0				1.5	15.3	4.6	.915
100.0-101.0				1.2	10.5	5.0	.917
101.0-102.0	3.1		94.1	1.6	8.2	2.9	.917
102.0-103.0	6.1	1.8	90.6	1.5	15.9	4.3	.914
103.0-104.0	6.7	2.8	88.8	1.7	17.8	6.7	0.902
104.0-105.0	3.6	2.5		1.1	9.4	6.0	.908
105.0-106.0	2.7			1.1	7.3	5.3	.898
106.0-107.0				1.0	7.3	4.6	.911
107.0-108.0				1.1	7.1	5.0	.908
108.0-109.0				.6	2.2a	4.6	. 300
109.0-110.0				.8	4.7a	5.3	
110.0-111.0				1.3	4.7a	4.1	
111.0-112.0				.8	6.0	5.3	012
112.0-113.0				1.0	9.1	5.5	.912
113.0-114.0				1.1			.915
114.0-115.0				.6	9.4	5.8	.927
					5.4	3.6	.918
				. 7	4.8a	4.6	
				1.1	4.9a	5.0	
				1.0	3.la	4.1	
				.8	2.2a	4.1	
				1.8	4.5a	3.4	
				1.0	4.9a	5.5	
				1.2	5.8	5.0	.912
				1.4	4.21	5.0	
				1.3	7.6	4.3	.906
124.0-125.0				1.2	13.1	4.8	.902
125.0-126.0				1.3	11.1	4.8	.905
126.0-127.0				1.1	10.5	4.3	.898
127.0-128.0				1.1	10.9	3.1	.892
128.0-129.0			94.3	1.1	8.7	3.1	.906
129.0-130.0		1.7	91.4	1.6	14.2	4.1	.902
130.0-131.0	1.7	1.5	95.8	1.0	4.4a	3.6	21.7
131.0-132.0	2.5	1.5	95.0	1.0	6.6	3.6	.911
132.0-133.0	2.0	1.5	95.5	1.0	5.2	3.6	.918
177-0-175-00-		i din di	7000		- 4-40	Die -	. > 1.0

IN VOICES STOLES OF LIGHT OF SYATAA LIAME-110

Samples from the U.S. Scalingham Survey a Contract

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Samples from the U.S. Geological Survey's Corehole 78-3 (Continued)

			Yield	of prod	NA PERSON	WA CAR	mote
		Weight	percent	or prodi	The second secon		Specific
Depth			Spent	Gas +	Gál pe	er ton	gravity
From To	011	Water	shale	loss	013-1/	Water	of oil at 60°/60° F
133.0-134.0	2.0	1.5	95.7	0.8	5.3	3.6	0.921
134.0-135.0	2.1	1.5	95.4	1.0	5.4	3.6	.922
135.0-136.0	2.7	1.5	94.8	1.0	7.0	3.6	.920
136.0-137.0	2.6	1.5	94.8	1.1	6.7	3.6	.916
137.0-138.0	1.6	1.1	96.4	.9	4.3a	2.6	
138.0-139.0	1.1	1.2	97.0	.7	2.8a	2.9	
139.0-140.0	.6	.9	97.4	1.1	1.5a	2.2	
140.0-141.0	. 8	1.0	97.4	.8	2.1a	2.4	
141.0-142.0	.5	1.2	97.7	.6	1.4a	2.9	
142.0-143.0	.3	1.5	97.8	.4	.7a		
143.0-144.0	.8	1.0	97.7	.5		3.6	
144.0-145.0	.1	1.4	98.0	.5	2.la .4a		
145.0-146.0	.2		97.9			3.4	
146.0-147.0		1.0		.9	.5a	2.4	
147.0-148.0	-4	1.2	97.8	.6	1.la	2.9	
148.0-149.0	- 4	1.2	97.8	.6	1.1a	2.9	
149.0-150.0	. 3	1.1	97.4	1.2	.7a	2.6	
150.0-151.0	. 2	1.5	97.9	. 4	.5a	3.6	
151.0-152.0	. 2	1.6	97.7	.5	.5a	3.8	
152.0-153.0	. 3	1.5	97.8	. 4	.7a	3.6	
153.0-154.0	. 2	1.4	97.9	.5	.5a	3.4	
154.0-155.0	. 3	1.4	97.8	.5	. 8a	3.4	
155.0-156.0	. 2	1.5	97.7	.6	.6a	3.6	
	.1	1.5	97.9	.5	. 3a	3.6	
156.0-157.0	. 3	1.6	97.5	.6	.9a	3.8	
157.0-158.0	. 8	1.8	96.4	1.0	2.0a	4.3	
158.0-159.0	.9	1.7	96.7	.7	2.5a	4.1	
159.0-160.0	1.3	1.8	96.1	. 8	3.3a	4.3	
160.0-161.0	2.1	1.9	95.0	1.0	5.5	4.6	.905
161.0-162.0	2.4	2.4	94.1	1.1	6.4	5.8	.911
162.0-163.0	3.5	2.1	93.1	1.3	9.4	5.0	.901
163.0-164.0	1.1	1.6	96.3	1.0	2.9a	3.8	
164.0-165.0	.8	2.1	96.1	1.0	2.2a	5.0	
165.0-166.0	1.0	2.2	96.1	.7	2.6a	5.3	
166.0-167.0	. 7	1.6	96.3	1.4	1.9a	3.8	
167.0-168.0	1.6	1.8		.8	4.1a	4.3	
163.0-169.0	3.2	1.8	93.9	1.1	8.4	4.3	0.917
169.0-170.0	1.6	1.0	96.4	1.0	4.la	2.4	
170.0-171.0	2.4	1.7	94.2	1.7	6.3	4.1	.920
171.0-172.0	1.6	2.0	95.5	.9	4.2a	4.8	
172.0-173.0	1.3	1.9	95.8	1.0	3.4a	4.6	
173.0-174.0	1.5	2.2	95.5	.8	3.9a	5.3	
174.0-175.0	1.4	2.0	95.7	.9	3.6a	4.8	
175.0-176.0	2.8	2.1	93.9	1.2	7.3	5.0	.913
176.0-177.0	2.6	1.6	95.0	.8	6.8	3.8	.918
177.0-178.0	1.6	1.3	96.3	.3	4.1a	3.1	
178.0-179.0	.6	1.3	97.5	.6	1.5a	3.1	
179.0-180.0	1.2	1.2	96.9	.7	3.1a	2.9	
180.0-181.0	1.2	1.2	96.8	. 8	3.3a	2.9	
181.0-132.0	1.3	1.6	96.3	.9	3.4a	3.6	

NAME AND ADDRESS OF PERSONS ASSESSED.

Samples from the Leological Minese's decements

			die.	

Samples from the U.S. Geological Survey's Corehole 78-3 (Continued)

			Yield	of proc	duct		5-15-
		Weight	percent		Gal pe	T TOD	Specific
Depth			Spent	Gas -		-1 5011	gravity
From To	011	Water	shale	loss	011-/	Water	of oil at 60°/60° F
182.0-183.0	2.1	1 5	05 (0			
183.0-184.0	1.5	1.5	95.6	. 8	5.4	3.6	.910
184.0-185.0	.1	1.4	96.4 95.5	. 7	4.0a	3.4	
185.0-186.0	.6	4.1	94.9	.4	. 3a	9.6	
186.0-187.0	1.6	2.5		. 4	1.6a	9.3	
187.0-188.0	1.7	1.5	94.5	1.4	4.1a	6.0	
188.0-189.0	1.3	1.4		.8	4.5a	3.6	
189.0-190.0	.4		96.7	.6	3.5a	3.4	
190.0-191.0	. 8	1.5	97.4	. 7	1.1a	3.6	
191.0-192.0	. 4	1.7	97.0	.5	2.2a	4.1	
192.0-193.0	1.3	1.8	97.2	.6	1.2a	4.3	
		1.5	96.6	.6	3.3a	3.6	
193.0-194.0	0.4	1.2	97.7	0.7	1.0a	2.9	
194.0-195.0	. 4	1.6	97.6	.4	1.la	3.8	
195.0-196.0	.7	1.5	97.2	.6	1.8a	3.6	
196.0-197.0	.5	1.0	97.3	1.2	1.4a	2.4	
197.0-198.0	1.1	1.4	97.0	.5	2.9a	3.4	
198.0-199.0	.9	1.5	97.1	.5	2.3a	3.6	
199.0-200.0	.8	1.5	97.1	.6	2.1a	3.6	
200.0-201.0	.9	1.3	97.4	.4	2.3a	3.1	
201.0-202.0	1.1	1.7	96.5	. 7	2.9a	4.1	
202.0-203.0	1.0	1.7	96.9	. 4	2.6a	4.1	
203.0-204.0	. 3	1.6	97.6	.5	.8a	3.8	
204.0-205.0	1.0	1.9	96.7	- 4	2.5a	4.6	
205.0-206.0	1.2	1.8	96.1	.9	3.1a	4.3	
206.0-207.0	1.9	2.5	94.5	1.1	4.9a	6.0	
207.0-208.0	1.2	3.0	95.1	. 7	3.1a	7.2	
208.0-209.0	.6	3.0	95.6	. 8	1.5a	7.2	
209.0-210.0	- 4	2.8	96.3	.5	1.1a	6.7	
210.0-211.0	.1	2.7	96.6	.6	.4a	6.5	
211.0-212.0	. 2	2.8	96.3	. 7	.5a	6.7	
212.0-213.0	. 2	2.7	96.7	.4	.4a	6.5	
213.0-214.0	.1	2.3	97.2	.4	.4a	5.5	
214.0-215.0	.0	1.2	97.8	1.0	Trace	3.0	
215.0-216.0	.2	2.7	96.7	. 4	.5a	6.5	
216.0-217.0	.1	1.7	97.8	.4	.2a	4.1	
217.0-218.0	. 2	1.5	97.6	. 7	.5a	3.6	
218.0-219.0	.1	1.1	98.0	.8	.4a	2.6	
219.0-220.0	.2	1.9	97.3	.6	.6a	4.6	
220.0-221.0	.0	1.5	98.0	.5	Trace	3.6	
221.0-222.0	.1	1.9	97.6	. 4	. 3a	4.6	
222.0-223.0	.1	1.8	97.8	.3	. 3a	4.3	

Designation of the Particular of Particular Printers and Particular Printers and Particular Particu

Samples from the U.S. organic to the Surpey's Coresents

Samples from the U.S. Geological Survey's Corehole 78-3 (Continued)

			Yield	of pro	duct		
		Weight	percent	or prot	The second liverage and the se	er ton	Specific
Depth			Spent	Gas 4		er rou	gravity
From To	011	Water	shale	loss	011-/	Water.	of oil at 60°/60° F
						MILETI	00 / ft() F
223.0-224.0	0.2	1.6	97.8	0.4	0.6a	3.8	
224.0-225.0	. 3	1.4	97.8	.5	.8a	3.4	
225.0-226.0	. 2	1.0	98.2	.6	.5a	2.4	
226.0-227.0	.1	1.0	98.4	.5	. 3a	2.4	
227.0-228.0	.2	.8	98.5	.5	.5a	1.9	
228.0-229.0	.3	1.3	97.9	.5	.7a	3.1	
229.0-230.0	.5	1.8	96.9	.8			
230.0-231.0	.6				1.4a	4.3	
231.0-232.0		1.0	97.9	.5	1.5a	2.4	
	.9	1.0	97.6	.5	2.2a	2.4	
232.0-233.0	.5	.9	98.0	.6	1.4a	2.2	
233.0-234.0	.4	.9	98.2	.5	1.1a	2.2	
234.0-235.0	.1	.5	98.6	. 8	. 2a	1.2	
235.0-236.0	. 3	.9	98.3	.5	.9a	2.2	
236.0-237.0	. 2	.9	98.3	.6	.6a	2.2	
237.0-238.0	. 3	1.0	98.3	. 4	.8a	2.4	
238.0-239.0	.3	.9	98.3	.5	.9a	2.2	
239.0-240.0	. 4	1.0	98.3	. 3	1.0a	2.4	
240.0-241.0	. 4	1.1	98.0	.5	1.la	2.6	
241.0-242.0	. 3	.9	98.0	. 8	.8a	2.2	
242.0-243.0	. 3	1.2	98.1	. 4	.7a	2.9	
243.0-244.0	. 4	1.2	98.0	.4	1.la	2.9	
244.0-245.0	. 2	.9	97.8	1.1	.5a	2.2	
245.0-246.0	. 2	1.3	98.1	.4	.4a	3.1	
246.0-247.0	.2	1.3	98.1	.4	.5a	3.1	
247.0-248.0	. 4	1.3	97.9	.4	1.0a	3.1	
248.0-249.0	. 4	1.4	97.7	.5	1.1a	3.4	
249.0-250.0	.5	1.3	97.8	. 4	1.2a	3.1	
250.0-251.0	.5	1.5	97.6	. 4	1.4a	3.6	
251.0-252.0	.6	1.3	97.7	.4	1.5a	3.1	
252.0-253.0	. 4	1.2	98.0	. 4	1.0a	2.9	
253.0-254.0	0.7	1.1	97.3	0.9	1.9a	2.6	
254.0-255.0	.7	1.3	97.2	.8	1.9a	3.1	
255.0-256.0	1.2	1.4	96.6	.8	3.la	3.4	
256.0-257.0	2.5	1.6	94.8	1.1	6.4	3.8	0.917
257.0-258.0	3.4	2.5	93.0	1.1	8.9	6.0	.923
258.0-259.0	2.9	2.1	93.8	1.2	7.5	5.0	
259.0-260.0	1.9	2.2	94.6	1.3			.913
	1.5	1.6	96.0		4.9a	5.3	
260.0-261.0	1.2	1.4		. 9	3.9a	3.8	
261.0-262.0	1.5		96.7	. 7	3.2a	3.4	
262.0-263.0		1.1	95.7	1.7	4.0a	2.6	000
263.0-264.0	4.9	1.9	91.7	1.5	13.0	4.6	.908
264.0-265.0	4.3	1.5	92.9	1.3	11.3	3.6	.905
265.0-266.0	3.0	1.5	94.1	1.4	8.1	3.6	.905
266.0-267.0	1.8	1.5	95.4	1.3	4.6a	3.6	
267.0-268.0	1.4	1.3	96.5	. 8	3.6a	3.1	
268.0-269.0	1.8	1.2	95.9	1.1	4.7a	2.9	
269.0-270.0	1.5	2.0	95.7	. 8	3.9a	4.8	

NAMED OF PERSONS NAMED AND PARTY ASSESSMENT OF PARTY ASSESSMENT OF

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Samples from the U.S. Geological Survey's Corehole 78-3 (Continued)

	-		Yield c	f produ	ct		Specific
Dept.	1 20 20	Weight	percent		Gal pe	r ton	gravity
Depth	FFREE		Spent	Gas +			of oil at
From To	011	Water	shale	loss	011-1/	Water	60°/60° F
270.0-271.0	2.3	2.1	94.6	1.0	6.0	5.0	.908
271.0-272.0	1.1	1.3	96.8	.8	3.0a	3.1	.,,,,
272.0-273.0	.8	1.0	97.8	.4	2.0a	2.4	
273.0-274.0	.8	1.0	97.4	. 8	2.2a	2.4	
274.0-275.0	.6	1.0	98.0	. 4	1.6a	2.4	
275.0-276.0	.2	1.1	98.3	. 4	.5a	2.6	
276.0-277.0	.3	2.2	97.1	. 4	.7a	5.3	
277.0-278.0	.3	1.1	98.1	.5	.8a	2.6	
278.0-279.0	.3	1.1	98.2	. 4	.9a	2.6	
279.0-280.0	.2	1.3	98.1	. 4	.6a	3.1	
280.0-281.0	. 2	1.3	98.0	.5	. 5a	3.1	
281.0-282.0	.2	1.2	98.2	. 4	.48	2.9	
282.0-283.0	.1	.9	98.3	. 7	. 3a	2.2	
283.0-284.0	0.4	1.3	97.8	0.5	1.0a	3.1	
284.0-285.0	.5	1.2	97.5	. 8	1.4a	2.9	
285.0-286.0	.4	1.2	97.8	. 6	1.1a	2.9	
286.0-287.0	.1	1.4	97.9	.6	. 3a	3.4	
287.0-288.0	.5	1.4	97.4	.7	1.3a	3.4	
288.0-289.0	. 3	1.5	97.6	.6	.7a	3.6	
289.0-290.0	.3	1.0	97.8	.9	. 8a	2.4	
290.0-291.0	.4	1.4	97.7	.5	1.0a	3.4	
291.0-292.0	.8	1.3	97.2	.7	2.1a	3.1	
292.0-293.0	5	1.0	97.6	.9	1.4a	2.4	
293.0-294.0	.8	1.2	97.4	.6	2.0a	2.9	
294.0-295.0	1.5	1.5	96.1	.9	4.0a	3.6	
295.0-296.0	1.4	1.5	96.3	.8	3.8a	3.6	
296.0-297.0	1.7	1.3	96.2	. 8	4.42	3.1	
297.0-298.0	1.4	1.4	96.3	. 9	3.8a	3.4	
298.0-299.0	.8	1.4	97.2	.6	2.0a	3.4	
299.0-300.0	1.0	1.4	96.9	.7	2.5a	3.4	
300.0-301.0	.8	1.2	97.3	.7	2.0a	2.9	
301.0-302.0	1.5	1.4	95.9	1.2	3.9a	3.4	
302.0-303.0	1.7.	1.5	96.0	.8	4.6a	3.6	

^{1/ &}quot;a"--indicates specific gravity estimated as 0.92.

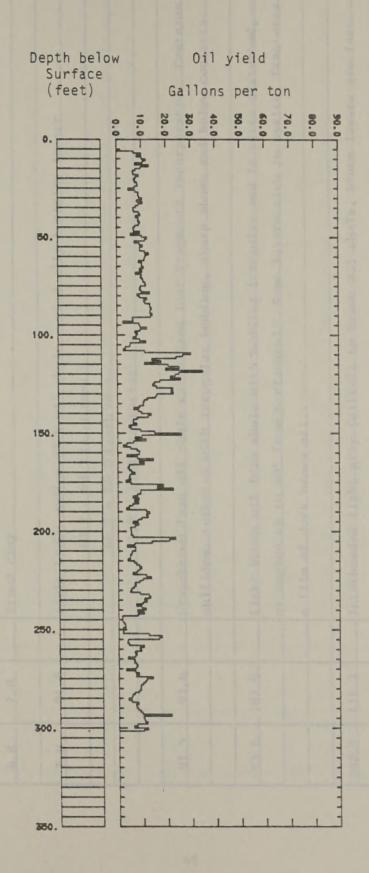
OIL-SHARE MILLY IN MONTH WHITE WATER STATES

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U.S. Geological Survey

Core hole 78-3A



FROM	TO	THICK- NESS	LITHOLOGIC DESCRIPTION
6.0	6.8		Gray-brown medium rich oil shale
6.8	7.0		Brown clay
7.0	91.5		Light brown medium rich oil shale - gradually becoming leaner 60.2 - 60.3 leach zone
			66.7 = 66.8 leach zone 71.0 = 75.0 fracturing
91.5	93.6		Gray-brown lean oil shale carbonized leaf fragments Incorporated. Contains from sulfides, turbated with irregular bedding, sharp above and below contacts.
93.6	107.9		Light brown oil lean shale with bedding irregular and in parts disturbed, commonly at angles up to 40° from horizontal. Some layers rich in pyrite, fractures have a film of dark brown oil.
107.9	131.3		Interhedded light gray (silty?) to brown oil shale, brown layers are lean. Bedding and contacts are irregular with common recumbant isoclinal folding less turbated toward bottom.
131.3	139.0		light brown lean oil shale, evenly and thinly bedded in most parts, some with contortion of layers. Darker brown layers rare and thin

FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION
139.0	140.1		Brown lean oil shale alternating with light brown and silty (?) layers thinly and evenly bedded, undisturbed.
140.1	147.8		Light gray brown lean oil shale with thin darker and silty beds. Bedding relatively undisturbed.
147.8	149.8		Brown layers alternating with tan and light brown layers. Bedding is uneven and somewhat disturbed. Brown layers are lean without oil film in fracture.
149.8	173.7		Light brown to gray lean oil shale, thinly to irregularly hedded beds dipping at angles up to \$\infty\$ 20°.
173.7	180.6	F	rown lean oil shale interbedded with white, tan, and tannish pink layers. Beds are irregular and disturbed with folding in parts.
BOTTOM	299.7 OF HOLE		Light gray brown lean oil shale thinly bedded with disturbed areas. Some light gray layers, some with pyrite, silty or dolomitic heds common. Darker brown ————————————————————————————————————

FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION		
			0.4' soft brown siltstone at 264.1-264.5, oll free. 0.3'	grayish brown	siltston
			at 0.7' dark brown to cream colored sillstone with minor 1		
			in upper part with solution pits of salts. Gray siltstone		
			of lean oll shale 0.3' at 280.1- 280.4.; 0.1' at 281.0-281		
			0.8' at 283.6 - 284.4. Gray siltstone interhedded and turb		
			oil shale from 292.0-294.4'.		
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OIL-SHALE ASSAYS BY MODIFIED FISCHER RETORT METHOD

Samples from the U.S. Geological Survey's Corchole 78-3Adrilled in sec. 26, T. 2 S., R. 95 W. Rio Blanco County, Colorado

			Viold a	·			
- 40,000,000		Weight	percent	of produ	Control of the Contro		Specific
Depth			Spent	Gas +	Gal pe	er ton	gravity
From To	Oil	Water	shale	loss	0111/	*11	of oil at
			BILLIATE	1055	011-	Water	60°/60° F
6.0-7.0	2.7	2.0	93.8	1.5	7.0	4.8	0.939
	4.0	2.0	92.9	1.1	10.2	4.8	.945
7.0-8.0	3.3	2.0	93.5	1.2	8.3	4.8	.945
8.0-9.0	4.1	1.8	93.0	1.1	10.3	4.3	.946
9.0-10.0	4.7	1.5	92.4	1.4	12.0	3.6	.948
10.0-11.0	4.2	1.2	93.4	1.2	10.7	2.9	.938
11.0-12.0	2.9	2.2	93.6	1.3	7.6	5.3	.925
12.0-13.0		1.7	91.8	1.4	13.2	4.1	.927
13.0-14.0	5.1		93.5	1.4	9.8	3.1	.934
14.0-15.0	3.8	1.3				2.6	
15.0-16.0	3.0	1.1	95.2	.7	7.7		.934
16.0-17.0	2.6	. 8	96.1	.5	6.6	1.9	.936 .
17.0-18.0	2.7	.9	95.9	.5	6.8	2.2	.935
13.0-19.0	3.6	2.1	93.2	1.1	9.1	5.0	.940
19.0-20.0	3.1	1.8	94.2	.9	7.8	4.3	.948
20.0-21.0	2.8	1.4	95.2	. 6	7.1	3.4	.943
21.0-22.0	3.0	1.6	94.8	.6	7.5	3.8	.942
22.0-23.0	3.3	1.5	94.2	1.0	8.4	3.6	.946
23.0-24.0	3.4	1.4	94.3	.9	8.6	3.4	.946
24.0-25.0	2.9	1.8	94.5	. 8	7.3	4.3	.947
25.0-26.0	. 1.8	1.4	96.1	.7	4.8a	3.4	.920
26.0-27.0	3.0	1.2	94.9	.9	7.6	2.9	.945
27.0-28.0	3.5	1.3	94.3	.9	8.9	3.1	.946
28.0-29.0	3.5	1.6	93.9	1.0	8.8	3.8	.946
29.0-30.0	3.6	1.6	93.8	1.0	9.2	3.8	.943
30.0-31.0	4.1	1.5	93.3	1.1	10.4	3.6	.942
31.0-32.0	3.2	1.2	94.6	1.0	8.2	2.9	.944
32.0-33.0	4.2	1.3	93.4	1.1	10.6	3.1	.943
33.0-34.0	3.5	1.8	93.5	1.2	8.8	4.3	.945
34.0-35.0	3.0	1.2	95.1	. 7	7.7	2.9	.943
35.0-36.0	2.6	1.1	95.5	8	6.7	2.6	.940
36.0-37.0	2.7	1.1	95.6	0.6	6.9	2.6	.939
37.0-38.0	3.6	1.5	93.7	1.2	9.1	3.6	.943
38.0-39.0	3.8		93.5	1.1	9.6	3.8	.942
39.0-40.0	3.1	1.5	94.6	8	7.8	3.6	.943
40.0-41.0	3.5	1.4	94.2	.9	8.9	3.4	.942
41.0-42.0	3.4	1.4	94.2	1.0	8.7	3.4	.941
42.0-43.0	. 3.7	1.2	94.2	.9	9.5	2.9	.944
43.0-44.0	3.5	1.5	94.2	. 8		. 3.6	.940
44.0-45.0	2.9	1.5	94.9	.7	7.4	3.6	.937
45.0-46.0	2.6	1.4	95.2	.8	6.7	3.4	.940
46.0-47.0	2.8	1.9	94.4	.9	7.0	4.6	.939
47.0-48.0	3.7	1.6	93.7	1.0	9.5	3.8	.942
1.8 0-1.9 0	2.2	1.4	95.6	. 8	5.7	3.4	.941
49.0-50.0	4.0	1.7	92.9	1.4.	10.2	4.1	.939
47.0 30.0							

THE PARTY NAMED IN TAXABLE PARTY OF PERSONS IN PERSONS

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WILL-SHALF ASSAYS BY MODITIED FISCHER RETORT MITHOD

Samples from the U.S. Geological Survey's Corehole 78-3A(Continued)

			Yaeld	of proc.	nc:		Specific
		Weigni	percent			er ton	gravity
Prom: To	011	Water	Spent	Cas +	0112/	Water	of oil at 60°/60° F
50.0-51.0	, 0	1					
51.0-52.0	4.9	1.6	92.2	1.3	12.4	3.8	.941
52.0-53.0	4.4	1.8	92.6	1.2	11.4	4.3	.937
53.0-54.0	2.8	1.5	94.8	.9	7.2	3.6	.927
	3.6	1.8	93.5	1.1	9.3	4.3	.920
54.0-55.0	4.1	1.7	93.0	1.2	10.6	. 4.1	.924
55.0-56.0	3.6	1.9	93.5	1.0	9.4	4.6	.919
56.0-57.0	3.6	1.8	93.6	1.0	9.4	4.3	.920
57.0-58.0	4.4	2.2	91.9	1.5	11.4	5.3	.919
58.0-59.0	5.0	1.8	91.8	1.4	13.1	4.3	.914
59.0-60.0	4.5	2.2	92.0	1.3	11.7	5.3	.914
60.0-61.0	4.3	2.1	92.2	1.4	11.4	5.0	.917
61.0-62.0	4.3	2.0	92.3	1.4	11.2	4.8	.920
62.0-63.0	3.4	1.5	94.2	.9	8.9	3.6	.917
63.0-64.0	4.0	1.4	93.4	1.2	10.3	3.4	.916
64.0-65.0	3.9	1.3	93.7	1.1	10.1	3.1	.916
65.0-66.0	4.2	1.5	93.2	1.1	10.9	3.6	.917
66.0-67.0	3.6	2.5	92.7	1.2	9.2	6.0	.924
67.0-68.0	4.0	2.1	92.2	1.7	10.3	5.0	.920
68.0-69.0	3.0	1.6	94.4	1.0	7.7	3.8	.923
69.0-70.0	3.9	1.9	92.9	1.3	10.1	. 4.6	.932
70.0-71.0	3.7	2.0	93.3	1.0	9.7	4.8	.928
71.0-72.0	4.1	1.8		1.1	10.5	4.3	.927
72.0-73.0	4.2	2.0	92.5	1.3	10.8	4.8	
73.0-74.0	4.5	1.9	92.3	1.3	11.5	4.6	.927.
74.0-75.0	4.6	1.8	92.3				.930
75.0-76.0	3.7			1.3	11.8	4.3	.927
76.0-77.0		2.2	93.0	1.1	9.6	5.3	.930
77.0-78.0	3.6	2.0	93.4	1.0	9.2	4.8	.925
78.0-79.0	3.8	1.9	93.2	1.1	9.9	4.6	.925
79.0-80.0	5.2	1.8	91.3	1.7	13.4	4.3	.926
80.0-81.0	3.2	2.0	93.7	1.1	8.3	4.8	.923
	3.5	2.1	93.1	1.3	9.2	5.0	.924
81.0-82.0	4.7	1.8	92.2	1.3	12.3	4.3	.925
82.0-83.0	4.2	1.8	92.7	1.3	10.9	4.3	.924
83.0-84.0	4.4		92.3	1.2	11.5	5.0	.924
84.0-85.0	5.2	2.0	91.6	1.2	13.5	4.8	.925
85.0-86.0	5.2	1.9	91.4	1.5	13.5	4.6	.926
86.0-87.0	5.4	1.6	91.4	1.6	14.1	3.8	.921
87.0-88.0	5.2	1.7	91.7	1.4	13.6	4.1	.919
88.0-89.0	5.2		91.9	1.4	13.5	3.6	.916
89.0-90.0	5.5		91.2	1.6	14.4		.919
90.0-91.0	5.3	1.1	92.3		13.7	2.6	.920
91.0-92.0	2.4	2.0	94.8		6.2	4.8	.925
92.0-93.0	2.5	2.3	94.0		6.6	5.5	.926
93.0-94.0	.9		96.9				
94.0-95.0	3.5	1.6			2.4a	3.8	.920
95.0-96.0		.6	94.7	1.2		1.4	.919
22.0 20.0	3.6	.7	94.0	1.7	9.4	1.7	.916

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OIL-SHALE ASSAYS BY MODIFIED PISCHER RETORT SECTION

Semples from the U.S. Geological Survey's Corehole 78-3A(Continued)

	-		Yanld a	of proc			
		Weight	percent	of proc		er ton	Specific gravity
Depth	.011	The same	Spent	Gas +			of oil at
דסת זם	0:1	Water	shale	1089	013-1/	Water.	60°/60° F
96.0-97.0	4.6	0.9	93.1	1.4	12.1	2.2	0.912
97.0-98.0	3.6	1.2	94.1	1.1	9.4	2.9	.919
98.0-99.0	2.8	. 9	95.5	. 8	7.3	2.2	.913
99.0-100.0	3.2	1.1	94.5	1.2	8.4	2.6	.919
100.0-101.0	3.0	1.2	94.9	.9	7.8	2.9	.924
101.0-102.0	2.5	1.2	95.5	. 8	6.5	2.9	.919
102.0-103.0	3.5	.7	94.8	1.0	9.3	1.7	.914
103.0-104.0	4.5	.6	93.5	1.4	11.7	1.4	.916
104.0-105.0	2.0	.9	96.4	.7	5.3	2.2	.919
105.0-106.0	2.0	.9	96.5	.6	5.2a	2.2	.920
106.0-107.0	1.3	1.1	97.1	.5	3.4a	2.6	.920
107.0-108.0	1.0	1.4	96.8	. 8	2.6a	3.4	.920
108.0-109.0	4.3	1.3	93.2	1.2	11.3	3.1	.916
109.0-110.0	11.5	2.1	83.6	2.8	30.1	5.0	.919
110.0-111.0	10.2	1.8	85.4	2.6	26.8	4.3	.915
111.0-112.0	9.2	1.9	86.7	2.2	24.0	4.6	.915
112.0-113.0	5.4	1.8	91.0	1.8	14.1	4.3	.923
113.0-114.0	6.9	1.6	89.3	2.2	18.0	3.8	.918
114.0-115.0	4.3	1.7	92.7	1.3	11.2	4.1	.919
115.0-116.0	. 8.0	1.6	88.5	1.9	20.8	3.8	.918
116.0-117.0	9.7	1.9	86.2	2.2	25.4	4.6	.915
117.0-118.0	7.5	1.5	89.3	1.7	19.7	3.6	.914
118.0-119.0	13.4	2.0	81.4	3.2	34.9	4.8	.917
119.0-120.0	9.6	1.6	86.2	2.6	25.1	3.8	.918
120.0-121.0	9.0	2.0	86.9	2.1	23.6	4.8	.915
121.0-122.0	8.3	2.0	87.6	2.1	21.6	4.8	.918
122.0-123.0	9.9	2.0	85.9	2.2	25.9	4.8	.913
123.0-124.0	6.6	2.0	89.9	1.5	17.3	4.8	.914
124.0-125.0	5.8	1.5	90.9	1.8	15.1	3.6	.919
125.0-126.0	5.5	1.6	91.7	1.2	14.5	3.8	.916
126.0-127.0	6.1	1.9	90.8	1.2	16.0	4.6	.918
127.0-128.0	8.7	2.0	86.8	2.5	22.7	4.8	.920
128.0-129.0	8.3	2.0		2.2	21.9	4.8	.912
129.0-130.0	8.7	1.8	87.2	2.3	22.8	4.3	.913
130.0-131.0	6.2	2.3	90.2	1.3	16.1	5.5	.923
131.0-132.0	6.0	2.1	90.1	1.8	15.6	5.0	
132.0-133.0	. 4.6	2.2	91.7	1.5	12.2		.915
133.0-134.0	4.2	2.0	92.6	1.2		5.3	.916
134.0-135.0	4.0	2.4	92.4	1.2		5.8	.917
135.0-136.0	4.1	1.8	93.0		10.5		.916
	3.5	2.1	92.9	1.1	10.7	4.3	.919
136.0-137.0	2.6	2.5		1.5	9.0	5.0	.923
137.0-138.0	3.3		94.0	.9	6.7	6.0	.923
138.0-139.0		1.6	94.1	1.0	8.6	3.8	.927
139.0-140.0	3.8	1.6	93.5	1.1.	9.8	3.8	.926

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WILL-SHALF, ASSAYS BY MODITIED FISCHER RETORT SETTIOD

Samples from the U.S. Geological Survey's Corehole 78-3A (Continued)

			¥101d	2/ 2222			
	-	Weight	percent	of proc			Specific
Depth			Spent	Gas 4		er ton	gravity
דר ייסד דס	011	Water	shale	loss	013-1/	Water.	of oil at
140.0-141.0			Timber 1				
	5.2	2.1	91.2	1.5	13.7	5.0	.918
141.0-142.0	4.8	2.0	91.8	1.4	12.5	4.8	.920
	3.1	2.1	93.4	1.4	8.0	5.0	.924
143.0-144.0	2.5	.9	95.4	1.2	6.5	2.2	.917
144.0-145.0	2.4	1.4	95.4	. 8	6.3	. 3.4	.920
145.0-146.0	3.0	2.3	93.6	1.1	7.8	5.5	.924
146.0-147.0	1.8	1.5	96.2	.5	4.6a	3.6	.920
147.0-148.0	2.1	1.4	95.8	.7	5.5	3.4	.922
148.0-149.0	3.6	1.6	93.5	1.3	9.4	3.8	.923
149.0-150.0	5.8	2.3	90.3	1.6	15.1	5.5	.923
150.0-151.0	9.9	1.7	86.2	2.2	26.1	4.1	.910
151.0-152.0	3.8	2.3	92.8	1.1	9.9	5.5	.919
152.0-153.0	2.7	2.6	93.8	.9	7.0	6.2	.921
153.0-154.0	4.4	2.9	91.3	1.4	11.6	7.0	.916
154.0-155.0	2.5	2.1	94.6	. 8	6.5	5.0	.922
155.0-156.0	1.4	1.8	96.2	.6	3.7a	4.3	.920
156.0-157.0	0.9	1.5	97.2	0.4	2.3a	3.6	.920
157.0-158.0	2.0	1.9	95.4	.7	5.3	4.6	.922
158.0-159.0	3.0	2.7	92.9	1.4	7.9	6.5	.922
159.0-160.0	3.4	2.2	93.3	1.1		5.3	.923
160.0-161.0	3.4	2.2	93.2	1.2	8.8	5.3	.923
161.0-162.0	1.4	1.1	96.7	. 8	3.7a	2.6	.920
162.0-163.0	3.1	1.8	94.1	1.0	8.1	4.3	. 927
163.0-164.0	5.6	2.1	89.9	2.4	14.5	5.0	.926
164.0-165.0	3.3	2.4	93.0	1.3	8.7	5.8	.919
165.0-166.0	4.1	2.0	92.7	1.2	10.8	4.8	
166.0-167.0	1.8	2.3	95.4	.5	4.7a	5.5	.916
167.0-168.0	1.6	2.1	95.6	.7			.920
168.0-169.0	1.8	1.8	95.7	.7	4.1a	5.0	.920
169.0-170.0	2.2	1.9	95.2		4.7a	4.3	. 920
170.0-171.0	2.6	2.6	93.8	. 7	5.6	4.6	.917
171.0-172.0	1.9	2.0		1.0	6.9	6.2	.916
172.0-173.0	1.7		95.4	.7	4.9a	4.8	.920
173.0-174.0	2.0	1.9	95.2	1.2	4.5a	4.6	.920
174.0-175.0		2.3	94.8	.9	5.2a	5.5	.920
175.0-176.0	1.3	1.6	96.3	. 8	3.3a	3.8	. 920
176.0-177.0	2.0	1.9	95.5	.6	5.3	4.6	.916
		. 2.4	88.7	1.8	18.7	5.8	.916
177.0-178.0	6.1	2.0	90.7	1.2	16.0	4.8	.913
178.0-179.0	8.6	3.3	86.0	2.1	22.6	7.9	.916
179.0-180.0	3.5	2.2	93.1	1.2	9.2	5.3	.921
180.0-181.0	3.6	2.2	93.1	1.1.	9.3	5.3	.922
181.0-182.0	3.0	2.4	93.5	1.1	7.9	5.8	.921
182.0-183.0	2.4	2.7	94.1	.8	6.1	6.5	.919.
183.0-184.0	3.3	2.6	93.0	1.1	8.5	6.2	:916
184.0-185.0	2.6	1.9	94.7	. 8	6.7	4.6	.918
185.0-186.0	3.2	2.0	93.7	1.1	8.4	4.8	.914

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Oll-Shalf ASSAYS BY MODIFIED FISCHER RETORT MITHOD Samples from the U.S. Geological Survey's Corehole

. 78-3A (Continued)

			Yield o	of prod	uct		Specific
230.0-311.0		Meignt	percent		Gal pe	T ton	gravity
Pepth From To	0:1	11	Spent	Gas +			of oil at
10	0:1	Water	shale	loss	013-1/	Water.	60°/60° F
186.0-187.0	2.3	1.9	95.2	0.6	5.9	4.6	0.920
187.0-188.0	1.7	1.6	95.9	. 8	4.5a	3.8	.920
188.0-189.0	1.3	1.5	96.6	.6	3.4a	3.6	.920
189.0-190.0	4.4	1.5	92.8	1.3	11.6	3.6	.915
190.0-191.0	5.0	2.1	91.4	1.5	12.9	5.0	.924
191.0-192.0	4.5	2.2 .		1.4	11.6	5.3	.925
192.0-193.0	4.7	2.2	91.9	1.2	12.2	5.3	
193.0-194.0	3.7	2.0	93.2	1.1	.9.6	4.8	.927
194.0-195.0	3.2	2.0	,93.9	.9.	8.1		.930
195.0-196.0	2.3	2.4	94.4	.9		4.8	.934
196.0-197.0	3.3	2.2	93.3	1.2	6.0	5.8	.933
197.0-198.0	2.7	2.0	94.8		8.4	5.3	.938
198.0-199.0	1.9	1.8	95.7	.5	6.8	4.8	.937
199.0-200.0	2.1	1.9		.6	5.0a	4.3	.920
200.0-201.0	2.1	2.1	95.5	.5	5.3	4.6	.935
			95.0	. 8	5.4	5.0	.931
201.0-202.0 202.0-203.0	2.1	2.3	94.9	. 7	5.3	5.5	.929
	2.3	2.0	95.0	. 7	6.1	4.8	.926
203.0-204.0	9.0	2.5	86.4	2.1	23.5	6.0	.921
204.0-205.0	8.1	2.2	87.8	1.9	20.9	5.3	.929
205.0-206.0	5.4	1.9	91.5	1.2	13.8	4.6	.934
206.0-207.0	2.6	2.0	94.7	.7	6.7	4.8	.930
207.0-208.0	1.4	1.3	96.3	1.0	3.6a	3.1	.920
208.0-209.0	2.7	1.3	95.2	.8	7.0	3.1	.928
209.0-210.0	2.7	1.0	94.9	1.4	7.0	2.4	.934
210.0-211.0	2.2	1.6	95.6	.6 .	5.6	3.8	.931
211.0-212.0	2.1	1.6	95.7	.6	5.4	3.8	.930
212.0-213.0	1.9	1.7	95.8	.6	4.8a	4.1	. 920
213.0-214.0	1.9	1.5	96.0	.6	4.8a	3.6	.920
214.0-215.0	1.5	1.9	96.0	.6	3.9a	4.6	.920
215.0-216.0	2.5	1.7	95.1	.7	6.5	4.1	.927
216.0-217.0	2.8	1.9	94.5	0.8	7.4	4.6	0.920
217.0-218.0	3.3	2.2	93.5	1.0	8.6	5.3	.915
218.0-219.0	3.6	2.2	92.4	1.8	9.5	5.3	.915
219.0-220.0	3.3	2.9	92.7	1.1		7.0	.914
220.0-221.0	3.0	1.9	94.4	. 7	7.7	4.6	.921
221.0-222.0	2.2	2.3		. 7	5.9	5.5	.919
222.0-223.0	4.4	2.5	91.8	1.3	11.5	6.0	.917
223.0-224.0	5.2	2.1	91.5	1.2	13.5	5.0	.929
224.0-225.0	4.0	1.8	,93.2	1.0.	10.2	4.3	.934
225.0-226.0	3.4	1.7	93.8	1.1	8.7	4.1	.931
226.0-227.0	2.6	1.8	94.9	. 7	6.7	4.3	.932
227.0-228.0	2.8	2.1	94.6	. 5	7.1	5.0	.935
228.0-229.0	2.4	1.9	95.2	.5	6.3	4.6	.932
229.0-230.0	2.1	1.6	95.7	. 6	5.3	3.8	.932

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215.0-215.0				

OIL-SHALE ASSAYS BY MODITIED FISCHER RETORT METHOD

Samples from the U.S. Geological Survey's Corehole 78-3A (Continued)

			Yzeld c	of proc.	4CI		Specific
		Weagnt	percent		Gus 3 91	er ton	gravity
Depth			Spent	Cas +			of oil at
From To	011	Water	shale	loss	0131/	Water.	60°/60° F
230.0-231.0	1.9	1.3	96.3	E			State Line
231.0-232.0	3.4	1.5	94.6	.5	4.9a	3.1	.920
	4.8			.5	8.8	3.6	.925
232.0-233.0		1.8	92.2	1.2	12.5	4.3	.925
233.0-234.0	5.1	2.3	91.3	1.3	13.1	5.5	.931
234.0-235.0	4.1	2.0	92.7	1.2	10.7	4.8	.929
235.0-236.0	4.6	2.1	92.2	1.1	11.7	5.0	.936
236.0-237.0	3.9	2.2	92.4	1.5	10.0	5.3	.938
237.0-238.0	2.9	2.3	93.9	.9	7.3	5.5	.930
238.0-239.0	3.7	2.8	92.6	.9	9.5	6.7	.929
239.0-240.0	4.3	1.7	92.9	1.1	11.2	4.1	.922
240.0-241.0	3.0	1.7	94.6	.7 .	7.7	4.1	.919
241.0-242.0	4.0	1.1	93.7	1.2	10.5	2.6	.914
242.0-243.0	3.0	1.2	94.8	1.0	7.9	2.9	.917
243.0-244.0	.6	.9	97.9	.6	1.6a	2.2	.926
244.0-245.0	.6	.9	98.1	.4	1.6a	2.2	.920
245.0-246.0	.6	1.1	97.5	.8	1.6a	2.6	.920
246.0-247.0	0.9	1.1	97.6	0.4	2.2a	2.6	.920
247.0-248.0	1.0	1.1	97.5	.4	2.7a	2.6	.920
248.0-249.0	1.1	1.2	97.2	.5	2.9a	2.9	. 920
249.0-250.0	.7	1.2	97.7	4	1.8a	2.9	.920
250.0-251.0	.8	1.2	97.6	.4	2.0a	2.9	.920
	. 7	1.2	97.7	.4	1.8a	2.9	.920
251.0-252.0			92.9		12.5	2.4	0.921
252.0-253.0	- 4.8	1.0		1.3			.921
253.0-254.0	6.8	2.9	88.6	1.7	17.7	7.0	
254.0-255.0	6.4	2.4	89.4	1.8	16.5	5.8	.924
255.0-256.0	1.5	1.5	96.1	.9	3.8a	3.6	.920
256.0-257.0	1.4	1.9	96.0	.7	3.6a	4.6	.920
257.0-258.0	1.6	1.1	96.1	1.2	4.2a	2.6	.920
258.0-259.0	4.0	2.0	92.8	1.2	10.4	4.8	.929
259.0-260.0	3.3	1.7	94.0	1.0	8.6	4.1	.926
260.0-261.0	3.6	1.2	94.2	1.0	9.3	2.9	.924
261.0-262.0	2.6	1.3	95.4	. 7	6.7	3.1	.923
262.0-263.0	2.8	1.2	95.2	.8		2.9	.923
263.0-264.0	2.6	1.1	95.6	.7	6.8	2.6	.923
264.0-265.0	1.5	1.3	96.6	.6	3.8a		.920
265.0-266.0	2.6	2.1	94.3	1.0	6.6	5.0	.935
266.0-267.0	2.4		94.5	.6	6.3	6.0	.930
267.0-268.0	2.8	1.6	94.9	.7	7.2	3.8	.932
268.0-269.0	3.0	1.4	95.0	.6	7.7	3.4	.930
269.0-270.0	2.8	1.2	95.4	.6	7.1	2.9	.929
270.0-271.0	1.2	1.4	97.0	.4	3.0a	3.4	.920
271.0-272.0	2.6	2.2	94.6	.6	6.8	5.3	.930
272.0-273.0	3.2	2.5	93.5	. 8	8.3	6.0	.929
273.0-274.0	2.8	1.8	94.8	.6	7.1	4.3	.930
274.0-275.0	5.4	2.4	90.9	1.3	14.0	5.8	.933
275.0-276.0	4.4	2.4	92.2	1.0	11.4	5.8	.931

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Oll-SHALE ASSAYS BY MODIFIED FISCHER RETORT METHOD Semples from the U.S. Geological Survey's Corehole 78-3A (Continued)

1 Wat .3 19 15 15 15 2.	3 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	93.3 93.6 94.3 94.6 94.4	1.1 1.3 .9 .9	013 ¹ / 10.9 10.0 9.1 8.9 9.0	3.1 2.9 3.1 2.4	Specific gravity of oil at 60°/60° y 0.934 .936 .937 .937
1 Wat .3 19 15 15 15 2.	3 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	93.3 93.6 94.3 94.6	1.1 1.3 .9 .9	10.9 10.0 9.1 8.9	3.1 2.9 3.1 2.4	of oil at 60°/60° F 0.934 .936 .937
.3 1. .9 1. .5 1. .5 1. .5 1. .5 2 1.	3 9 2 9 3 0 9 1 9	93.3 93.6 94.3 94.6	1.1 1.3 .9	10.9 10.0 9.1 8.9	3.1 2.9 3.1 2.4	0.934 .936 .937
.9 1. .5 1. .5 1. .5 1. .2 1.	2 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	93.6 94.3 94.6 94.4	1.3	10.0 9.1 8.9	2.9 3.1 2.4	.936
.9 1. .5 1. .5 1. .5 1. .2 1.	2 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	93.6 94.3 94.6 94.4	1.3	10.0 9.1 8.9	2.9 3.1 2.4	.936
.5 1. .5 1. .5 1. .2 1. .5 2.	3 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	94.3 94.6 94.4	.9	9.1	3.1	.937
.5 1. .5 1. .2 1. .5 2.	1 9	94.6	.9	8.9	2.4	
.5 1. .2 1. .5 2.	2 . 9	94.4				.937
. 2 1. . 5 2.	2 . 9		1.0	9 0		
.5 2.		94.8		7.0	2.6	.941
	0	700	. 8	8.2	2.9	.938
	0 .	94.8	.7	6.4	4.8	. 937
.2 2.	7 9	94.2	.9	. 5.5	6.5	.941
.1 1.	3 .	96.2	.4	5.3		.930
.5 2.						.920
.1 2.	4	94.9				.935
						.928
						.924
						.924
						.925
						.927
						.932
						.932
						.939
						.940
						.936
						.936
						.940
						.936
						.939
						.940
	.1 15 21 21 .784 189 31 32 26 29 14 1.	1 1.3 .9 .1 .7 .7 .5 .8 .6 .1 .7 .4 1.1 .8 .9 .4 2.2 .9 3.7 .1 3.2 .2 2.7 .6 2.0 .9 1.5 .4 1.5 .7 1.6	1 1.3 .96.2 .5 2.8 95.2 .1 2.4 94.9 .1 .7 95.6 .7 .5 96.0 .8 .6 95.9 .1 .7 95.3 .4 1.1 94.8 .8 .9 94.3 .4 2.2 87.5 .9 3.7 91.4 .1 3.2 91.8 .2 2.7 92.2 .6 2.0 92.3 .9 1.5 95.0 .4 1.5 95.6 .7 1.6 92.7	.1 1.3 .96.2 .4 .5 2.8 .95.2 .5 .1 2.4 .94.9 .6 .1 .7 .95.6 .6 .7 .5 .96.0 .8 .8 .6 .95.9 .7 .1 .7 .95.3 .9 .4 1.1 .94.8 .7 .8 .9 .94.3 1.0 .4 2.2 .87.5 1.9 .9 3.7 .91.4 1.0 .1 3.2 .91.8 .9 .2 2.7 .92.2 .9 .6 2.0 .92.3 1.1 .9 1.5 .95.6 .5 .7 1.6 .92.7 1.0	.1 1.3 .96.2 .4 5.3 .5 2.8 .95.2 .5 3.9a .1 2.4 .94.9 .6 5.3 .1 .7 .95.6 .6 8.0 .7 .5 .96.0 .8 7.0 .8 .6 .95.9 .7 7.3 .1 .7 .95.3 .9 7.9 .4 1.1 .94.8 .7 8.9 .8 .9 .94.3 1.0 .9.7 .4 2.2 .87.5 1.9 21.5 .9 3.7 .91.4 1.0 9.9 .1 3.2 .91.8 .9 10.4 .2 2.7 .92.2 .9 10.7 .6 2.0 .92.3 1.1 11.7 .9 1.5 .95.6 .5 6.1 .7 1.6 92.7 1.0 11.9	.1 1.3 .96.2 .4 5.3 3.1 .5 2.8 .95.2 .5 3.9a 6.7 .1 2.4 .94.9 .6 5.3 5.8 .1 .7 .95.6 .6 8.0 1.7 .7 .5 .96.0 .8 7.0 1.2 .8 .6 .95.9 .7 7.3 1.4 .1 .7 .95.3 .9 7.9 1.7 .4 1.1 .94.8 .7 8.9 2.6 .8 .9 .94.3 1.0 9.7 2.2 .4 2.2 87.5 1.9 21.5 5.3 .9 3.7 .91.4 1.0 9.9 8.9 .1 3.2 .91.8 .9 10.4 7.7 .2 2.7 .92.2 .9 10.7 6.5 .6 2.0 92.3 1.1 11.7 4.8 .9 1.5 95.6 .5 6.1 3.6 .7 1

^{1/ &}quot;a"-indicates specific gravity estimated as 0.92.

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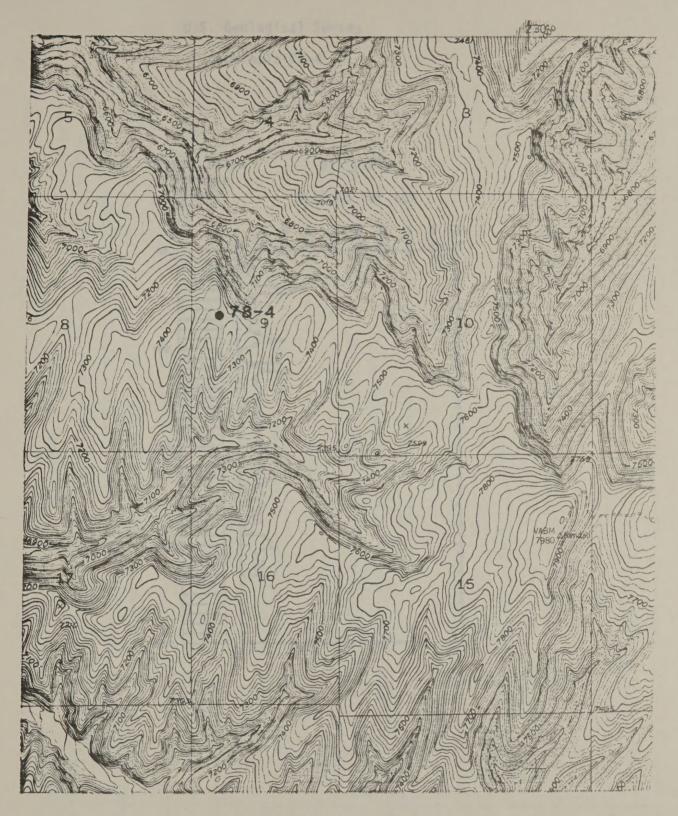
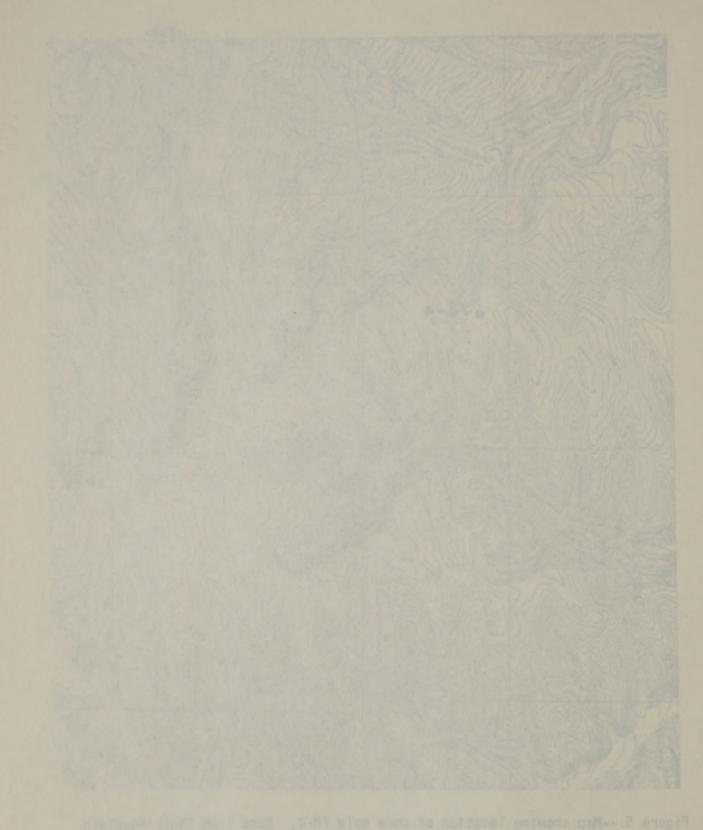


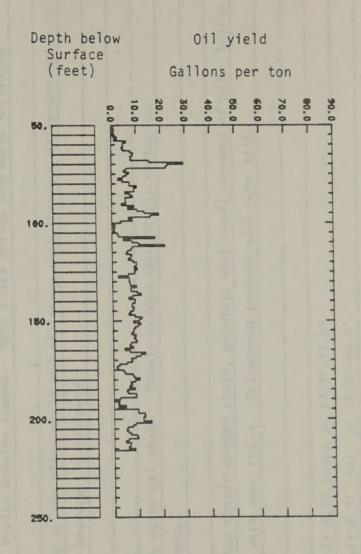
Figure 5.--Map showing location of core hole 78-4. Base from Segar Mountain Quadrangle (1952). Scale 1:24,000.



"Squre 5.--Map showing location of core note 78-4. Essa 104 Squr Fourteen Quadrangle (1952). Scale 1:21.000

U.S. Geological Survey

Core hole 78-4



0.0

FROM	то	THICK-	LITHOLOGIC DESCRIPTION
20.0'	50.5'	111033	Gray to oxidized yellow brown fine to coarse grained sandstone and siltstone
20.0	30.3		Interbedded with minor silty shale. Calcite cemented with disturbed, Irregular
			bedding. Pyrite nodules common. Most parts porous and water saturated.
			The state of the s
50.5'	69.1'		Light-gray to tan silty shale and siltstone with thin but irregular and
50.5	109.1		disturbed bedding. Calcareous.
			distance bedding. Outwiese
60.11	71.9'		Brown lean silty oil shale. Thinly bedded with little turbation.
69.1'	71.9		Noncalcareous.
			Noncal careous.
			Brown to tan thinly bedded shale, possibly with small amounts of oil. Little
71.9'	106.2'		
			turbation with some tuffs. Calcareous perhaps with some silt.
			Tuff 0.2' thick at 77.7'-77.9'
			Tuff 0.2' thick at 85.8'-86.0'
			Tuff 0.6' thick at 88.7'-89.3' with minor shale
			Tuff 0.25' thick at 90.5'-90.75' with minor shale
			Dark brown bed without smell of oil, otherwise similar to rest of this unit,
			93.7'-97.0', 3.3' thick.
			Tuff 0.1' thick at 96.7'
			Tuff 0.1' thick at 100.1'
		-	

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FROM	TO	THICK- NESS	LITHOLOGIC DESCRIPTION
		14633	Fine-grained calcite cemented sandstone 0.4' thick at 102.8'-103.2'
			with crossbedding
			With Crossbeduing
-			Brown to dark-brown oll shale, lean and somewhat calcareous. Thinly bedded
106.2'	220.0		with little turbation. Somewhat silty in parts. Carbonized plant impressions
			common.
			Dark-brown moderately lean oil shale 0.4' thick at 107.5'-197.9'
			Dark-brown moderately lean oil shale 0.7' thick at 111.2'-111.9'
			Well sorted gray siltstone 0.3' thick at 121.1'-121.4'
			gray siltstone 0.3' thick at 122.1'-122.4'
			Sandstone and gray siltstone 0.6' thick at 127.4'-128.0'
			Sandstone and gray siltstone 1.1' thick at 137.3'-138.4' with some shale
			Sandstone and gray siltstone 0.1' thick at 139.3'
	1		Sandstone and gray slitstone 0.3' thick at 154.1'-154.4' with some shale
			Sandstone and gray slitstone 0.2' thick at 156.2'-156.4'
			Sandstone and gray siltstone 0.4' thick at 161.7'-162.1' with some shale
			White siltstone 0.1' thick at 162.8'
	-		Gray siltstone 0.1' thick at 164.5'
-			Sandstone 0.1' thick at 171.1'
			Tuff 0.1' thick at 172.2'
			Unit of sandstone, gray and coarse grained with shale beds and parts with shale
			chips. Calcite cemented with most parts porous and water saturated with others
			massive 6.1' thick at 188.7'-194.8'

OIL-SHALE ASSAYS BY MODIFIED FISCHER RETORT HETHON

Samples from the U.S. Geological Survey's Corchole 78-4 drilled in sec. 9, T 18., R. 95W., Rio Blanco County, Lolorado

		-			Gall In			
			Weight	Yield	of prod			Specific
Dep	th		mergat	percent Spens		Gal p	er ton	ETOVITY
From	To	Oil	Water	shale	loss +	013	13	of oil at
					2087	011	Water	60°/60° F
50 51 52 53 54	51 52 53 54 55		•	97.5 97.6 97.6 96.4 96.6	0.4	TRACE 0.92 1.2 0.96 TRACE	5.0 3.7 3.9 5.8 6.1	.920 * .920 * .920 *
55 56 57 58 59	56 57 58 59 60	*		97.4 96.5 97.7 93.9 94.9	0.2 0.4 0.2 0.6 0.3	1.0 2.3 1.2 6.1 4.7	L.7 5.8 4.1 7.6 7.3	.920 * .920 * .920 * .916 .908
60 61 62 63 64	61 52 63 64 65			94.7 95.5 95.0 92.4 92.1	0.6 0.5 0.4 1.5	4.9 4.2 4.7 7.7 8.9	6.9 5.9 6.6 7.7 7.5	.920 * .900 .920 * .900 .903
65 66 67 68 69	66 67 68 69 70			92.1 94.1 94.1 90.2 80.8	1.5 0.8 0.8 1.3 5.6	8.6 7.8 7.9 15.4 29.4	7.7 4.9 5.0 6.5 5.8	.912 .915 .914 .907
70 71 72 73 74	71 72 73 74 75			85.9 86.2 95.1 94.8 94.3	2.6 2.4 0.8 1.2 0.8	22.9 22.1 6.0 5.0 7.1	6.3 6.3 4.4 4.9 5.0	.925 .946 .926 .926
75 76 77 78 79	76 77 78 79 80			94.6 95.3 96.4 95.7 93.8	1.0 1.0 0.7 0.8 1.4	6.0 4.7 2.7 4.4 7.3	5.1 4.4 4.5 4.8	.913 .914 .920 * .905

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OIL-SHALE ASSAYS BY MODIFIED FISCHER RETORT MUTHOD

Samples from the U.S. Geological Survey's Corehole 78-4 (Continued)

. 40 .

	Depth	No. of Concession, Name of			of procu	ci		Specific
De	nth	-	Weight	percent		Gal pe	r ton	gravity
From	To	011	Water	Spent	Cas +	Oil	**	of oil at
	1913			0.1012	1055	011	Water.	60.190. E
80 81 82 83 84	81 82 83 85 85			94.1 93.7 92.9 92.5 93.8	1.2 0.4 1.1 1.7	7.3 10.2 9.1 9.2 5.5	4.5 4.8 6.0 5.5 6.9	.919 .913 .922 .918 .916
85 86 87 88 89	86 87 88 89 90			92.4 93.1 93.5 93.4 93.1	1.4 1.2 1.2 1.0	7.5 8.5 5.5 5.6 5.8	7.8 5.7 7.6 8.2 8.3	.918 .948 .920 .928 .935
90 91 92 93 94	91 92 93 945			94.1 92.8 93.0 91.9 88.3	0.9	4.0 9.1 6.6 10.5 13.2	8.4 5.5 6.3 6.4 7.7	.925 .914 .923 .912 .923
95 96 97 98 99	96 97 98 99 100			86.8 87.3 95.4 94.7 96.4	2.6 2.9 0.7 0.5 0.6	19.2 15.7 6.7 8.3 3.6	7.8 9.1 3.2 3.8 3.8	.919 .917 .908 .902 .920 *
100 101 102 103 104	101 102 103 104 105			98.9 97.9 98.3 98.0 97.5	0.1 0.2 0.1 0.3 0.1	0.8 1.3 0.8 1.1 0.9	3.4 3.5 3.2 5.0	.920 * .920 * .920 * .920 * .920 *
105 106 107 108 109	106 107 108 109 110			96.6 96.3 89.5 94.1 92.8	0.5 Q.1 1.5 1.6 1.3	2.2 2.6 17.6 4.6 8.1	5.0 5.4 5.6 6.1 6.6	.920 * .920 * .914 .920 *
110 111 112 113 114	111 112 113 114 115			91.5 86.6 93.2 93.6 95.8	1.1 2.0 1.1 1.1 ••.1	10.8 21.5 8.2 7.7 6.3	7.6 7.6 6.0 5.7 4.5	.928 .917 .922 .917

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OIL-SHALE ASSAYS BY MODILIED FISCHER RETORT MITHOD Samples from the U.S. Geological Survey's Corehole 78-4 (Continued)

				Yzelo	o! procus	1		Secretaria
		Sireman	height	percent		Gel pe	rion	apecific gravity
Prom	To	0:1	Water	Spen: Bhale	Las 4	Oil	Water.	of oil at 60*/60* F
115 116 117 115 119	116 117 118 119 120			96.2 91.2 93.5 94.8 93.8	Q.1 0.1 0.4 0.9	5.70,5,5,5,6.6.4	L.2 6.2 7.5 5.6 5.0	920* .924 .928 .914 .925
120 121 122 123 124	121 122 123 124 125			91.8 90.8 92.7 91.7 93.6	1.7 1.5 1.4 2.4 1.0	10.0 9.7 8.9 10.1 9.0	6.33	.927 .935 .921 .920 .922
125 126 127 128 129	126 127 128 129 130		6	93.7 95.3 94.8 95.4	1.2	9.135.49.7	3.7 3.7 10.6 3.0 2.9	.930 .922 .920* .922
130 131 132 133 134	131 132 133 134 135			94.5 95.6 94.7 95.0 94.2	1.7	7.1 7.3 9.7 7.3	2.7 2.3 4.1	.920 .921 .920 .928 .923
135 136 137 138 139	135 137 138 139 140			92.5 91.0 92.2 93.1 93.4	1.8	10.1 11.7 8.0 6.6 9.1	1.00 A A A A A A A A A A A A A A A A A A	.921 .932 .922 .929
140 141 142 143 144	141 142 143 144 145			93.6 94.2 95.9 94.0	0.7	9.0 7.9 7.8 8.6 8.3	55.4092.4	.926 .933 .916 .931 .933
145 146 147 148 149	146 147 148 149 150			93.8	1.0 0.2 0.8 0.3	7.2 6.6 9.0 11.8 10.7	85067 54434	.937 .919 .928 .946 .935

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OIL-SHALF ASSAYS BY MODITIED FISCHER RETORT METHOD Bamples from the U.S. Omological Survey's Corenole 78-4 (Continued)

			7024						
		-	Taeld of procus					apelifat	
Depth		-		Spen:	Cas +	rel b	er ton	ETAVITY	
7	То	611	Water	mha) e	1055	Oil	Water.	of oil at 60°/60° F	
150 151 152 153 154	151 152 153 153 155 155			93.9 93.9 93.3 93.9 94.3	1.1 0.6 1.6 1.3	S.3 11.3 10.1 9.0 8.3	4.1	934 933 933 933 933	
155 156 157 158 159	156 157 153 159 160			93.8 92.6 92.5 93.6 93.3	1.3 1.5 1.6 0.8 0.9	8.315.315.2	11864	.920 .942 .949 .922	
160 161 162 163 164	161 162 163 164 165			92.8 93.2 94.0 95.8	1.1 0.9 0.8 1.1 0.7	9.7 7.3 6.7 8.1 4.7	5.00 7.10 4.1	.932 .928 .923 .921	
165 166 167 168 169	166 167 163 169 170			94.8 91.9 92.3 93.5 95.6	0.8 1.8 1.5 1.9	6.8 13.1 11.1 9.1 7.3	4.1 2.9 3.4 2.8 4.3	.936 .916 .916 .921	
170 171 172 173 174 175 176 177 178	171 172 173 174 176 177 178 179 180			95.1 96.1 96.1 98.8 976.3 96.3 976.3 976.3	9.1 9.1 9.1 9.1 0.2 0.3 0.2 0.5	7.75.44.48 1.48 1.79.46	380000000000000000000000000000000000000	.914 .927 .920 * .920 * .920 * .920 * .920 * .912 .913	
180 181 182 183 184	181 182 183 184 185			92.6 93.5 93.2 93.6 92.6	211010-510	8.5 7.0 7.4 6.6	15.823	.913 .919 .916 .904 .907	

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OIL-SHALF ASSAYS BY MODIFIED PISCHER RETORT METHOD Samples from the U.S. Employical Survey's Corehole 78-4 (Continued)

5.4 6 6 5 5 6 6 8 6 1 2 7 9 1 1 1 9 1 1 1 1 1 1 1 1 1 1 1 1 1 1	on pro-	######################################
11 WA 5.4 66556 55.8 225 6 685 9.225 0.1 886 1.7 4.9	10	909 909 920 913 920 *
5.48 6 55 5 6 6 8 6 1 1 2 7 9 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	.0 .0 .3 .1 .4	760° F 902 903 920 913 920 *
5.8 6556 6556 6556 6556 6556 6556 6556	.0 .3 .1 .4	.920 .920 .920 * .920 *
9.2 556 6.2 5 6.2 6 7.2 6 1.7 6 1.9	3.4 3.4 3.6 3.0	.920 * .920 * .920 *
9.2 56 0.1 68 2.2 1.7 4.9	3.4 3.9 3.6 3.0	913 920 * .920 *
2.5 6 0.1 6 2.2 8 1.7 6 1.9 L	3.6 3.6	* CSQ. * CSQ. * CSQ.
0.1 6 2.2 8 1.7 6 4.9 L	3.6 3.6	.920 *
2.2 8 1.7 6 1.9 L	3.6 3.0	920 ¥
1.7 £	5.0 1.2	920 *
4.9 1	.0	227 #
	2	
1.7 5		· 920 *
	0.0	* CSE.
0.0 1	101	.935 .934 .937
9.9 1	5	.934
2.5	4.1	.927
12.8	1.1	.925
12.0	4.0	.918
12.0	4.2	.920
5.2	5-3	.923
6.6	2	.922
1-1	2.7	.939
2.2	3.0	• 7 57
5.0	3-7	.924
5.8	2.9	.935
	3.5	• 727
7.4	2.2	.921
7.0	3.4	
5.8	3.8	.919
4.7	L.1	.312
6.5	3.3	.923 .920 >
5.0	10	.920
2.0	7.0	.915
8 1.	10	
	1.7 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1.7 5.6 45.1 1.0 2.32.9.6 7.9.6.2.2 8.1.3.4.8 6.5.8 7.5 5.5.6.9.9.8 8.7.8 5.8 6.8 9.4 8.7 8.7 8.7 8.7 8.7 8.7 8.7 8.7 8.7 8.7

^{*} Assumed Specific Gravity

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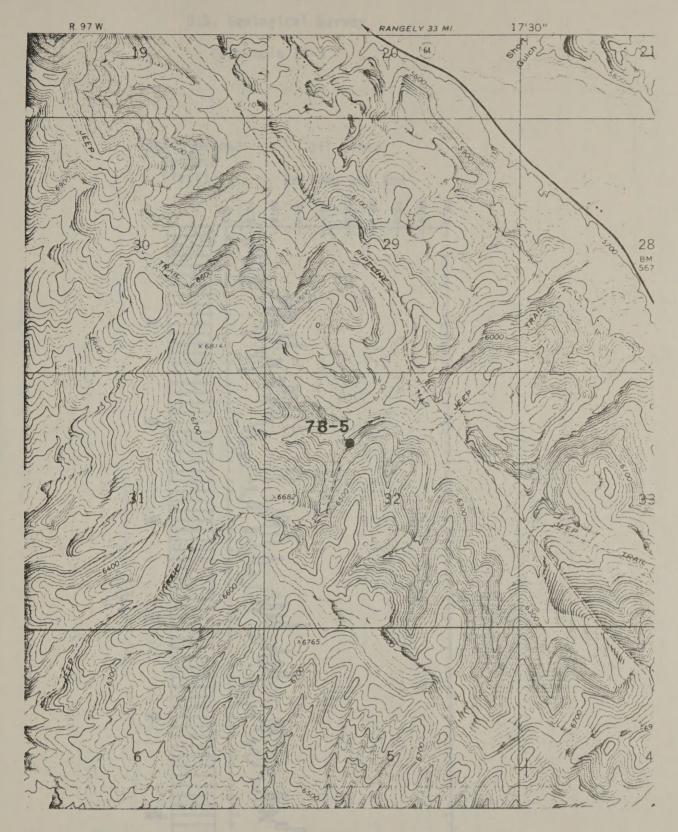


Figure 6.--Map showing location of core hole 78-5. Base from Barcus Creek SE. Quadrangle (1966). Scale 1:24,000.

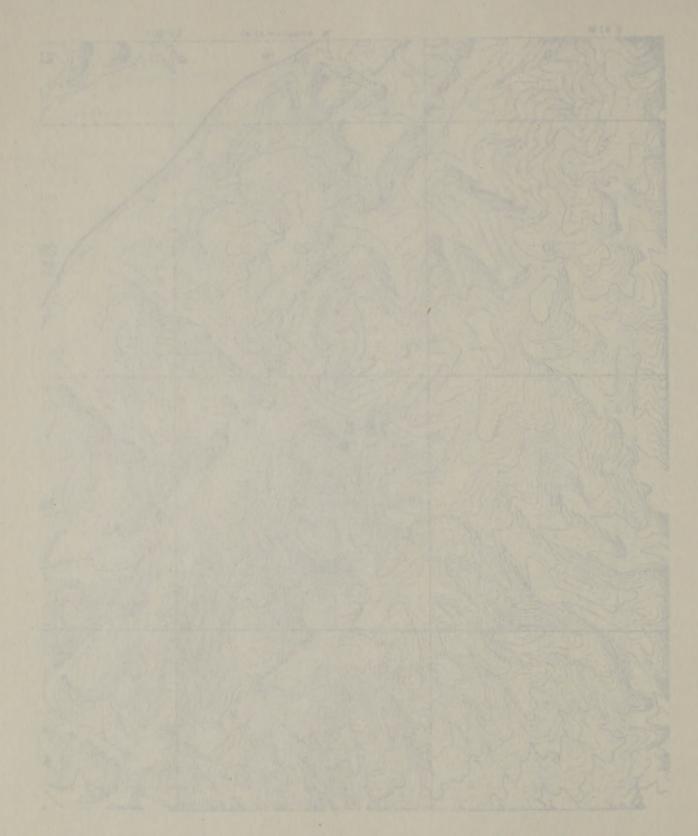
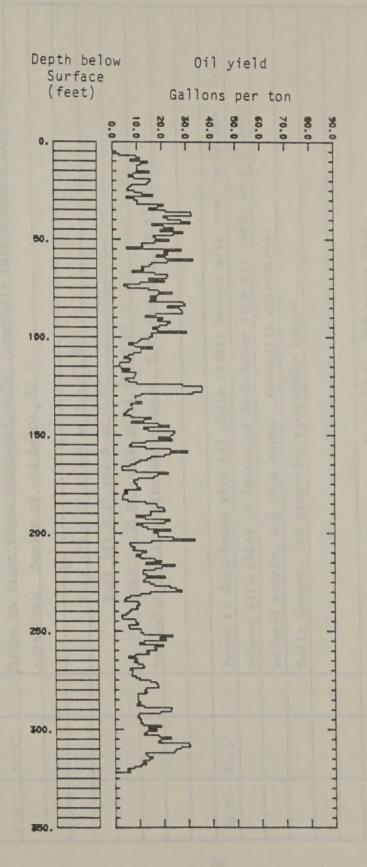


Figure 5. -- Map showing location of cute hole 75-5. Base From Berous Creek 56. Quadrangle (1956), Scale 1-34,000.

U.S. Geological Survey

Core hole 78-5



FROM	то	THICK-	LITHOLOGIC DESCRIPTION
6.0'	30.9'		Brown to light brown weathered shale, generally thinly bedded with some
O.U.			turbation. Smells of oll below -12.0'.
			Tuff (?) 0.2' thick at 7.6'-7.8'
			Tuff (?) 0.1' thick at 7.9'
			Clay 0.2' thick at 11.8'-12.0'
			Tan calcitic layer with shale chips, 0.2' thick at 25.5'-25.7'
			tunketien Units
30.91	97.1'		Brown to dark-brown rich oil shale thinly bedded with some turbation. Units
			common with chips or lenses of dark-brown rich oil shale in a lighter
			colored matrix, and vice versa. Generally calcareous.
	1		Tuffs common, few gray-clay rich shale layers
			There are the comment of the comment
			The state of the s
			Tuff 0.2' thick at 37.3'-37.5' with minor shale
			Tuff 0.1' thick at 38.7'
			Tuff 0.2' thick at 49.3'-49.5'
			Tuff 0.4' thick at 51.0'-51.4' with minor shale
			Tuff 0.1' thick at 55.8'
			Tuff 0.1' thick at 68.1' with minor shale
			Tuff 0.1' thick at 72.1'
and at a death or description any other or			Tuff 0.3' thick at 72.5'-72.8'
			Tuff 0.1' thick at 79.8'

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FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION
			Tuff 0.2' thick at 93.0'-93.2'
			Total Committee of the
			· ·
97.1'	177.5		Dark-gray and gray-brown to reclay rich oil shale with tan lean to brown
			moderately-rich oil shale interbedded. Thinly bedded with some distinct
			tuffs. Virtually noncalcareous.
	- 11,111		Tuff 0.2' thick at 113.4'-113.5'
			Tuff 0.1' thick at 113.8'
			Tuff 0.1' thick at 133.0'
			Tuff 0.2' thick at 146.6'-146.8'
			Tuff 0.1' thick at 147.8'
			Very dark brown rich oil shale, 157.9'-162.2', 5.3' thick
			Tuff 0.1' thick at 165.0'
			Tuff 0.2' thick at 165.6'-165.8'
			Dark-brown rich oil shale 169.0'-172.0', 3.0' thick
			•
			THE REPORT OF THE PROPERTY OF
			Settle 1922 Third Set 1 -2-3 I with allow shale
na material de l'autoris de descrito de	-	- CL-Disease	

FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION
177.5'	197.8'		Gray to brown somewhat silty shale, lean oil shale. Medium bedding with some
			tuffs. Somewhat calcareous.
			The same to the second
			Tuff 9.1' thick at 181.7'
-			Tuff 0.1' thick at 191.5'
			Dark brown moderately rich oil shale 192.8'-194.4', 1.6' thick
			Management 2 Transport of the Control of the Contro
			- Discourse de la constant de la con
197.8'	323.0'		Dark brown thinly bedded oil shale with some light brown oil shale and tuffs.
Bottom	of hole		Very clay rich with some calcite
			Allegations D. 32 Oblak at 787 As707.72
			Tuff 0.1' thick at 205.7'
			Tuff 0.2' thick at 207.7'-207.9'
			Tuff 0.1' thick at 218.1'
			Tuff 0.2' thick at 222.1'-222.3'
-			Tuff 0.2' thick at 236.2-236.5'
-			Tuff 0.1' thick at 236.8'
A COM PROPERTY OF THE PARTY OF			Tuff 0.1' thick at 245.7'
			Tuff 0.2' thick at 246.8'-247.0'
	-		Tuff 0.1' thick at 248.4'
and the second state state of the			Tuff O.l' thick at 248.8'
			Tuff 0.2' thick at 250.1'-250.3'
and the same of th			Tuff 0.2' thick at 253.1'-253.3' with minor shale
AND DESCRIPTION OF PERSONS ASSESSMENT AND PARTY.	to the second contract to the second	~ . ~ . ~ . ~	Tuff 0.2' thick at 254.5'~254.7'

FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION
			Tuff 0.1' thick at 255.8'
			Tuff 0.1' thick at 256.4'
			Limestone 0.2' thick at 260.8'-261.0'
			Limestone 0.25' thick at 265.8'-266.05' ostrocods?
			Sandstone? 0.3' thick at 268.4'-268.7'
			Limestone 0.1' thick at 271.0'
			Limestone 0.2' thick at 275.6'-275.8'
			Limestone 0.1' thick at 282.3'
			Limestone 0.2' thick at 284.2'-284.4'
			Limestone 0.1' thick at 284.9'
			Limestone 0.3' thick at 287.4-287.7'
			Limestone 0.2' thick at 300.3'-300.5'
			Limestone 0.1' thick at 308.7'
			Limestone 0.2' thick at 309.6'-309.8'
			Limestone 0.1' thick at 311.7'
			Limestone 0.25' thick at 318.95'-319.2'
			The hole was capped with a large stone slab and is in service as a Water
			Resources Division observation and test well. Water production with drilling
	and the second s		fluid probably began between 50-100' denth and slowly increased with increasing
			depth. At 290' water production dropped off, possibly due to loss in lower
			fractures or fluid back pressure scaling.
manufaction of the other states		-	

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FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION
			Slickenside ranged in dip from $\sim 10^{\circ}$ to 70° most commonly being 20° - 50° . Low
			angle dips (20°-30°) are particularly common. Fault striations are usually
			parallel to the dip, rarely perpendicular or oblique.
			Many tuffs, lean maristones, dolomite, and impure limestones were difficult
+			to distinguish due to similar color and texture and some confusion may have
41.3			resulted.
		-	

Samples from the U.S. Geological Survey's Corchole 78-5 drilled in sec. 32, T 2 N., R. 97 W. Rio Blanco County, Lolorado

					of proc	luct		Specific
Dep	th		Weight	percent		Gal p	er ton	: Eravity
From		0.1	ALC: NO	Spent	606 +			of oil at
Colli	To	Oil	Water	stiale	loss	0111/	Water	60°/60° F
4.0				- Shall	- 2200	Dr. 1-5	Maler	650/400 9
6.0	7.0	1.1	2.8	94.8	1.3	2.8a	6.7	
7.0	8.0	3.7	2.8	91.3	2.2	9.7	6.7	0.911
8.0	9.0	4.3	3.7	89.7	2.3	11.3	8.9	.916
9.0	10.0	2.8	3.5	91.9	1.8	7.4	8.4	.903
10.0	11.0	5.5	3.9	87.7	2.9	1.4.6	9.3	.907
11.0	12.0	4.4	5.4	87.4	2.8	11.6	12.9	.910
12.0	13.0	3.8	3.7	89.8	2.7	10.0	8.9	.900
13.0	14.0	3.9	4.1	89.8	2.2	10.3	9.8	.903
14.0	15.0	3.7	2.9	91.6	1.8	9.9	7.0	.901
15.0	16.0	5.8	5.0	86.6	2.6	15.2	12.0	.913
16.9	17.0	3.2	3.5	91.7	1.6	8.6	8.4	. 898
17.0	18.0	2.5	5.0	90.9	1.6	6.7	12.0	. 898
18.0	19.0	3.4	4.6	90.3	1.7	9.0	11.0	.903
19.0	20.0	6.0	4.0	87.4	2.6	15.6	9.6	.917
20.0	21.0	5.7	2.5	89.6	2.2	15.0	6.0	.905
21.0	22.0	5.4	2.6	89.2	2.8	14.2	6.2	.914
22.0	23.0	2.9	2.2	92.4	2.5	7.7	5.3	
23.0	24.0	2.4	2.8	93.1	1.7	6.6		. 896
24.0	25.0	2.2	2.1				6.7	.886
25.0	26.0	4.6		94.4	1.3	6.0	5.0	.887
26.0			2.0		1.7	12.1	4.3	.901
27.0	27.0	6.3	2.2	89.3	2.2	16.6	5.3	. 909
28.0	28.0	2.1	2.0	94.3	1.6	5.6	4.8	. 89 7
	29.0	3.3	2.3	93.0	1.4	8.9	5.5	. 895
29.0	30.0	3.9	1.9	92.7	1.5	10.3	4.6	.900
30.0	31.0	3.8	2.3	92.3	1.6	10.1	5.5	. 899
31.0	32.0	7.9	2.0	87.1	3.0	20.9	4.8	.913
32.0	33.0	7.1	1.9	88.0	3.0	18.5	4.6	.920
33.0	34.0	5.7	2.0	89.6	2.7	14.9	4.8	.920
34.0	35.0	8.3	2.1	85.0	4.6	21.7	5.0	.920
35.0	36.0	12.3	2.5	78.8	6.4	32.1	6.0	.914
36.0	37.0	12.3	2.6	80.6	4.5	32.3	6.2	0.915
37.0	38.0	7.9	2.0	87.5	2.6	20.8	4.8	.908
38.0	39.0	8.6	2.1	86.7	2.6	22.6	5.0	.911
39.0	40.0	10.6	2.9	83.6	2.9	27.9	7.0	.909
40.0	41.0	12.1	2.9	81.9	3.1	31.8	7.0	.908
41.0	42.0	6.1	2.6	89.1	2.2	16.1	6.2	.913
42.0	43.0	8.0	2.2	87.3	2.5	20.9	5.3	.910
43.0	44.0	9.5	2.2	85.7	2.6	25.0	5.3	.914
44.0	45.0	7.4	2.6	87.0	3.0	19.4	6.2	.917
45.0	46.0	11.0	2.4	81.7	4.9	28.9	5.8	.914
46.0	47.0	9.5	2.7	84.2	3.6	24.9	6.5	.913
47.0	48.0		2.0	89.7	2.0	16.6	4.8	.917
48.0	49.0	6.3			2.1	17.7	4.8	.921
49.0	50.0	6.8	2.0	89.1			4.8	.924
50.0	51.0	. 8.9	2.0	86.8	2.3	23.2	4.0	

as battire that it is a to describe the distance former, the translated and

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OIL-SHALE ASSAYS BY MODIFIED FISCHER RETORT MITHOD

Samples from the U.S. Geological Survey's Corehole 78-5 (Continued)

			Yield	of prod	1000		
		Weight	percent	o. prou.	Gal pe	7 700	Specific
Depth			Spent	Gas +		Lon	gravity
From To	Oi1	Water	shale	loss	0i11/	Water.	of oil at 60°/60° F
51.0-52.0	6.7	1.7	00 5	2 7			
52.0-53.0	4.4	2.7	89.5	2.1	17.3	4.1	.922
53.0-54.0	4.6	2.8	91.4	1.5	11.8	6.5	.901
54.0-55.0	6.0	3.2	89.0	1.7	12.4	6.7	.897
55.0-56.0	10.8	2.4	83.7	1.8	5.7	7.7	.911
56.0-57.0	8.0	3.0	86.2	3.1	28.2	5.8	.919
57.11-53.0	8.6	2.4	86.2	2.8	20.9	7.2	.915
58.0-59.0	6.8	2.8		2.8	22.6	5.8	.911
59.0-60.0	8:3	2.2	87.8	2.6	17.8	6.7	.911
60.0-61.0	12.6		86.2	3.3	21.6	5.3	.916
		2.3	81.6	3.5	32.9	5.5	.915
61.0-62.0	8.6	2.0	86.4	3.0	22.4	4.8	.919
62.0-63.0	6.1 5.7	1.9	90.0	2.0	16.0	4.6	.919
63.0-64.0		2.8	89.7	1.8	15.0	6.7	.913
64.0-65.0	4.4	2.9	90.7	2.0	11.8	7.0	. 899
65.0-66.0	4.8	2.8	. 90.6	1.8	12.7	6.7	.901
66.0-67.0	3.0	3.0	92.4	1.6	8.0	7.2	.892
67.0-68.0	0.6	2.9	87.6	2.9	17.3	7.0	0.913
68.0-69.0	8.6	1.7	86.9	2.8	22.6	4.1	.917
69.0-70.0	8.5	2.4	85.4	3.7	22.1	5.8	.921
70.0-71.0	5.6	3.4	88.7	2.3	14.6	8.1	.920
71.0-72.0	8.2	2.9	86.2	2.7	21.3	7.0	.921
72.0-73.0	4.2	2.5	91.5	1.8	11.1	6.0	.903
73.0-74.0	1.7	2.6	94.8	.9	4.5a	6.2	
74.0-75.0	2.3	2.3	94.1	1.3	6.1	5.5	.896
75.0-76.0	5.6	2.6	90.1	1.7	14.7	6.2	.909
76.0-77.0	7.2	2.7	88.1	2.0	18.8	6.5	.910
77.0-78.0	9.2	2.7	85.3	2.8	24.3	6.5	.912
78.0-79.0	6.9	3.2	87.3	2.6	18.4	7.7	.907
79.0-80.0	5.8	2.8	89.4	2.0	15.3	6.7	.909
80.0-81.0	6.7	2.4	88.4	2.6	17.7	5.8	.906
81.0-82.0	5.7	2.6	89.0	2.7	15.0	6.2	. 91,6
82.0-83.0	10.9	2.5	82.7	3.9	28.9	6.0	.906
83.0-84.0	11.2	2.7	82.8	3.3	29.7	6.5	.904
84.0-85.0	8.4	3.0	85.5	3.1	22.2	7.2	.903
85.0-86.0	10.3	3.1	83.4	3.2	27.3	7.4	.902
86.0-87.0	10.6	2.7	83.6	3.1	28.3	6.5	.903
87.0-88.0	10.8	2.7	83.5	3.0	28.5	6.5	.907
88.0-89.0	6.7	2.7	88.5	2.1	17.6	6.5	.903
89.0-90.0	5.0	3.5	89.7	1.8	13.2	8.4	.902
90.0-91.0	7.8	3.1	85.8	3.3	20.5	7.4	.913
91.0-92.0	7.0	2.1	88.3	2.6	18.3	5.0	.917
92.0-93.0	9.1	1.7	86.1	3.1	23.5	4.1	.924
93.0-94.0	8.5					4.1	
94.0-95.0		1.7	87.5	2.3	22.1		.923
95.0-96.0	7.3	3.1	87.5	2.1	19.0	7.4	.923
	6.2	3.1	88.9	1.8	16.2	7.4	.913
96.0-97.0	7.0	3.4	87.4	2.2	18.2	8.1	.920

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Samples from the U.S. Confederal Servey's Corebett

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			9.3	
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OLL-SHALF ASSAYS BY MODIFIED FISCHER RETORT MITHOD

Samples from the U.S. Geological Survey's Corehole 78-5 (Continued)

	-		Yield	of prod	uct		Specific
Depth		Weight	percent		Gal p	er ton	gravity
From: To	011	Water	Spent	Gas +		3.3	of oil at
	011	Murer	shale	loss	0i11/	Water.	60°/60°
							/ 1975
97.0-98.0	11.5	3.0	82.1	3.4	30.2	7.2	0.911
98.0-99.0	5.9	2.9	89.0	2.2	15.5	7.0	.912
99.0-100.0	6.2	2.5	89.4	1.9	16.2	6.0	.917
100.0-101.0	5.6	2.8	89.4	2.2	14.8	6.7	.905
101.0-102.0	4.2	2.4	92.0	1.4	11.2	5.8	.901
102.0-103.0	3.8	3.6	90.6	2.0	10.2	8.6	.893
103.0-104.0	2.3	3.5	93.1	1.1	6.4	8.4	.876
104.0-105.0	3.2	2.7	92.8	1.3	8.7	6.5	.879
105.0-106.0	6.0	2.9	89.0	2.1	16.1	7.0	. 896
106.0-107.0	4.2	2.9	91.6	1.3	11.3	7.0	.893
107.0-108.0	4.2	2.4	91.3	2.1	11.3	5.3	.896
108.0-109.0	3.1	3.5	92.2	1.2	8.3	8.4	.894
109.0-110.0	2.3	2.8	93.3	1.6	6.3	6.7	.885
110.0-111.0	1.7	2.9	94.8	.6	4.4a	7.0	.003
111.0-112.0	2.7	2.9	93.5	.9	7.3		000
112.0-113.0	2.5	3.0	93.3	1.2	6.7	7.0	.889
113.0-114.0	1.0	1.4	97.0	.6		7.2	. 894
114.0-115.0	.9	2.3	96.0	.8	2.64	, 3, 4	
115.0-116.0	1.2	2.5	95.6	. 7	2.3a	5.5	
116.0-117.0	2.6	2.6	93.0	1.8	3.2a	6.0	0.00
117.0-118.0	1.4	1.3	95.2		6.8	6.2	.906
118.0-119.0	3.5	2.9	92.0	2.1	3.6a	3.1	
119.0-120.0	3:3	2.3		1.6	9.3	7.0	.901
120.0-121.0	3.2		92.8	1.6	8.9	5.5	.902
121.0-122.0	1.9	2.3	93.0	1.5	8.5	5.5	.899
122.0-123.0	2.4	1.6	95.1	1.4	4.9a	3.8	
123.0-124.0		1.6	94.0	2.0	6.4	3.8	.912
124.0-125.0	3.6	1.9	93.0	1.5	9.6	4.6	.908
125.0-126.0	10.8	1.9	84.5	2.8	28.3	4.6	.910
126.0-127.0	13.8	2.1	80.6	3.5	36.3	5.0	.910
127.0-128.0	13.8	2.1 2.3	80.6	3.5	36.4	5.0	. 906
			79.8	4.2	36.2	5.5	0.910
128.0-129.0	12.3	2.4	81.5	3.8	32.5	5.8	.909
129.0-130.0	4.2	2.2	91.4	2.2	11.2	5.3	.905
130.0-131.0	3.4	2.0	92.6	2.0	8.8	4.3	.909
131.0-132.0	3.4	1.8	92.5	2.2	9.2	4.3	.909
132.0-133.0	3.4	1.9	92.8	1.9	9.1	4.6	.912
133.0-134.0	4.4	1.7	92.1	1.8	11.6	4.1	.910
134.0-135.0	2.6	1.6	94.3	1.5	7.0	3.8	.909
135.0-136.0	3.0	1.8	93.8		. 7.8	4.3	.908
136.0-137.0	2.9	2.0	93.5	1.6	7.6	4.8	.910
137.0-138.0	2.3	1.8	94.2	1.7	6.0	4.3	.911
138.0-139.0	2.0	1.9	94.5	1.6	5.2	4.6	.917

NAME AND ADDRESS OF PERSONS ASSESSED ASSESSED.

Semples from the U.S. Contractor Shreet's Corenals

Samples from the U.S. Geological Survey's Corehole 78-5 (Continued)

		•	. 70-3	COBEIL			
	-	Weight	Yield o	of proo			Specific
Depth		ac a Kill		6	Gel po	er ton	gravity
From To	011	Water	Spent	Gas +	0111/		of oil at
70.00			BIIGIE	loss	011-	Water.	60°/60° F
.139.0-140.0	1.6	2.2	94.3	1.9		E 2	27
140.0-141.0	2.7	2.3	93.3	1.7	4.1a 7.2	5.3	
141.0-142.0	5.8	2.0	90.1	2.1	15.4	5.5	.907
142.0-143.0	4.7	1.8	91.5	2.0	12.4	4.8	.905
143.0-144.0	2.7	2.4	93.2	1.7	7.2	4.3	.907
144.0-145.0	7.0	2.0	89.0	2.0	18.4	5.8	.903
145.0-146.0	8.7	2.3	86.2	2.8	22.8	4.8	.906
146.0-147.0	4.7	2.3	91.1			5.5	.910
147.0-148.0	5.4	2.2	90.2	1.9	12.2	5.5	.910
148.0-149.0	9.6	2.4	85.0	2.2	14.2	5.3	.912
149.0-150.0	9.3	2.3		3.0	25.1	5.8	.917
150.0-151.0	9.0		85.5	2.9	24.4	5.5	.917
151.0-152.0	7.1	2.3	86.1	2.6	23.4	5.5	.920
152.0-153.0		2.3	87.7	2.9	18.3	5.5	.924
153.0-154.0	9.2	2.3	85.4	3.1	24.0	5.5	.921
154.0-155.0	5.0	2.4	90.1	2.5	13.1	5.8	.918
	2.7	2.1	93.0	2.2	7.2	5.0	.907
155.0-156.0	2.4	2.2	93.8	1.6	6.4	5.3	.903
150.0-157.0 157.0-158.0	5.0	2.0	90.9	2.1	13.1	4.8	.908
	8.8	1.9	86.8	2.5	23.2	4.6	0.913
158.0-159.0	11.0	2.1	83.1	3.2	30.3	5.0	.920
159.0-160.0	8.8	2.8	85.5	2.9	23.0	6.7	.910
160.0-161.0	7.8	2.5	87.3	2.4	20.7	6.0	.899
161.0-162.0	5.7	2.7.	89.5	2.1	15.1	6.5	.903
162.0-163.0	5.0	3.0	90.5	1.5	13.6	7.2	.892
163.0-164.0	3.9	3.5	90.2	2.4	10.4	8.4	.904
164.0-165.0	3.3	2.2	92.4	2.1	8.9	5.3	.899
165.0-166.0	2.5	1.9	94.6	1.0	6.7	4.6	.891
166.0-167.0	1.2	2.9	94.9	1.0	3.2a	7.0	
167.0-168.0	1.3	2.8	94.9	1.0	3.4a	6.7	
163.0-169.0	3.4	2.8	91.3	2.5	9.1	6.7	.902
169.0-170.0	8.5	2.0	86.4	3.1	22.4	4.8	.909
170.0-171.0	6.3	2.5	88.4	2.3	18.0	6.0	.901
171.0-172.0	6.2	2.6	89.1	2.1	16.4	6.2	.902
172.0-173.0	3.6	3.2	91.3		9.8	7.7	.837
173.0-174.0	2.9	3.5	90.9	2.7	8.0	8.4	
174.0-175.0	3.2	3.2	92.1	1.5	8.6	7.7	.883
175.0-176.0	3.5	3.0	91.1				.894
176.0-177.0	3.6	3.7	90.7	2.4	9.4	7.2	.891
177.0-178.0	4.1		91.7	2.0	9.6	8.9	.898
178.0-179.0	1.7	2.6		1.6	10.9	6.2	.908
179.0-186.0		2.1	95.3	.9	4.3a	5.0	200
180.0-181.0	2.1	2.5	94.0	1.4	5.6	6.0	.885
181.0-182.0	1.6	2.3	94.9	1.2	4.0a	5.5	
182.0-183.0	1.4	2.3	95.3	1.0	3.6a	5.5	
183.0-184.0	1.3	2.5	95.0	1.2	3.4a	6.0	4450
	2.2	2.5	94.0	1.3	5.8	6.0	.931
154.0-185.0	4.9	2.1	91.2	1.8	13.1	5.0	.890
185.0-186.0	6.6	2.1	88.88	2.5	17.5	5.0	.901
186.0-187.0	6.7	2.4	88.5	2.4	17.8	5.8	.897

CONTRACTOR OFFICE AND ADDRESS OF TAXABLE PARTY.

despite from the U.S. designed increase of the state of

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OIL-SHALF ASSAYS BY MODIFIED FISCHER RETORT MITHOD

Samples from the U.S. Geologics) Survey's Corehole
78-5 (Continued)

			Yield	of prod	uc:		Specific gravity
Jane 1	-	Weight	percent		Gal pe	T ton	
Depth	2011	. Name and	Spent	Gas +			of oil at
From To	Oil	Water	shale	loss	0i11/	Water.	60°/60° F
147 6 100 6	7 7	2 0					
187.0-188.0	7.7	2.0	86.8	3.5	20.3	4.8	0.909
188.0-189.0	7.9	1.9	87.3	2.9	20.9	4.6	.910
169.0-190.0	5.6	2.1	90.2	2.1	14.8	5.0	.911
190.0-191.0	5.7	1.9	90.4	2.0	15.2	4.6	.908
191.0-192.0	3.4	2.2	92.5	1.9	9.0	5.3	.907
192.0-193.0	4.8	1.9	91.5	1.8	12.8	4.6	.909
193.0-194.0	8.7	2.6	36.0	2.7	23.0	6.2	.907
194.0-195.0	7.8	1.7	88.1	2.4	20.8.	4.1	.904
195.0-196.0	3.5	2.1	92.7	1.7	9.2	5.0	.904
196.0-197.0	. 4.4	1.9	91.6	2.1	11.7	4.6	.913
197.0-198.0	5.3	1.9	90.8	2.0	13.7	4.6	.916
198.0-199.0	8.9	1.6	86.5	3.0	23.2	3.8	.919
199.0-200.0	6.1	2.2	89.7	2.0	1ó.2	5.3	.900
200.0-201.0	6.8	2.8	88.1	2.3	18.0	6.7	.900
201.0-202.0	6.9	2.9	. 87.2	3.0	18.1	7.0	.918
202.0-203.0	9.3	2.2	85.6	2.9	24.2	5.3	.921
203.0-204.0	12.9	2.2	81.4	3.5	33.2	5.3	.929
204.0-205.0	5.8	2.5	88.7	3.0	15.3	6.0	.918
205.0-206.0	2.4	2.5	92.8	2.3	6.3	6.0	.895
206.0-207.0	- 2.5	3.5	91.2	2.8	6.9	8.4	.884
207.0-208.0	3.2	2.7	92.2	1.9	8.5	6.5	.898
208.0-209.0	2.8	3.0	91.4	2.8	7.7	7.2	.883
209.0-210.0	4.9	3.5	89.2	2.4	13.3	8.4	.892
211.0-212.0	3.4	3.9	87.9	4.8	9.0	9.3	.893
212.0-213.0	4.0	3.8	89.0	3.2	10.8	9.0	.896
213.0-214.0	6.4	3.0	83.1	2.5	16.8	7.2	
214.0-215.0	7.5	1.8	87.9	2.8	19.5	4.3	.906
215.0-216.0	5.0	1.7	90.8	2.5	12.9		.920
216.0-217.0	9.6	2.0	85.5	2.9	24.9	4.1	.925
217.0-218.0	7.5	2.6	87.2	2.7	19.5	6.2	.930
218.0-219.0	6.4	2.5	88.7	2.4		6.0	.928
219.0-220.0	4.6	2.4	90.9	2.1	11.8	5.8	
220.0-221.0	4.5	3.2	89.7	2.6	11.6	7.7	.926
221.0-222.0	5.1	3.4	87.7	3.8			.925
222.0-223.0	8.1	2.8	86.2		13.2	8.1	.925
223.0-224.0	4.9	2.0		2.9	20.9	6.7	.929
224.0-225.0	4.6	3.0	90.7	2.4	12.6	4.8	.927
225.0-226.0	5.5		90.0	2.4	11.8	7.2	.921
226.0-227.0	6.2	3.2	89.1	2.2	14.6		.906
		4.0	87.2	2.6	16.3	9.6	.911
227.0-228.0	8.7	2.4	85.9		22.8	5.8	.914
228.0-229.0	9.7	1.8	85.7	2.8	25.4	4.3	.916
229.0-230.0	10.6	2.2	84.2	3.0	27.6	5.3	.918
230.0-231.0	5.6	3.1	89.0	2.3	14.7	7.4	.920
231.0-232.0	4.0	3.3	90.4	2.3	10.7	7.9	.894
232.0-233.0	2.4	2.8	93.3	1.5	6.5	6.7	.879

NAMES OF TAXABLE PARTY OF TAXABLE PARTY

OLL-SHALE ASSAYS BY MODIFIED FISCHER RETORT MITHOD

Samples from the U.S. Geological Survey's Corehole 78-5 (Continued)

. Denth

	-	17	Yiela	of prod	וחכו		Specific
Depth		Weight	percent	No. of the last	Gal p	er con	gravity
From To	Oil	Water	Spent shale	Cas +	0i1 <u>1</u> /	Water.	of oil at 60°/60° ;
233.0-234.0	1.8	3.6	91.7	2.9	4.8a	8.6	
234.0-235.0	1.6	3.5	92.7	2.2	4.1a	8.4	
235.0-236.0	3.6	2.7	91.2	2.5	9.8	6.5	901
236.0-237.0	3.9	3.4	90.3	2.4	10.4	8.1	.891
237.0-238.0	3.4	1.5	93.6	1.5	9.1	3.6	.904
238.0-239.0	3.5	2.1	91.6	2.8	9.6	5.0	.893
239.0-240.0	2.5	2.6	92.1	2.8	6.8		.888
240.0-241.0	2.2	2.6	92.8	2.4		6.2	.881
241.0-242.0	1.9	2.7	94.1		6.0	6.2	.875
242.0-243.0	1.1	3.2	94.1	1.3	4.9a	6.5	
243.0-244.0	1.2	3.2	93.9	1.6	3.0a	7.7	
244.0-245.0	3.2			1.7	3.3a	7.7	
245.0-246.0		2.3	93.0	1.5	8.6	5.5	.879
246.0-247.0	3.2	2.7	92.3	1.8	8.9	6.5	.880
247.0-248.0	3.6	2.7	92.2	1.5	9.8	6.5	.880
248.0-249.0	2.1	2.6	93.4	1.9	5.8	6.2	.875
249.0-250.0	2.6	2.8	92.0	2.9	6.2	6.7	0.874
230.0-251.0	4.0	3.0	91.3	1.7	10.9	7.2	. 887
251.0-252.0	4.1	2.3	91.4	2.2	10.8	5.5	.903
	4.4	3.0	90.5	2.1	11.8	7.2	.887
252.0-253.0	8.9	2.8	85.6	2.7	23.8	6.7	. 896
253.0-254.0	7.0	2.0	89.0	2.0	18.5	4.8	.903
254.0-255.0	8.0	2.3	86.8	2.9	21.2	5.5	.905
255.0-255.0	4.5	2.9	90.9	1.7	12.1	7.0	. 889
256.0-257.0	3.8	3.0	90.9	2.3	10.3	7.2	.897
257.0-258.0	7.5	2.8	87.1	2.6	20.1	6.7	.890
258.0-259.0	6.0	3.2	88.5	2.3	16.3	7.7	.886
259.0-260.0	6.5	3.2	88.0	2.3	17.3	7.7	.895
260.0-261.0	4.9	3.1	89.4	2.6	13.0	7.4	.899
261.0-262.0	5.3	2.4	90.2	2.1	14.2	5.8	.905
262.0-263.0	3.1	2.9	. 92.1	1.9	8.5	7.0	.883
263.0-264.0	2.1	3.5	92.8	1.6	5.8	8.4	.876
264.0-265.0		3.9	90.9	1.8		9.3	
265.0-266.0		1.9					.877
266.0-267.0		2.9			.9.6		.895
267.0-268.0		2.8		2.0	11.7		.902
268.0-269.0		2.5	90.1	2.0	11.7	6.7	.914
269.0-270.0	2.3			2.0	12.2	6.0	.904
270.0-271.0		2.8	91.8	2.0	6.2	7.9	.897
271.0-272.0			92.6	1.9	7.4	6.7	.891
		3.4	91.8	2.2		8.1	.882
272.0-273.0	2.6	3.4	91.2	2.8		8.1	. 879
273.0-274.0	3.2	3.0	91.8		8.7	7.2	.881
274.0-275.0	3.9	2.7	91.4		10.3	6.5	. 894
275.0-276.0		2.2	90.0		14.6	5.3	.915
276.0-277.0			88.6		17.0	6.0	.913
277.0-278.0	6.7	2.0	88.8	2.5	17.7	4.8	.912

THE REAL PROPERTY AND PERSONS ASSESSED AND PARTY TO SERVE AND PARTY TO

Samples from the U.S. Geological Survey's Coronors

· Par				
			4.5.	

78-5 (Continued)

	-	Yield of product							
Depth		Weight	The second name of the second		Gal pe	er ton	Specific gravity		
From To	0:1		Spent	Gas +			of oil at		
10	Oil	Water	shale	loss	011-1/	Water.	60 160 1		
278.0-279.0	6.9	2.2	88.3	2.6	18.0	5.3	0.913		
279.0-280.0	4.9	3.4	89.6	2.1	13.0	8.1	.909		
280.0-281.0	4.6	3.5	88.88	3.1	12.2	8.4	.905		
281.0-282.0	5.0	3.6	88.7	2.7	13.2	8.6	.904		
282.0-283.0	3.5	2.8	91.8	1.9	9.4	6.7	.902		
284.0-285.0	3.5	2.4	91.6	2.5	9.5	5.8			
285.0-286.0	3.6	2.7	91.6	2.1	9.6	6.5	.899		
286.0-287.0	3.9	2.7	91.0		10.5	6.5	.899		
287.0-288.0	3.4	2.6	92.3	1.7	9.0		. 896		
288.0-289.0	4.6	2.4	91.1	1.9		6.2	.902		
289.0-290.0	8.8	2.5	85.5		12.0	5.8	.910		
290.0-291.0	8.6	3.0		3.2	23.3	6.0	.911		
291.0-292.0	7.0		85.1	3.3	22.9	7.2	.904		
292.0-293.0	3.7	3.0	86.6	3.4	18.7	7.2	.900		
293.0-294.0		2.6	91.8	1.9	9.9	6.2	.895		
294.0-295.0	3.5	2.9	90.7	2.9	9.3	7.0	.899		
	3.8	2.3	90.9	3.0	10.1	5.5	.893		
295.0-296.0	4.0	2.7	91.2	2.1	10.8	6.5	. 886		
290.0-297.0	3.9	2.6	91.4	2.1	10.5	6.2	.839		
297.0-298.0	4.3	2.3	91.3	2.1	11.5	5.5	.889		
298.0-299.0	7.1	2.8	87.9	2.2	19.1	6.7	.895		
299.0-300.0	5.1	2.6	90.0	2.3	13.6	6.2	.896		
300.0-301.0	6.4	2.3	89.5	1.8	17.1	5.5	.902		
301.0-302.0	4.9	3.4	89.9	1.8	13.0	8.1	.893		
302.0-303.0	4.4	2.5	91.6	1.5	11.9	6.0	. 894		
303.0-304.0	6.8	1.9	88.8	2.5	18.1	4.6	.901		
304.0-305.0	8.6	3.7	85.1	2.6	23.0	8.9	. 896		
305.0-306.0	7.1	2.4	87.5	3.0	18.7	5.8	.916		
306.0-307.0	6.7	2.8	87.9	2.6	17.7	6.7	.912		
307.0-308.0	11.6	2.1	83.7	2.6	30.3	5.0	.915		
308.0-309.0	11.7	2.4	83.2	2.7	30.8	5.8	.909		
309.0-310.0	10.2	2.6	84.4	2.8	26.9	6.2	0.908		
310.0-311.0	9.3	2.3	85.5	2.8	24.9	5.5	.910		
311.0-312.0	9.2	2.9	85.5	2.4	24.2	7.0	.907		
312.0-313.0	4.6	3.2	90.2	2.0	12.3	7.7	.893		
313.0-314.0	4.9	2.9	90.3	1.9	13.3	7.0	.892		
314.0-315.0	5.8	2.6	89.0	2.6	15.4	6.2	.903		
315.0-316.0	5.3	2.9	88.6	3.2	14.0	7.0	.905		
316.0-317.0	4.3	3.4	90.1	2.2					
317.0-318.0	4.7	3.3			11.4	8.1	.900		
			89.6	2.4	12.7	7.9	.892		
318.0-319.0	3.9	2.6		2.4	10.5	6.2	.859		
319.0-320.0	2.9	2.8	92.0	2.3	7.9	6.7	.889		
320.0-321.0 321.0-322.0	1.9	2.9	93.5	1.7	5.0a	7.0	12/19/2017		
	2.3	2.8	92.2	2.7	6.2	6.7	.874		

^{1/ &}quot;a"--indicates specific gravity estimated as 0.92.

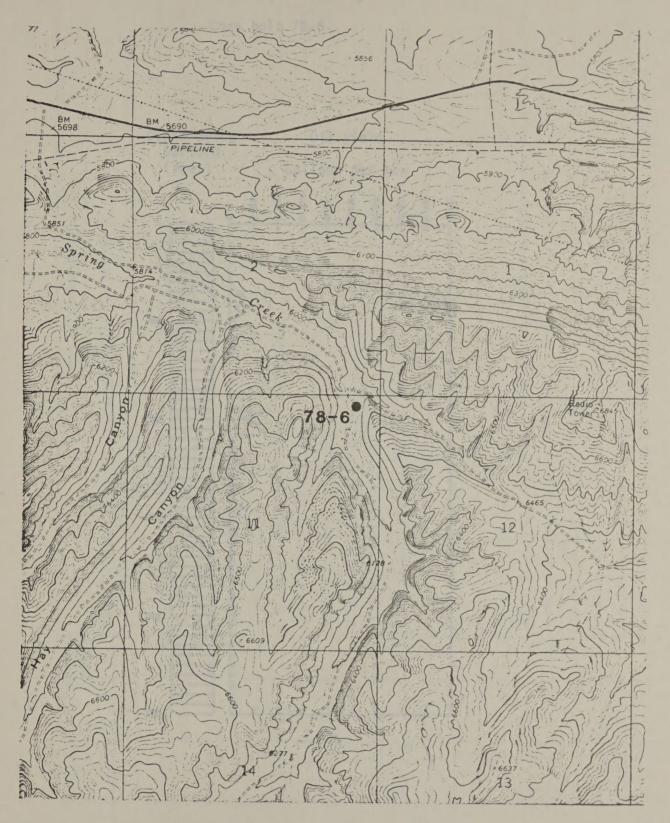


Figure 7.--Map showing location of core hole 78-6. Base from Rough Gulch Quadrangle (1966). Scale 1:24,000.

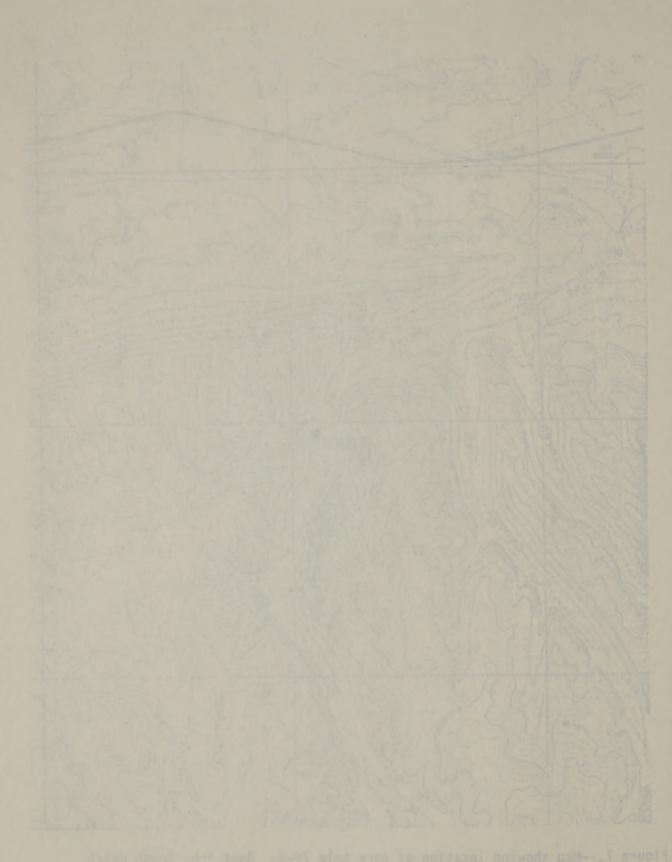
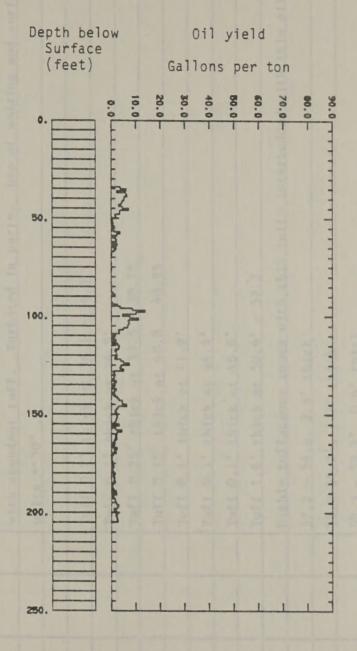


Figure 7. -- Map showing location of core tole 20-5. Base rele Tolen Guadrangle (1966), Scale Isla, 000.

U.S. Geological Survey

Core hole 78-6



Core Nole 78-6

with abundant tuff. Turbated in parts. Dip of bedding and surface rock

LITHOLOGIC DESCRIPTION

Massive tuff 1.1' thick at 74.5 - 75.6' minor shale

Massive tuff 0.1' thick at 70.2'

Massive tuff 0.1' thick at 76.8

Massive tuff 0.15' thick at 79.35 - 79.5

Brown to dark and gray brown oil shale interbedded

THICK-

NESS

units ~30°.

TO

64.0

FROM

34.0

										Settle with		

FROM	TO	THICK- NESS	LITHOLOGIC DESCRIPTION
			ruff 0.15' thick at 145.5-145.65
	·		Highly turbated zone with local unconformities and auto-conglomerate of oil shale
		× 10 100	and tuff clasts in a muddy calcific matrix 156.4 to 156.9 , 0.5' thick
167.0	204.8		Highly tuffaceous with brown to gray lean oil shale interbedded with abundant
			tuff. Most tuff is off white creame to tan and light gray. May contain
			abundant silt.
			Tuff 0.1' thick at 170.0
-			Tuff 0.1' thick at 170.8
			Tuff 1.4' thick at 170.9-172.3' nearly white in color - turbated at base Tuff 2.1' thick at 172.6 - 174.7 with minor shale
			Tuff 0.9 thick at 174.9-175.8
			Tuff 0.3 thick at 176.9-177.2
			Tuff 0.3' thick at 177.9 - 178.2
			Tuff 0.2' thick at 178.5 - 178.7
			Tuff 0.2' thick at 179.1-179.3
			Tuff 0.15' thick at 179.85-180.0
			Tuff 0.3' thick at 180.3-180.6 with minor shale
			Tuff 0.3' thick at 180.9-181.2
			Tuff 0.1' thick at 182.3
			Tuff 0.1' thick at 182.6

FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION		
			Tuff 0.3' thick at 182.0-182.3		
			Tuff 0.15' thick at 185.4-185.55		
			Tuff 0.1' thick at 186.0		
			Tuff 0.5' thick at 188.9 - 5189.4		
			-> 0.2' lost from 189.3 - 189.5		
			Tuff 0.4' thick at 191.5-191.9		
			Tuff 0.4' thick at 204.8 - BOTTOM OF HOLE		
					Town Process
			NH .VOR B - HUNGARD BEFORE HER		
	,				
				BEE E	

OIL-SHALE ASSAYS BY MODIFIED FISCHER RETORT METHOD

Samples from the U.S. Geological Survey's Corchole 78-6 drilled in sec. 11, T. 2 N., R. 99 W., Rio Blanco County, Colorado

	-		Yield o	of prod	uct		Specific
Depth		Weight	percent		Gal pe	er ton	gravity
			Spent	Gus +			of oil at
TOTAL TO	Oil	Water	shale	loss	0111/	Water	60°/60° F
34.0-35.0	1 /	1 0	05.0	0.0			
35.0-36.0	1.4	1.8	95.9	0.9	3.7a	4.3	0.000
	2.3	1.7	95.3	. 7	6.1	4.1	0.921
36.0-37.0	.9	3.3	95.2	. 6	2.3a	7.9	
37.0-38.0	2.3	2.7	94.1	. 9	6.0	6.5	.921
38.0-39.0	2.5	1.6	95.2	. 7	6.5	3.8	.914
39.0-40.0	2.1	1.6	95.6	. 7	5.3	3.8	.919
40.0-41.0	2.0	1.5	95.7	.8	5.2	3.6	.914
41.0-42.0	1.7	1.9	95.8	.6	4.5a	4.6	
42.0-43.0	1.6	1.5	96.3	.6	4.1a	3.6	
43.0-44.0	1.2	1.0	97.1	* *	3.1a	2.4	
44.0-45.0	1.8	1.5	95.7	1.0	4.6a	3.6	
45.0-46.0	2.7	1.4	94.7	1.2	7.1	3.4	.913
46.0-47.0	1.3	1.9	96.0	.8	3.4a	4.6	
47.0-48.0	1.4	1.3	96.8	.5.	3.5a		
48.0-49.0	.6	1.2	97.4	. 8	1.6a	2.9	
49.0-50.0	. 7	1.0	97.3	1.0	1.9a	2.4	
50.0-51.0	. 2	.9	98.6	.3	.6a	. 2.2	
51.0-52.0	.0	. 4	99.5	.1	No oil	.9	
52.0-53.0	. 3	.7	98.7	. 3	.8a	1.7	
53.0-54.0	.1	1.2	98.4	3	.4a	2.9	
54.0-55.0	.5	1.3	97.6	. 5	1.3a	3.1	
55.0-56.0	.1	1.0	98.5	. 4	.4a	2.4	
56.0-57.0	.5	1.3	97.7	.5	1.2a	3.1	
57.0-58.0	1.4	1.3	96.8	. 5	3.6a	3.1	
58.0-59.0	.9	1.3	97.3	.5	2.3a	3.1	
59.0-60.0	. 2	1.1	98.2	. 5	.5a	2.6	
60.0-61.0	. 7	1.6	97.2	. 5	1.8a	3.8	
61.0-62.0	.9	2.0	96.4	. 7	2.2a	4.8	
62.0-63.0	.1	1.9	96.9	1.1	.la	4.6	
63.0-64.0	. 9	2.2	96.1	. 8	2.4a	5.3	
64.0-65.0	0.1	1.4	97.8	0.7	0.2a	3.4	
65.0-66.0	. 8	2.4	96.1	.7	2.0a	5.8	
66.0-67.0	.5	1.8	97.5	.2	1.3a	4.3	
67.0-68.0	.1	2.3	97.1	.5	.2a	5.5	
68.0-69.0	.0	1.9	97.7	.4	.la	4.6	
69.0-70.0	.0	1.5	98.2	.3	Trace	3.6	
70.0-71.0	.0	1.8	97.9	. 3	Trace	4.2	
71.0-72.0	.0	2.3	97.3	.4	Trace	5.5	
72.0-73.0	.0	1.3	,98.2	. 5	Trace	3.1	
73.0-74.0	.1	1.9	97.7	.3	.la	4.6	
74.0-75.0	.0	2.1	97.6	. 3	Trace	5.1	
75.0-76.0	.0	4.2	95.4	. 4	Trace	10.1	
76.0-77.0	.0	2.2	97.3	.5	.la	5.3	
77.0-78.0	.0	2.0	97.6	.4	Trace	4.8	

NAMES AND PARTY OF PERSON OF PERSON PARTY PARTY.

samples from the Hall Louisian Course to Course 14-5 service the Course to C

			*

OLL-SHALE ASSAYS BY MODIFIED FISCHER RETORT MITHOD

Samples from the U.S. Geological Survey's Corehole 78-6 (Continued)

			V10-0	of prod			
		Weight	percent	or proc	The second secon		Specific
Depth			Spent	Gas +	Gal p	er ton	gravity
From To	011	Water	shale	loss	0i11/	Water	of oil at
124 0-121 0	5 4				011	Water.	60°/60° F
78.0-79.0	.0	2.2	97.4	.4	Trace	5.3	1- 0.911
79.0-80.0	.0	1.9	97.6	. 5	Trace	4.6	
80.0-81.0	.0	1.6	98.1	. 3	No oil	3.9	
81.0-82.0	.0	2.1	97.4	.5	Trace		
82.0-83.0	.0	2.1	97.6	. 3	Trace	5.1	
83.0-84.0	.0	1.4	98.1	.5	.la	5.0	
84.0-85.0	.0	2.0	97.3	.7		3.4	
85.0-86.0	.1	. 8	98.8	.3	No oil	4.7	
86.0-87.0	.0	. 8	98.8	. 4	.la	1.9	
87.0-88.0	.1	1.0	98.5		Trace	1.9	
88.0-89.0	. 3	. 7	98.5	-4	.la	2.4	
89.0-90.0	.6	. 5	98.5	.5 .	.8a	1.7	
90.0-91.0	.0	. 2	99.5	. 4	1.5a	1.2	
91.0-92.0	.0	.2		. 3	No oil	. 6	
92.0-93.0	.0	.2	99.5	. 3	No oil	. 5	,
93.0-94.0	. 2		99.6	. 2	No oil	. 4	
		. 4	99.0	. 4	. 5a	1.0	
94.0-95.0	1.0	0.4	98.1	0.5	2.5a	1.0	
95.0-96.0	1.4	. 7	97.3	.6	3.6a	1.7	
96.0-97.0	3.3	2.7	92.6	1.4	8.6	6.5	0.909
97.0-98.0	5.2	1.9	91.2	1.7	13.7	4.6	.910
98.0-99.0	3.8	1.5	93.4	1.3	10.1	3.6	.908
99.0-100.0	1.7	1.0	96.4	.9	4.6a	2.4	
100.0-101.0	2.8	1.4	94.9	.9	7.5	3.4	.906
101.0-102.0	4.2	2.2	92.2	1.4	11.1	5.3	.913
102.0-103.0	2.6	1.7	94.8	.9	6.8	4.1	.910
103.0-104.0	2.8	1.8	94.6	. 8	7.4	4.3	.911
104.0-105.0	2.6	1.4	95.3	.7	6.8	3.4	
105.0-106.0	2.4	1.1	95.7	. 8	6.5	2.6	.908
106.0-107.0	1.8	1.1	96.3	.8			.903
107.0-108.0	1.1	2.0	96.4	.5	4.8a	2.6	
108.0-109.0	1.2	1.7	96.4		2.9a	4.3	
109.0-110.0	.2	.6		. 7	3.2a	4.1	
110.0-111.0	.5		98.4	. 8	.6a	1.4	* *
111.0-112.0		. 7	98.3	.5	1.3a	1.7	
	. 3	.4	98.7	. 6	.7a	1.0	
112.0-113.0	. 7		97.9	.6	1.9a	1.9	
113.0-114.0	3	. 7	98.6	. 4	.9a	1.7	
114.0-115.0	1.0	.9	97.5	.6	2.6a	2.2	
115.0-116.0	1.2	1.3	96.9	. 6	3.2a	3.1	
116.0-117.0	1.1	1.1	97.3.	.5	2.9a	2.6	
117.0-118.0	.6	1.0	97.9	. 5	1.5a	2.4	
118.0-119.0	. 8	. 7	97.9	.6	2.1a	1.7	
119.0-120.0	. 8	1.3	97.3	.6	2.1a	3.1	
120.0-121.0	.9	2.1	96.5	.5	2.3a	5.0	
121.0-122.0	.6	2.5	96.5	.4	1.5a	6.0	
122.0-123.0	1.5	1.4	96.6	.5	3.9a	3.4	
123.0-124.0	1.9	1.3	96.1	.7	5.0a	3.1	
*.							

NAME AND POST OF PERSON OF PERSON PARTY AND PERSONS ASSESSED.

Section from the College of Section Section is described to

OLL-SHALE ASSAYS BY MODIFIED FISCHER RETORT MUTHOD

Samples from the U.S. Geological Survey's Corehole 78-6 (Continued)

		-		Yield	of produ	uct		
			Weight	percent			er ton	Specific
Depth				Spent	Cas +		er ton	gravity
From To		011	Water	shale	loss	011-/	Water	of oil at
124 0 125 0		0 0		01010		011	Water.	60°/60° F
124.0-125.0		2.8	1.5	94.9	0.8	7.3	3.6	0.911
125.0-126.0		1.5	1.2	96.6	. 7	3.9a	2.9	01711
126.0-127.0		1.4	1.2	96.9	.5	3.5a	2.9	
127.0-128.0		1.9	1.6	95.8	. 7	5.0a	3.8	
128.0-129.0		. 4	. 8	98.4	. 4	.9a	1.9	
129.0-130.0		. 5	. 8	98.3	.4	1.3a	1.9	
130.0-131.0		.4	.5	98.8	. 3	1.1a	1.2	
131.0-132.0		.5	.3	98.8	.4	1.2a		
132.0-133.0		. 3	. 2	98.6	.9	.7a	. 7	
133.0-134.0		.8	. 3	98.5	.4		. 5	
134.0-135.0		.5	.1	99.0		2.0a	. 7	
135.0-136.0		.5	.3	98.7	. 4	1.2a	. 2	
136.0-137.0		. 2	. 3		. 5	1.3a	.7	
137.0-138.0		. 7		99.2	. 3	.5a	. 7	
138.0-139.0		.5	. 4	98.1	. 8	2.0a	1.0	
139.0-140.0			. 4	98.7	.4	1.3a	1.0	
	,	. 2	. 4	99.0	. 4	.5a	1.0	
140.0-141.0		. 4	. 4	98.7	. 5	1.2a	1.0	
141.0-142.0		.9	. 5	98.0	. 6	2.4a	1.2	
142.0-143.0		1.2	. 8	97.0	1.0	3.1a	1.9	
143.0-144.0		. 1.7	1.3	96.4	.6	4.4a	3.1	
144.0-145.0		1.7	1.1	96.5	. 7	4.5a	2.6	
145.0-146.0		2.4	1.9	94.7	1.0	6.2	4.6	022
146.0-147.0		1.0	1.3	97.2	. 5	2.7a	3.1	.923
147.0-148.0		. 8	1.4	97.0	.8	2.1a	3.4	
138.0-139.0		.6	1.5	97.3	.6	1.5a		
149.0-150.0		. 8	1.4	97.1	. 7	2.1a	3.6	
150.0-151.0		. 8	1.5	97.2	.5		3.4	
151.0-152.0	***	.9	1.7	96.9		2.2a	3.6	
152.0-153.0		. 8	1.5	97.1	. 5	2.4a	4.1	
153.0-154.0		. 7	.8		.6	2.1a	3.6	
154.0-155.0		0.4	1.0	97.9	. 6	1.8a	1.9	
155.0-156.0		1.2	1.3		0.6	1.2a	2.4	
156.0-157.0		.3		96.5	1.0	3.2a	3.1	
157.0-158.0			.6	98.5	.6	.7a	1.4	
158.0-159.0		.7	1.0	97.4	. 9	1.8a	2.4	
		1.6	1.9	95.6	.9	4.2a	4.6	
159.0-160.0		.9	1.6	96.8	. 7	2.3a	3.8	
160.0-161.0		. 8	1.8	96.7	. 7	2.2a	4.3	
161.0-162.0		. 7	1.8	96.4	1.1	1.7a .	4.3	
162.0-163.0		.9	1.9	96.2	1.0	2.2a	4.6	
163.0-164.0		. 5	1.8	96.9	. 8 .	1.4a	4.3	
164.0-165.0		. 4	1.7	97.0	.9	1.1a	4.1	
165.0-166.0		. 4	1.4	97.4	. 8	1.2a	3.4	
166.0-167.0		. 2	1.2	97.8	.8	.6a	2.9	
167.0-168.0		.9	1.4	97.0	.7.			
168.0-169.0		.5	.9	98.0		2.3a	3.4	
169.0-170.0					. 6	1.3a	2.2	
103.0-170.0		. 7	. 7	98.0	. 6	1.9a	1.7	

NAMED AND ADDRESS OF PERSON AS SAUGH TO SAUGH THE PARTY OF THE PARTY O

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Oll-SHALE ASSAYS BY MODIFIED FISCHER RETORT MITHOD Samples from the U.3. Geological Survey's Corehole 78-6 (Continued)

		-	F1 /	Yzeld c	I prod	uci		Spiriter
Dep	th	-	Weight	percent		Gel pe	r ton	Specific gravity
TOR.	70	011	21-4	Spent	Gas +			of cil at
		011	Water	shale	loss	011-1	Water.	60 100
170.0-	171.0	. 3	. 4	98.9				
171.0-	172.0	.0	. 2	99.6	.4	.8a	1.0	
172.0-		.1	. 2	99.5	. 2	Trace	. 4	
173.0-		.0	. 2	99.4	.2	.3a	.5	
174.0-		. 2	. 2	99.4	4	Trace	.4	
175.0-		.3	. 2	99.2	. 2	.5a	.5	
176.0-		. 4	. 4	98.9	.3	.7a	.5	
177.0-		.3	. 4		. 3	1.0a	1.0	
178.0-		.1	. 2	98.9	. 4	.7a	1.0	
179.0-		.4	.6	99.0	. 7	.4a	. 5	
180.0-		.6		98.6	.4	1.0a	1.4	
181.0-		.3	. 3	98.8	. 3	1.4a	. 7	
182.0-		.5	- 4	98.8	.5	.9a	1.0	
183.0-			- 4	98.6	.5	1.3a	1.0	
184.0-		.4	.4	98.7	.5	1.1a	1.0	
185.0-		0.6	0.3	98.6	0.5	1.5a	0.7	
186.0-		. 3	. 2	99.1	.4	.8a	.5	
187.0-		.1	. 4	99.1	.4.	. 3a	1.0	
188.0-		. 2	. 3	99.1	.4	.5a	7	
		.4	. 4	98.6	.6	1.0a	1.0	
189.0-		. 7	.8	98.1	.4	1.9a	1.9	
190.0-		. 8	.6	.98.1	.5	2.1a	1.4	*
191.0-		.2	.4	98.8	.6	.6a	1.0	
192.0-		3	.7	.98.4	.6.	.9a	1.7	
193.0-		.6	.9	98.0	.5	1.5a	2.2	
194.0-		.6	. 8	98.1	.5	1.6a	1.9	
195.0-		. 8	.9	97.7	.6	2.1a	2.2	
196.0-		. 1.1	1.3	97.0	.6	2.9a	3.1	
197.0-		.9	1.3	97.2	.6	2.4a	3.1	
198.0-	199.0	. 4	1.2	97.6	.8	1.1a	2.9	
199.0-	200.0	.7	1.7	97.0	.6	1.9a	4.1	
200.0-		1.0	2.4	95.1	1.5	2.6a	5.8	
201.0-	202.0	.7	1.0	97.4	.9	1.8a	2.4	
202.0-	203.0	.9	2.3	95.7	1.1	2.3a		
203.0-	204.0	.9	1.7	95.8	1.6	2.4a	5.5	
204.0-	204.95	1.0	3.6	94.7	.7	2.4a 2.6a	8.6	

^{1/ &}quot;a"--indicates specific gravity estimated as 0.92.

THE PERSON NAMED IN COLUMN TWO IS NOT THE OWNER, NAMED AND POST OFFICE ADDRESS OF THE OWNER, NAMED IN COLUMN TWO IS NOT THE OWNER, NAMED IN COLUMN TWO IS NAMED IN COLUMN TWO IS NAMED IN COLUMN TRANSPORT TO THE OWNER, NAMED IN COLUMN TWO IS NAM

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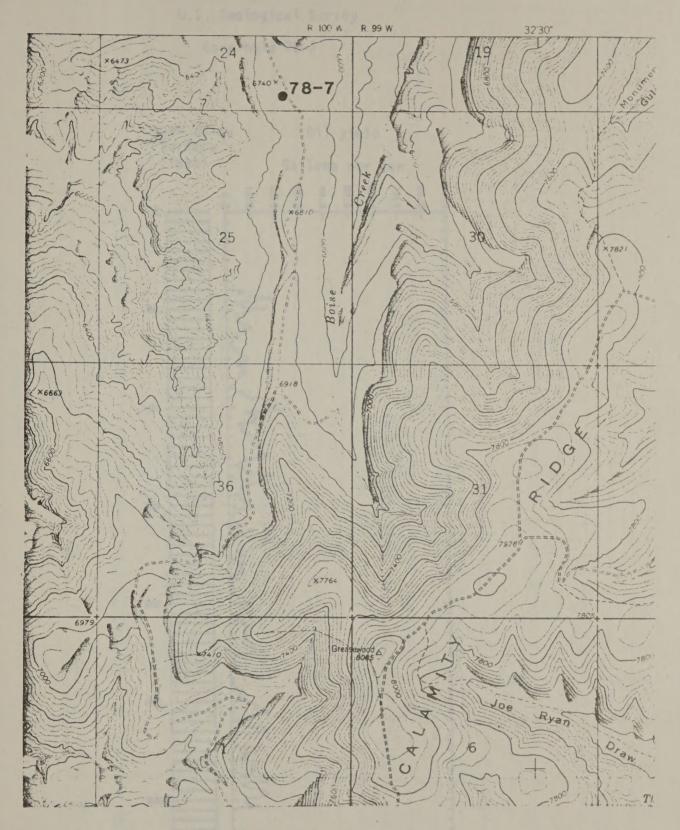


Figure 8.--Map showing location of core hole 78-7. Base from Calamity Ridge Quadrangle (1962). Scale 1:24,000.

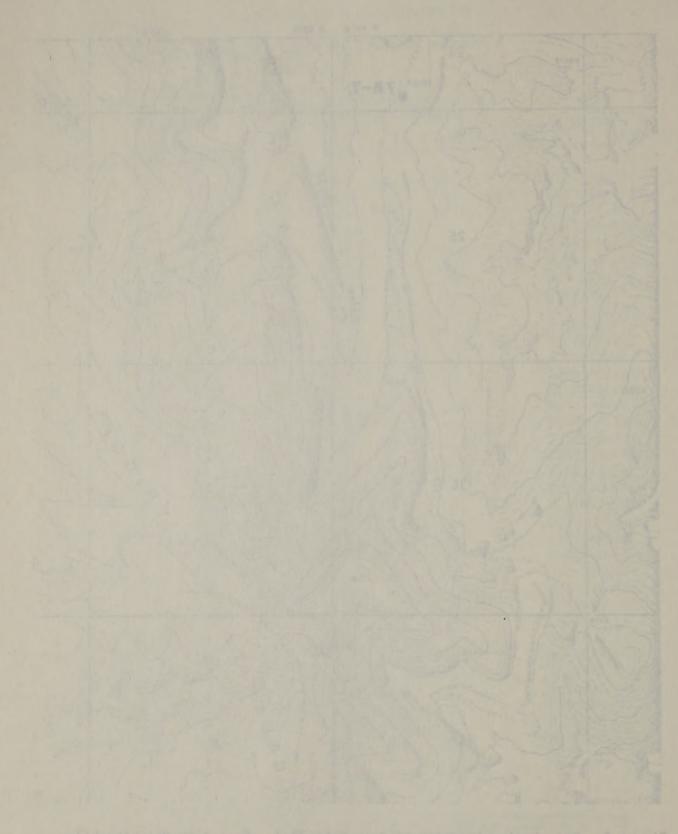
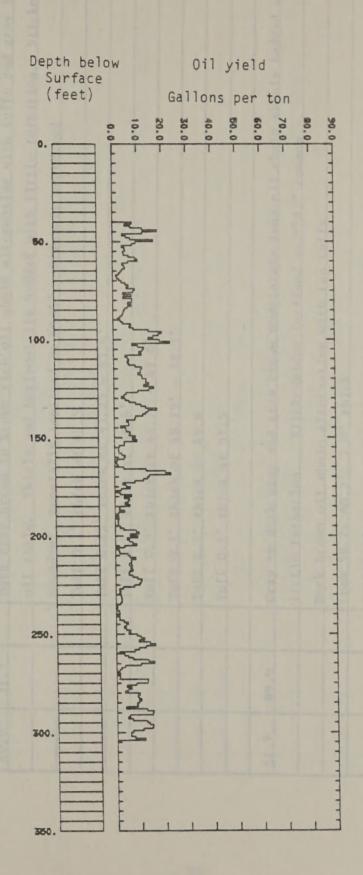


Figure 3. -- Nep showing total total of dres hale 75-7. Sees from Calendary Files-Quadrangle (1962). Scale-11-4.000.

U.S. Geological Survey

Core hole 78-7



U.S. September 2.U

FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION
40.0	51.7		Dark gray brown to brown rich oil shale alternating with tuffs and gray lean
			oil shale. Thinly and horizontally bedded with little turbation. Slickensides
			abundant, generally inclined at 45°. Slightly weathered
	-		Tuff 0.1' thick at 42.5
			Tuff 0.15' thick at 43.25 - 43.4'
			Tuff 0.1' thick at 44.6'
			Tuff 0.3' thick at 46.7' - 47.0'
			Tuff 0.1' thick at 48.15' - 48.3'
			Tuff 0.1' thick at 49.8
			Tuff 0.1' thick at 51.5
			CONTRACTOR DE LA CONTRACTOR DEL CONTRACTOR DE LA CONTRACTOR DE LA CONTRACTOR DE LA CONTRACT
51.7	89.9		Gray to dark gray and gray brown moderately lean oil shale thinly hedded with
			little turbation. Slickensides inclined at \$45° common
			Dark brown oil shale alternating with tan tuffs
			from 58.2- 60.2', 2.0' thick
			Tuff_0.1' thick at 60.0'
			Interval 65.0-68.2' highly shattered, probable core loss V1.2'
			Dark brown rich oil shale alternating with tan tuffs
			from 73.1 - 83.5, 10.4' thick
			THE RELEASE OF THE PARTY OF THE

office and of have

FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION
			Tuff 0.1' thick at 75.3'
			Tuff 0.2' thick at 76.6 - 76.8'
-			Tuff 0.1' thick at 78.4'
			Tuff 0.15' thick at 80.85'-81.0'
			Tuff 0.2' thick at 83.9-84.1
			Cray Jean Ball Works British - 170, 2. B. C. Blank
89.9	226.5		Dark gray brown and dark brown rich oil shale, thinly bedded with tuffs.
			ATTICLE CO. ATTICLE OF A SECURE .
			APPAY AS IN THE BUILDING THE RESPONDED TO THE RESPONDED T
			Tuff 0.15' thick at 106.1-106.25
			Tuff 0.2' thick at 106.6 - 106.8
			Tuff 0.2 thick at 109.0-109.2
			Tuff 0.1' thick at 111.1-111.2
			Tuff 0.2' thick at 112.8-113.0
			112.0' - 112.8' highly fractured
			116.1-118.8 tuffaceous zone with abundant intermixed tan tuff
			Tuff 0.1'thick at 125.6
			Tuff 0-2' thick at 129.5-129.7
			Tuff 0.15! thick at 133.7-133.85
			Tuff_0.15' thick_at_140.5=140.65
			Tuff 0.1' thick at 144.5'
			Tuff 0.2' thick at 145.0-145.2
			Turreno.2' thick at 148.3 - 148.5.

|--|

FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION
256.8	273.1		Abundant intermixed and layered tuff with oil shale
			259.4-262.3', 2.9' thick
			Tuff 0.2' thick at 259.4-259.6
			Gray oil shale with tuff
			Abundant Interlayered tuff
			Tuff 0.1' thick at 269.5
			Tuff 0.5' thick at 270,4-270.9
273.1	304.0		Rich dark brown oil shale with some gray brown leaner oil shale.
			Thinly and evenly bedded with little turbation
			Tuff 0.1' thick at 285.0
			Tuff 0.1' thick at 287.8
			Tuff 0.1' thick at 291.6
			Tuff 0.1' thick at 295.4
			Tuff 0.15 thick at 298.3-298.45
			Tuff 0.15' thick at 299.2-299.35
			Tuff_0_l' thick at 301_6
			Comments: Post consolidation faults, slickensides, and breceiated zones very
			common. Fault planes often undulatory, but most between 30° and 60° from
			borizontal. Most slickensides have movement striations parallel to din, rarely
			with lineations in other directions. Movement sense rarely discernable, but

FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION		
			both normal and reverse motions were seen. The rock wa	s difficult	to core due
			to its being tough but soft. The rock is rich in clay.		
			when wet.		
		- 1-			
					:
10					
				FIRE	152 11
				The state of the same of the Same State of the S	
			OHIERONE MENUSANDENDE MENUSANDE DE PERSONALES		
10			the terms are the		

Coretole 18-7 (Continued)

OIL-SHALE ASSAYS BY MODIFIED FISCHER RETORT METHOD

Samples from the U.S. Geological Survey's Corchole 78-7 drilled in sec. 24, T. 2 N., R. 100 W. Rio Blanco County, Colorado

				Bar an	The alle			
				fielo	of proce	151		Specific
I	epth	-	METALIT	percent		Gai pe	er inn	gravity
From	To	Oil	Water	Spent	1000	013-1/		of oil at
0				BIIGIE	loss	01!-	Water	60°/60° F
,	0.0-41.0	2.0	4.0	02.0	7 0	7.0	0.6	0.01/.
	1.0-42.0	3.0	4.0	92.0	1.0	7.9 5.0a	9.6	0.914
	2.0-43.0	2.7	3.9	92.4	1.0	7.3	9.3	.900
	3.0-44.0	4.7	3.6	90.6	1.1	12.1	8.6	.923
	4.0-45.0	7.0	3.3	87.4	2.3	18.2	7.9	.919
	5.0-46.0	4.5	5.0	88.8	1.6	12.2	2.0	.908
	6.0-47.0	1.5	2.0	95.8	.7	3.9a	4.8	. 700
	7.0-48.0	2.0	2.8	93.4	1.8	5.5	6.7	. 890
	8.0-49.0	2.7	3.8	92.6	.9	7.2	9.1	. 898
	9.0-50.0	6.3	4.4	87.1	2.2	16.6	10.5	.913
	0.0-51.0	3.6	4.2	90.1	2.1	9.4	10.1	.915
	1.0-52.0	3.0	4.0	91.4	1.6	7.9	9.6	.922
	2.0-53.0	1.4	4.0	93.5	1.1	3.7a	9.6	1744
	3.0-54.0	1.8	3.6	93.4	1.2	4.8a	8.6	
	4.0-55.0	1.9	3.8	93.2	1.1	5.1a	9.1	
	5.0-56.0	1.6	5.0	92.1	1.3	4.2a	12.0	
	6.0-57.0	1.7	5.0	92.1	1.2	4.5a	12.0	
	7.0-58.0	2.4	4.4	91.6	1.6	6.5	10.5	. 893
	8.0-59.0	3.5	3.8	90.4	2.3	9.2	9.1	.908
	9.0-60.0	3.8	3.8	90.9	1.5	10.1	9.1	.908
	0.0-61.0	2.3	3.6	92.5	1.6	6.2	8.6	.900
	1.0-62.0	1.5	4.5	92.6	1.4	3.8a	10.8	
	2.0-63.0	1.7	4.5	91.9	1.9	4.5a	10.8	
	3.0-64.0	1.9	3.5	93.1	1.5	5.0a	8.4	
	4.0-65.0	1.5	4.2	93.3	1.0	3.8a	10.1	
	6.0-67.0	1.0	4.0	93.8	1.2	2.5a	9.6	
	7.0-68.0	.5	2.9	95.7	.9	1.3a	7.0	
	8.0-69.0	.7	2.6	95.1	1.6	1.8a	6.2	
	9.0-70.0	1.0	4.5	93.0	1.5	2.7a	10.8	
	70.0-71.0	1.4	4.0	93.0	1.6	3.6a	9.6	
7	71.0-72.0	1.9	3.8	92.8	1.5	5.1a	9.1	
7	7.2.0-73.0	2.5	3.7	92.3	1.5	6.4	8.9	0.918
	73.0-74.0	2.1	2.7	93.9	1.3	5.6	6.5	.911
	74.0-75.0	3.4	3.4	91.3	1.9	8.9	8.1	.921
1337	75.0-76.0	3.1	3.2	91.5	2.2	8.2	7.7	.925
12-7	76.0-77.0	1.6	2.3	95.5	.6	4.1a	5.5	
1235	77.0-78.0	2.9	3.5	92.4	1.2	7.6	8.4	.919
1445	78.0-79.0	1.6	2.5	93.9	2.0		6.0	
	79.0-80.0	3.0	3.7	92.2	1.1	7.8	8.9	.907
8	30.0-81.0	2.9	2.8	93.3		7.8	6.7	.903
8	31.0-82.0	2.3	2.5	94.3	.9	6.0	6.0	.906
	32.0-83.0	2.8	3.8	92.2	1.2	7.5	9.1	.901
	33.0-84.0	2.2	3.2	93.5		5.9	7.7	.891
8	34.0-85.0	1.8	2.3	94.9	1.0	4.7a	5.5	

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OLL-SHALE ASSAYS BY MODITIED FISCHER RETORT MITHOD

Samples from the U.S. Geological Survey's Corehole 78-7 (Continued)

Nepth Prcn 70								
Section Sect			Weight	Derron:	of proc	THE RESERVE OF THE PERSON NAMED IN COLUMN TWO IS NOT THE PERSON NAMED IN COLUMN TWO IS NOT THE PERSON NAMED IN		Specific
85.0-86.0 1.7 2.6 94.9 8.8 4.3a 6.2 86.0-87.0 1.6 3.5 93.8 1.1 4.1a 8.4 88.0-88.0 1.4 2.8 94.0 1.8 3.7a 6.7 88.0-88.0 1.1 3.1 94.7 1.1 2.8a 7.4 89.0-90.0 7. 3.4 95.0 9 1.8a 8.1 91.0-92.0 1.5 3.5 93.9 1.1 3.9a 8.1 92.0-93.0 2.7 3.2 92.9 1.2 7.2 7.7 90.8 94.0-95.0 3.1 3.3 92.0 1.6 8.2 7.9 90.8 94.0-95.0 3.1 3.3 92.0 1.6 8.2 7.9 90.8 94.0-95.0 3.1 3.3 92.0 1.6 8.2 7.9 90.8 94.0-95.0 3.1 3.3 92.0 1.6 8.2 7.9 90.8 97.0-96.0 5.6 3.5 88.6 2.3 14.4 8.4 921 96.0-97.0 7.6 2.9 87.3 2.2 19.8 7.0 920 97.0-98.0 6.9 99.0-100.0 5.4 4.6 87.3 2.7 1.6 2.8 1.8 8.4 90.7 101.0-102.0 8.7 3.7 84.9 2.7 2.8 88.4 90.7 101.0-102.0 8.7 3.7 84.9 2.7 2.8 88.4 90.7 101.0-102.0 8.7 3.7 84.9 2.7 2.8 88.4 9.90 7.0 99.0-100.0 5.4 4.6 87.3 2.7 1.6 2.8 1.8 8.4 9.90 7.0 99.0-100.0 5.4 4.6 87.3 2.7 1.6 2.8 1.8 8.4 9.90 7.0 99.0-100.0 5.4 4.6 87.3 2.7 1.6 2.8 1.8 8.4 9.90 7.0 99.0-100.0 5.4 4.6 87.3 2.7 1.6 2.8 1.8 8.4 9.90 7.0 99.0-100.0 1.7 1.3 3.8 3.4 91.3 1.5 9.9 8.1 1.8 8.4 9.90 1.8 1.9 1.9 1.9 1.9 1.9 1.9 1.9	_			THE RESERVE OF THE PERSON NAMED IN COLUMN TWO IS NOT THE PERSON NAMED IN COLUMN TWO IS NAME	Can d	Lie J D	er ton	
85.0-86.0 86.0-87.0 1.6 3.5 93.8 1.1 4.1a 8.4 87.0-88.0 1.4 2.8 94.0 1.8 3.7a 6.7 88.0-89.0 1.1 3.1 94.7 1.1 2.8a 7.4 89.0-90.0 7. 3.4 95.0 9. 1.8a 8.1 90.0-91.0 1.5 3.5 93.9 1.1 3.4 94.0 1.5 3.0a 8.1 91.0-92.0 1.5 3.5 93.9 1.1 3.9a 8.4 92.0-93.0 2.7 3.2 92.9 1.2 7.2 7.7 908 94.0-95.0 3.1 3.3 92.0 1.6 8.2 7.9 908 95.0-96.0 5.6 3.5 88.6 2.3 14.4 8.4 907 98.0-99.0 6.9 3.5 87.3 2.2 19.8 7.0 99.0-100.0 5.4 4.4 87.2 2.3 16.2 10.5 99.0-100.0 5.4 4.6 8.7 3.7 84.9 2.7 2.30 8.9 101.0-101.0 7.1 3.5 84.9 2.7 2.30 8.9 102.0-103.0 102.0-103.0 2.9 3.9 90.8 2.7 3.4 89.1 2.0 1.6 3.5 84.9 2.7 2.30 8.9 0.906 101.0-101.0 7.1 3.5 84.9 2.7 2.30 8.9 0.906 102.0-103.0 2.9 3.9 90.8 2.7 2.30 8.9 0.906 102.0-108.0 4.7 3.8 84.9 2.7 2.30 8.9 0.906 102.0-108.0 4.7 3.8 84.9 2.7 2.30 8.9 0.906 102.0-108.0 4.7 3.8 84.9 2.7 2.30 8.9 0.906 102.0-108.0 4.7 4.8 8.9 1.1 1.1 1.2 1.1 1.2 1.1 1.3 1.4 1.8 4.1 1.4 1.8 4.1 1.8 4.1 1.9 1.8 1.9 1.8 1.8 1.1 1.9 1.9	From To	 011	Water			011-1	Water.	of oil at
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118.0-119.0 4.3 2.3 92.0 1.4 11.4 5.5 .905 119.0-120.0 4.3 4.5 89.3 1.9 11.6 10.8 .898 120.0-121.0 4.9 3.9 89.1 2.1 13.2 9.3 .898 121.0-122.0 4.9 3.7 89.5 1.9 13.0 8.9 .897 122.0-123.0 5.4 4.6 87.8 2.2 14.3 11.0 .904 123.0-124.0 4.6 4.0 88.6 2.8 12.2 9.6 .897 124.0-125.0 6.1 2.7 90.1 1.1 16.3 6.5 .895 125.0-126.0 5.4 3.1 89.4 2.1 14.3 7.4 .895 126.0-127.0 3.6 3.2 90.5 2.7 9.8 7.7 .885 127.0-128.0 1.9 4.0 92.6 1.5 4.9a 9.6 128.0-129.0 1.6 3.3 94.0 1.1 4.1a 7.9 129.0-130.0 1.2 2.7 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>								
119.6-120.0 4.3 4.5 89.3 1.9 11.6 10.8 .898 120.0-121.0 4.9 3.9 89.1 2.1 13.2 9.3 .898 121.0-122.0 4.9 3.7 89.5 1.9 13.0 8.9 .897 122.0-123.0 5.4 4.6 87.8 2.2 14.3 11.0 .904 123.0-124.0 4.6 4.0 88.6 2.8 12.2 9.6 .897 124.0-125.0 6.1 2.7 90.1 1.1 16.3 6.5 .895 125.0-126.0 5.4 3.1 89.4 2.1 14.3 7.4 .895 126.0-127.0 3.6 3.2 90.5 2.7 9.8 7.7 .885 127.0-128.0 1.9 4.0 92.6 1.5 4.9a 9.6 128.0-129.0 1.6 3.3 94.0 1.1 4.1a 7.9 129.0-130.0 1.2 2.7 95.2 .9 3.0a 6.5								
120.0-121.0 4.9 3.9 89.1 2.1 13.2 9.3 .898 121.0-122.0 4.9 3.7 89.5 1.9 13.0 8.9 .897 122.0-123.0 5.4 4.6 87.8 2.2 14.3 11.0 .904 123.0-124.0 4.6 4.0 88.6 2.8 12.2 9.6 .897 124.0-125.0 6.1 2.7 90.1 1.1 16.3 6.5 .895 125.0-126.0 5.4 3.1 89.4 2.1 14.3 7.4 .895 126.0-127.0 3.6 3.2 90.5 2.7 9.8 7.7 .885 127.0-128.0 1.9 4.0 92.6 1.5 4.9a 9.6 128.0-129.0 1.6 3.3 94.0 1.1 4.1a 7.9 129.0-130.0 1.2 2.7 95.2 .9 3.0a 6.5								.905
121.0-122.0 4.9 3.7 89.5 1.9 13.0 8.9 .897 122.0-123.0 5.4 4.6 87.8 2.2 14.3 11.0 .904 123.0-124.0 4.6 4.0 88.6 2.8 12.2 9.6 .897 124.0-125.0 6.1 2.7 90.1 1.1 16.3 6.5 .895 125.0-126.0 5.4 3.1 89.4 2.1 14.3 7.4 .895 126.0-127.0 3.6 3.2 90.5 2.7 9.8 7.7 .885 127.0-128.0 1.9 4.0 92.6 1.5 4.9a 9.6 128.0-129.0 1.6 3.3 94.0 1.1 4.1a 7.9 129.0-130.0 1.2 2.7 95.2 .9 3.0a 6.5				89.3	1.9	11.6	10.8	. 898
122.0-123.0 5.4 4.6 87.8 2.2 14.3 11.0 .904 123.0-124.0 4.6 4.0 88.6 2.8 12.2 9.6 .897 124.0-125.0 6.1 2.7 90.1 1.1 16.3 6.5 .895 125.0-126.0 5.4 3.1 89.4 2.1 14.3 7.4 .895 126.0-127.0 3.6 3.2 90.5 2.7 9.8 7.7 .885 127.0-128.0 1.9 4.0 92.6 1.5 4.9a 9.6 128.0-129.0 1.6 3.3 94.0 1.1 4.1a 7.9 129.0-130.0 1.2 2.7 95.2 .9 3.0a 6.5		4.9	3.9	89.1	2.1	13.2	9.3	. 898
122.0-123.0 5.4 4.6 87.8 2.2 14.3 11.0 .904 123.0-124.0 4.6 4.0 88.6 2.8 12.2 9.6 .897 124.0-125.0 6.1 2.7 90.1 1.1 16.3 6.5 .895 125.0-126.0 5.4 3.1 89.4 2.1 14.3 7.4 .895 126.0-127.0 3.6 3.2 90.5 2.7 9.8 7.7 .885 127.0-128.0 1.9 4.0 92.6 1.5 4.9a 9.6 128.0-129.0 1.6 3.3 94.0 1.1 4.1a 7.9 129.0-130.0 1.2 2.7 95.2 .9 3.0a 6.5	121.0-122.0	4.9	3.7	89.5	1.9	13.0	8.9	.897
123.0-124.0 4.6 4.0 88.6 2.8 12.2 9.6 .897 124.0-125.0 6.1 2.7 90.1 1.1 16.3 6.5 .895 125.0-126.0 5.4 3.1 89.4 2.1 14.3 7.4 .895 126.0-127.0 3.6 3.2 90.5 2.7 9.8 7.7 .885 127.0-128.0 1.9 4.0 92.6 1.5 4.9a 9.6 128.0-129.0 1.6 3.3 94.0 1.1 4.1a 7.9 129.0-130.0 1.2 2.7 95.2 .9 3.0a 6.5	122.0-123.0	5.4	4.6	87.8				
124.0-125.0 6.1 2.7 90.1 1.1 16.3 6.5 .895 125.0-126.0 5.4 3.1 89.4 2.1 14.3 7.4 .895 126.0-127.0 3.6 3.2 90.5 2.7 9.8 7.7 .885 127.0-128.0 1.9 4.0 92.6 1.5 4.9a 9.6 128.0-129.0 1.6 3.3 94.0 1.1 4.1a 7.9 129.0-130.0 1.2 2.7 95.2 .9 3.0a 6.5	123.0-124.0							
125.0-126.0 5.4 3.1 89.4 2.1 14.3 7.4 .895 126.0-127.0 3.6 3.2 90.5 2.7 9.8 7.7 .885 127.0-128.0 1.9 4.0 92.6 1.5 4.9a 9.6 128.0-129.0 1.6 3.3 94.0 1.1 4.1a 7.9 129.0-130.0 1.2 2.7 95.2 .9 3.0a 6.5	124.0-125.0							
126.0-127.0 3.6 3.2 90.5 2.7 9.8 7.7 .885 127.0-128.0 1.9 4.0 92.6 1.5 4.9a 9.6 128.0-129.0 1.6 3.3 94.0 1.1 4.1a 7.9 129.0-130.0 1.2 2.7 95.2 .9 3.0a 6.5								
127.0-128.0 1.9 4.0 92.6 1.5 4.9a 9.6 128.0-129.0 1.6 3.3 94.0 1.1 4.1a 7.9 129.0-130.0 1.2 2.7 95.2 .9 3.0a 6.5								
128.0-129.0 129.0-130.0 1.2 2.7 95.2 .9 3.0a 6.5								. 005
129.0-130.0 1.2 2.7 95.2 .9 3.0a 6.5								
1.8 3.8 92.6 1.8 4.65 9.1								
	130.0-131.0	1.5	3.8	92.6	1.8	4.03	9.1	

NAME OF TAXABLE PERSONS ASSESSED TO SERVICE PROPERTY.

secretary from the U.S. Gardenters Survey's Consulation

OLL-SHALE ASSAYS BY MODIFIED FISCHER RETORT MITHOD

Samples from the U.S. Geologica) Survey's Corehole 78-7 (Continued)

			. /0-/		rasa)		
	-		Yield	of proc	nei		-
Depth	-	Weignet	percent			per ton	Specific
From To	0/1		Spent	£85 +			gravity
10	Oil	Water	shale	loss	0i3-1	Water.	of oil at
131.0-132.0	2.3	2.0	0.				00 / 17 1
		3.9	91.6	2.2	6.1	9.3	0.895
132.0-133.0	3.3	3.5	91.7	1.5	8.8	8.4	.901
133.0-134.0	4.2	2.6	91.9	1.3	11.0	6.2	.907
134.0-135.0	4.9		90.1	1.7	12.9	7.9	.911
135.0-136.0	6.6	3.4	86.9	3.1	17.4	8.1	.911
136.0-137.0	5.2	3.8	88.9	2.1	13.8	9.1	.902
137.0-138.0	4.8	3.9	89.3	2.0	12.8	9.3	. 898
138.0-139.0	4.4	4.0	88.9	2.7	11.6	9.6	.904
139.0-140.0	3.3	3.8	90.7	2.2	8.7	9.1	.901
140.0-141.0	3.2	3.0	91.8	2.0	8.4	7.2	.901
141.0-142.0	1.9	3.8	92.1	2.2	5.0a	9.1	
142.0-143.0	2.1	3.8	92.0	2.1	5.8	9.1	. 884
143.0-144.0	2.2	4.2 .		2.2	6.0	10.1	.893
144.0-145.0	1.0	2.9	94.0	2.1	2.6a	7.0	
145.0-146.0	1.8	3.7	92.6	1.9	4.7a	8.9	
146.0-147.0	1.9	3.6	92.0	2.5	4.9a	8.6	
147.0-148.0	2.5	4.5	90.2	2.8	6.5	10.8	.921
148.0-149.0	2.4	5.3	90.9	1.4	6.1	12.7	.925
149.0-150.0	3.3	3.5	91.3	1.9	8.6	8.4	.921
150.0-151.0	2.8	3.3	91.4	2.5	7.3	7.9	.918
151.0-152.0	3.5	3.3	91.4	1.8	9.2	7.9	.912
152.0-153.0	1.5	4.0	93.1	1.4	3.9a	9.6	
153.0-154.0	1.6	3.7	93.2	1.5	4.1a	8.9	
154.0-155.0	. 7	4.2	93.6	1.5	1.9a	10.1	
155.0-156.0	.6	4.4	92.6	2.4	1.5a	10.5	
156.0-157.0	.6	4.6	92.8	2.0	1.7a	11.0	
157.0-158.0	.7	4.0	93.3	2.0	1.8a	9.6	
158.0-159.0	1.2	4.0	92.9	1.9	3.0a	9.6	
159.0-160.0	1.7	4.1	92.1	2.1	4.3a	9.8	
160.0-161.0	1.5	3.9	93.4	1.2	3.9a	9.3	
161.0-162.0		2.5	95.3	1.8	1.la	6.0	
162.0-163.0	.3	2.9	95.8	1.0	.7a	7.0	
163.0-164.0		3.7	94.6	1.3	1.0a	8.9	
164.0-165.0	.6	2.9	94.4	2.1	1.5a	7.0	
165.0-166.0	1.4	3.8	93.1	1.7	3.7a	9.1	
166.0-167.0	5.0	3.7	89.2	2.1	12.9	8.9	0.928
167.0-168.0	8.0	3.9	85.5	2.6	20.8	9.3	.921
168.0-169.0	8.7	3.7	85.1		22.9	8.9	.914
169.0-170.0	5.4	3.6	89.4		14.1	8.6	.920
170.0-171.0	5.1	4.5	88.7		13.3	10.8	.930
171.0-172.0	4.5	3.8	89.3		11.7	9.1	.924
172.0-173.0	3.0	4.0	91.8	1.2	8.2	9.6	. 890
173.0-174.0	1.2	4.2	93.2	1.4	3.3a	10.1	
174.0-175.0	1.7	3.7	91.9	2.7	4.7	8.9	.881

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and described the state of the

OLL-SHALE ASSAYS BY MODILIED FISCHER RETORT MITHOD

Samples from the U.S. Geological Survey's Corehole 78-7 (Continued)

		, (Concluded)										
		Weight	Yzeld	of proc	THE RESERVE OF THE PARTY OF THE		Specific					
Depth		MEIRIN	THE RESERVE AND ADDRESS OF THE PARTY OF THE		Gál p	er ton	gravity					
Free To	Oil	Water	Spent	loss	011-/		of oil at					
		3 5	011022	1055	011-	Water	60°/60° F					
175.0-176.0	2.3	4.7	91.0	2.0	6.3	11.3	.878					
176.0-177.0	1.0	3.4	94.4	1.2	2.6a	8.1	.070					
177.0-178.0	.3	2.8	95.8	1.1	.8a	6.7						
178.0-179.0	. 8	3.1	94.5	1.6	2.2a	7.4						
179.0-180.0	2.5	4.4	90.6	2.5	6.8		001					
180.0-181.0	1.5	4.4	91.8	2.3	3.8a	10.5	.881					
181.0-182.0	2.1	4.6	91.3	2.0		10.5						
182.0-183.0	2.0	4.1	91.3		5.9	11.0	.873					
183.0-184.0	1.6	4.6	90.6	2.6	5.4	9.8	. 869					
184.0-185.0	2.2	4.5		3.2	4.1a	11.0						
185.0-186.0	.8		91.3	2.0	6.0	10.8	. 865					
186.0-187.0		3.7	93.8	1.7	2.0a	8.9						
	.6	3.7	93.4	2.3	1.7a	8.9						
187.0-188.0	1.5	4.2	92.1	2.2	3.9a	10.1						
188.0-189.0	.5	3.5	94.3	1.7	1.4a	8.4						
189.0-190.0	. 3	3.5	94.8	1.4	. 8a	8.4						
190.0-191.0	. 2	3.3	95.0	1.5	.6a	7.9						
191.0-192.0	0.6	2.8	94.6	2.0	1.5a	6.7						
192.0-193.0	. 5	2.9	94.6	2.0	1.2a	7.0						
193.0-194.0	. 5	2.4	96.2	.9	1.3a	5.8						
194.0-195.0	.5	3.4	94.7	1.4	1.2a	8.1						
195.0-196.0	. 8	3.1	94.5	1.6	2.1a	7.4						
196.0-197.0	1.3	3.4	93.1	2.2	3.5a	8.1						
197.0-198.0	3.3	3.8	90.8	2.1	8.6	9.1	0.910					
198.0-199.0	3.8	3.7	90.3	2.2	9.8	8.9	.922					
199.0-200.0	2.3	4.5	91.8	1.4	6.1	10.8	. 896					
200.0-201.0	3.5	3.4	91.0	2.1	9.2	8.1	.913					
201.0-202.0	1.8	3.6	93.0	1.6	4.8a	8.6						
202.0-203.0	2.1	3.5	92.6	1.8	5.8	8.4	.883					
203.0-204.0	2.6	3.9	91.2	2.3	7.1	9.3	.895					
204.0-205.0	3.3	4.5	89.9		8.7							
205.0-206.0				2.3		10.8	.897					
206.0-207.0	1.4	3.2	94.4	1.0	3.7a	7.7						
207.0-208.0	. 3	2.5	96.4	.8	.7a	6.0						
	.5	2.2	96.1	1.2	1.4a	5.3						
208.0-209.0	. 6	2.5	95.2	1.7	1.7a	6.0						
209.0-210.0	1.9	3.2	91.7	3.2	5.0a	7.7						
210.0-211.0	2.2	3.2	92.7	1.9	5.9	7.7-	.889					
211.0-212.0	3.1	3.3	91.5	2.1	8.2	7.9	.898					
212.0-213.0	2.4	3.5	92.2	1.9	6.4	8.4	.891					
213.0-214.0	2.4	3.4	92.1	2.1	6.5	8.1	.893					
214.0-215.0	2.0	3.3	92.8	1.9	5.5	7.9	. 893					
215.0-216.0	2.5	2.7	93.3	1.5	6.8	6.5	.890					
216.0-217:0	2.3	2.6	93.1	2.0	6.2	6.2	.888					
217.0-218.0	2.6	3.0	92.6	1.8	7.0	7.2	.891					
218.0-219.0	2.0	2.7	94.2	1.1	5.5	6.5	. 881					
219.0-220.0	2.0	2.7	93.4	1.9	5.4	6.5	.881					
220.0-221.0	2.5	2.5	93.7	1.3	6.9	6.0	.882					
			, , , ,	1.0	0.7	0.0	1 U C 2					

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pleased after the bull designated that and anoth adopted

						209.0-210.0 210.0-211.0 211.0-211.0 211.0-211.0 211.0-211.0

OIL-SHALE ASSAYS BY MODIFIED FISCHER RETORT MITHOD

Bemples from the U.S. Geological Survey's Corehole 78-7 (Continued)

		Yield of product									
		Weight	percen:			Specific					
Depth			Spent	Gas +	[e] pe	T LOT	gravity				
From To	011	Water	shale	loss	011-1	Water	of oil at				
					011	MULES	60°/60° F				
221.0-222.0	3.3	2.7	92.6	1.4	8.9	6.5	0.889				
222.0-223.0	4.0	3.1	90.5	2.4	10.7	7.4					
223.0-224.0	3.8	3.2	90.2	2.8	10.3	7.7	.894				
224.0-225.0	3.7	3.3	90.8	2.2	9.8	7.9	.897				
225.0-226.0	2.8	3.9	91.2	2.1	7.6	9.3	. 896				
226.0-227.0	1.1	3.9	93.4	1.6	3.0a	9.3	. 893				
227.0-228.0	.5	2.5	95.8	1.2	1.4a	6.0					
228.0-229.0	. 7	3.5	93.2	2.6	1.9a	8.4					
229.0-230.0	.5	2.7	95.2	1.6	1.3a	6.5					
230.0-231.0	.8	3.0	94.3	1.9	2.1a	7.2					
231.0-232.0	.9	3.2	94.1	1.8	2. 3a						
232.0-233.0	.9	2.8	94.6	1.7	2.4a	7.7					
233.0-234.0	.9	2.6	95.4			6.7					
234.0-235.0	.7	2.7	95.5	1.1	2.4a	6.2					
235.0-236.0	. 2	2.2	96.1	1.1	1.8a	6.5					
236.0-237.0	.2	2.2	96.7	1.5	.5a	5.3					
237.0-238.0	.2	2.3	96.6	.9	.5a	5.3					
238.0-239.0	.5	2.2	96.0	.9	.4a	5.5					
239.0-240.0	.5	1.9	96.2	1.3	1.3a	5.3					
240.0-241.0	. 2	1.4	97.1	1.4	1.4a	4.6					
241.0-242.0	.5	2.1	95.9	1.3	.6a	3.4					
242.0-243.0	.6	2.3	95.4	1.5	1.4a	5.0					
243.0-244.0	1.2	2.9	93.9	2.0	1.4a	5.5					
244.0-245.0	1.9	3.7	91.6		3.2a	7.0					
245.0-246.0	1.6	3.4	93.5	2.8	4.8a	8.9					
246.0-247.0	1.2	3.2	93.9	1.5	4.0a	8.1					
247.0-248.0	1.6	3.1	93.2	1.7	3.2a	7.7					
248.0-249.0	2.2	2.7	93.6	2.1	4.la	7.4	005				
249.0-250.0	1.9	2.6		1.5	5.8	6.5	.896				
250.0-251.0	3.2	3.0	93.4	2.1	5.1a	6.2	000				
251.0-252.0	3.8	2.8	90.7	2.0	8.6	7.2	.898 0.897				
252.0-253.0		3.1	90.4	2.2	11.5	7.4	.886				
253.0-254.0	3.5	3.3	91.3			7.9	.896				
254.0-255.0	5.2	2.8	90.2		13.8	6.7	.900				
255.0-256.0	6.1	2.8	89.5		15.9	6.7	.911				
256.0-257.0	4.6	3.2	89.5	2.7		7.7	.915				
257.0-258.0	3.4	3.2	91.6	1.8	9.3	7.7	.884				
258.0-259.0	2.7	3.8	91.8	1.7	7.4	9.1	. 881				
259.0-260.0	.5	1.6	95.8	2.1	1.2a	3.8	. 001				
260.0-261.0	1.3	2.9	94.3	1.5	3.3a	7.0					
261.0-262.0	1.9	3.1	93.4	1.6	4.8a	7.4					
262.0-263.0	2.6	3.5	92.0	1.9	6.8	8.4	.911				
263.0-264.0	5.0	3.6	89.3	2.1	13.1	8.6	.919				
264.0-265.0					15.5	8.9	.927				
204.0-203.0	6.0	3.7	87.8	2.5	77.7	0.7	1761				

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Oll-Shalf ASSAYS BY MODIFIED FISCHER RETORT MITHOD Samples from the U.S. Geological Survey's Corehole 78-7 (Continued)

		Yaeld of product						
Depth		Weight perce			Gal per ton			
			Spent	Gas +			gravity	
From To	Oil	Water	shale	loss	013-1/	Water.	of oil at 60°/60° F	
265.0-266.0	3.8	4.0	90.2	2.0	10.0	9.6		
266.0-267.0	1.3	4.0	93.2	1.5	3.5a	9.6	.905	
267.0-268.0	.8	3.7	94.0	1.5	2.0a			
268.0-269.0	.5	3.0	94.6	1.9	1.3a	8.9		
269.0-270.0	.3	1.8	97.1	.8		7.2		
270.0-271.0	.1	1.2	98.0	.7	.7a	4.3		
271.0-272.0	.5	2.6	95.3	1.6	. 3a	2.9		
272.0-273.0	.5	1.8	95.9	1.8	1.4a	6.2		
273.0-274.0	4.9	3.3	90.0	1.8	1.2a 12.8	4.3	01/	
274.0-275.0	4.8	3.4	89.7			7.9	.914	
275.0-276.0	2.9	3.0	92.9	2.1	12.6	8.1	.910	
276.0-277.0	1.5	2.9	94.4	1.2		7.2	.882	
277.0-278.0	2.2	3.4	92.1		4.0a	7.0	0.00	
278.0-279.0	1.7	3.2	93.5	2.3	6.0	8.1	.880	
279.0-280.0	1.3	3.3	93.6	1.6	4.5a	7.7		
280.0-281.0	3.5	3.9	90.4	1.8	3.4a	7.9	202	
281.0-282.0	3.2	3.8	91.2	2.2	9.4	9.3	.892	
282.0-283.0	3.4		90.8	1.8	8.6	9.1	0.897	
283.0-284.0	3.8	3.4	90.8	2.4	8.9	8.1	.921	
284.0-285.0	3.5	4.0		1.9	10.0	8.4	.922	
285.0-286.0	3.0	3.1	90.9	1.6	9.1	9.6	.916	
286.0-287.0	3.2	3.8	90.0	1.9	8.1	7.4	.897	
	1.4	3.5	93.9	3.0	8.5	9.1	.892	
287.0-288.0				1.2	3.6a	8.4	0.00	
288.0-289.0	4.7	3.2	90.5	1.6	12.3	7.7	.920	
289.0-290.0	5.7	3.7	88.4	2.2	14.9	8.9	.919	
290.0-291.0	5.5	3.6	88.6	2.3	14.6	8.6	.899	
291.0-292.0	2.0	3.2	92.9	1.9	5.2	7.7	.906	
292.0-293.0	1.7	. 3.8	93.1	1.4	4.42	9.1		
293.0-294.0	2.4	3.9	91.6	2.1	6.4	9.3	.915	
294.0-295.0	4.7	3.4	89.8	2.1	12.3	8.1	.911	
295.0-296.0	5.0	2.9	90.1	2.0	13.2	7.0	.904	
296.0-297.0	5.5	3.5	88.8	2.2	14.7	8.4	.893	
	5.4				14.5		. 899	
	4.0	2.7	90.8	2.5	10.7	6.5		
299.0-300.0	2.4	3.2	93.0	1.4	6.4	7.7	. 897	
300.0-301.0	2.1	3.5	92.9	1.5	5.6	8.4		
301.0-302.0	2.1	2.0	93.8	2.1	5.6	4.8	.907	
302.0-303.0	2.8	3.6	91.9	7.	1.3	8.0	.903	
303.0-304.0	4.4	3.0	91.2	1.4	11.4	7.2	.921	

^{1/ &}quot;a"--indicates specific gravity estimated as 0.92.

DOWNER THOUSE MANDELS HAT THE PARTY HAVE AND ADDRESS OF THE PARTY

states from the U.S. Cartesteel Survey's Coretain

					263.0
					0.386
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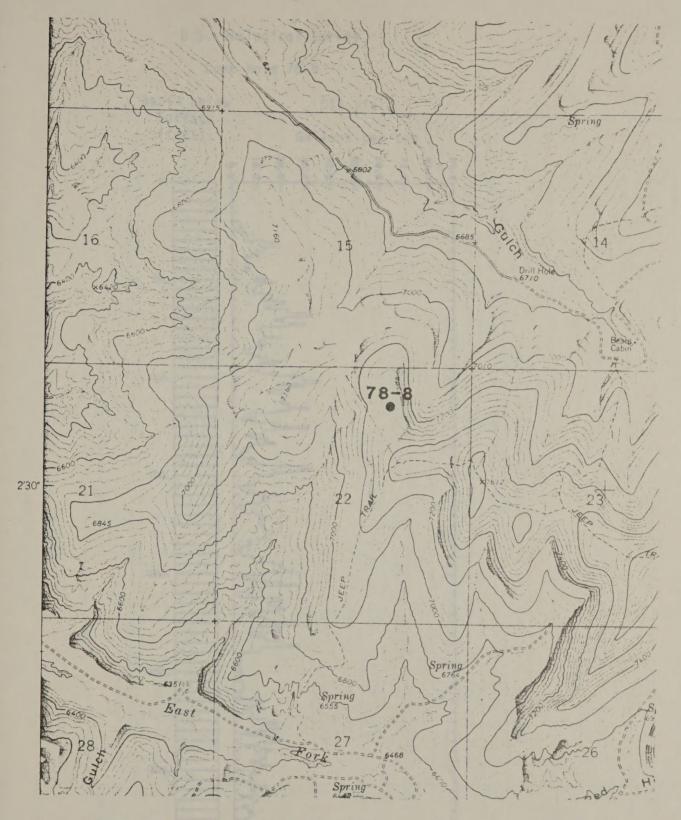
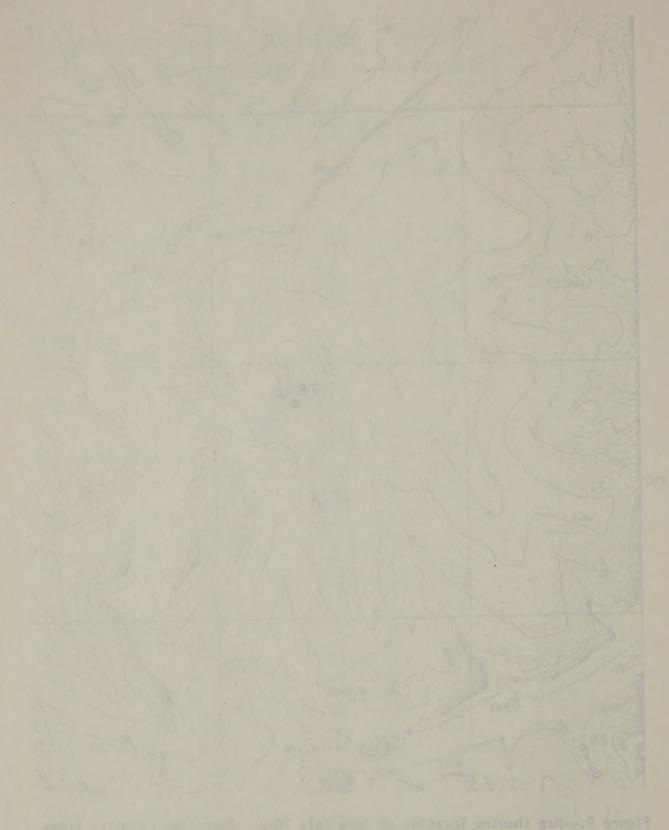
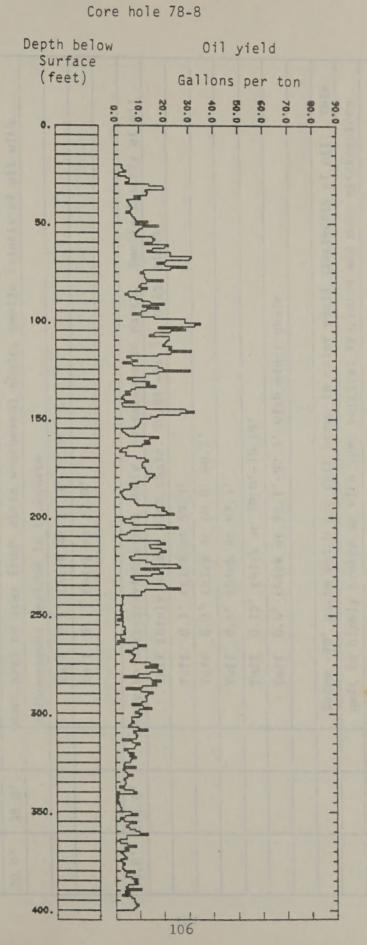


Figure 9.--Map showing location of core hole 78-8. Base from Calamity Ridge Quadrangle (1962). Scale 1:24,000.



Floure 9.-- Hap showing tocaston of core tote food. Execution country Floure Quadrangle (1962). State 1:24,000.

U.S. Geological Survey



Corehole 78-8

Logged by Kurt Hollocher

FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION
20.0'	38.0'		Dark gray to gray (rust where weathered) shale, smells faintly of oil with
			carbonaceous residue in fractures.
			Tuff 0.2' thick at 21.3'-21.5'
			Tuff 0.1' thick at 37.8'
38.0'	276.8'		Gray to dark-grayish brown shale, calcareous in parts. Smells faintly of oil
			Tuff thinly bedded with shale. 50.85'-51.3', 9.45' thick
			Tuff 0.1' thick at 59.3'
			Tuff 0.2' thick at 60.0'-60.2'
			Tuff 0.1' thick at 67.3'
			Tuff 0.15' thick at 70.0'-70.15'
			Tuff 0.4' thick at 92.1'-92.5' with minor shale
			Below ~70' parts which are dark brown in color smell distinctly of oil. This
			unit is highly broken up with some vertical fractures and many slickensides
			with brecciated zones. Fault striations occur both parallel and perpendicular
			to the dip, which can be from horizontal to vertical.

Perfect by Ent; Roll

FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION
			Tuff 0.1' thick at 104.8'
			Tuff 0.1' thick at 121.4'
			Tuff 0.3' thick at 132.2'-132.5' with minor shale
			Below ~135' the shale is getting soft and greasy in texture, indicating
			abundant clay.
			Tuff 0.1' thick at 165.3'
			Tuff 0.1' thick at 183.2'
			Tuff 0.2' thick at 186.2'-186.4'
			-0.71 philips are lifered
			Barrelon B. 22 - Chile S. D. 203 - N 161 - 2
			Service and Arabi Chile at March 1962.
			Control and the control of the contr
			Currents 0.5" shield of 205.0" 285.5"
			Controvendes Co. St. and govern 200-00" - 200-00" .
			THE PLANE AND ADDRESS OF THE PARTY OF THE PA
	AND THE PERSON NAMED IN COLUMN TWO		
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FROM	TO	THICK-	LITHOLOGIC DESCRIPTION
			Tuff 0.2' thick at 197.8-198.0' with oil staining
			Tuff 0.15' thick at 234.75'-234.9'
			Drilling was switched at 238.0' from 2^{l_5} " (H) core to 1^{l_5} " (NQ) core using a
			colloid based mud, with the 312" drill pipe used as casing.
			THE OUT OF THE RESPONSE
			The state of the s
	-		Ostrocod fossils beginning at 259.7', rich beds
			>0.1' thick are listed
			Ostrocods 0.2' thick at 261.0'-261.2'
			Ostrocods 0.1' thick at 262.2'=262.3'
			Ostrocods 1.8' thick at 262.8'-264.6' (~50% shale)
			Ostrocods 0.5' thick at 265.0'-265.5'
			Ostrocods 0.5' thick at 266.0'-266.5'
			Tuff 0.1' thick at 273.4'
			The second of th
			Albertone U.T. Bules of MARK District
			Bery to breed measured to characterists to an entiry header with factors
	-		Fruchetten. Does comes although provider leads that in technology in
			The allies of the company of the next with the company of the comp
			THE STATE OF THE S
		A LONG AND ADDRESS OF THE PARTY	1 decade and the state of the s

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FROM	то	THICK- NESS				ITHOLOGIC DESCRIP	TION		
				Tuff 0.15' tl	ilck at 31	7.9-318.05'			
				Limestone 0.2	thick at	318.6'-318.8'	Dirty	w/ostrocods	
				Limestone 0.1	thick at	319.2'	Dirty		
				Limestone 0.3	thick at	320.71-321.01	Dirty		
				Limestone 0.1	thick at	321.4'	Dirty		
				Limestone 0.2			Dirty		
				Limestone 0.1	thick at	322.3'	Dirty		
				Limestone 0.1			Dirty	w/ostrocods	
			15381	Limestone 0.1			Dirty	w/ostrocods	
			The state of	Limestone 0.2			Dirty	w/ostrocods	
				Limestone 0.3			Dirty		
				Limestone 0.1'			Dirty		
				Limestone 0.1			Dirty		
				Limestone 0.1'			Dirty		
	-			Limestone 0.1'			Dirty		
				Limestone 0.4'			Dirty		
				Limestone 0.3'			Dirty	w/ostrocods with 1	Imestone
						340.05'-340.2'	Dirty		pebb1
				Limestone 0.1'				w/ost.rocods	
				Limestone 0.2'			Dirty	w/ostrocods	
		C.	Water	Limestone 7.6'				w/ostrocods	
		13.0	unatea	Limestone 0.3'			Dirty		
	-			Linescone 0. J	CHECK AL	The second secon			

FROM	то	THICK- NESS		LITHOLOGIC DESCRIPT	ION
				Limestone 0.2' thick at 352.7'-352.9'	Dirty
				Limestone 0.3' thick at 353.7-354.0'	Dirty
				Limestone 0.1' thick at 355.8'-355.9'	Dirty
				Limestone 0.15' thick at 356.15-'356.3'	Dirty
				Limestone 0.35' thick at 356.6'-356.95'	Dirty
				Limestone 0.2' thick at 360.2'-360.4'	Dirty
				Limestone 0.2' thick at 361.7'-361.9'	Dirty
				Limestone 0.2' thick at 362.0'-362.2'	Dirty
Due u	sinki	g of	312"	Limestone 0.1' thick at 362.5'	Dirty
	to top			Limestone 0.4' thick at 364.0'-364.4'	Dirty
	352'.	MITEI	corrug	Limestone 0.3' thick at 368.0'-368.3'	Dirty w/ostrocods
			Louis	Limestone 0.15' thick at 371.05'-371.2'	Dirty
				Limestone 0.15' thick at 372.45'-372.6'	Dirty
At 37	2' the	1' ac	d on	Limestone 0.3' thick at 374.5'-374.8'	Dirty
	on of ca			Limestone 0.2' thick at 381.0'-381.2'	Dirty
	on and			Limestone 0.1' thick at 383.8'	Dirty
241'.				Limestone 0.6' thick at 388.0'-388.6'	Dirty
				Limestone 0.2' thick at 390.1'-390.3'	Dirty
				Limestone 0.6' thick at 392.1-392.7'	Dirty w/ostrocods
				Limestone 0.6' thick at 399.8'-400.4-	Dirty w/ostrocods
				aturne Med. Shales sussell are exhalt to	with detroces deformation
				residues - Labore results assessed to be the	
				Application of Commission of Commission and Commission of the Commission of Commission	

FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION
	1-1-1-1		Limestone 0.1' thick at 403.2' with ostrocods
	*		Limestone 0.2' thick at 403.3'-403.5' with ostrocods
			Limestone 0.2' thick at 403.9'-404.1' with ostrocods
			Limestone 0.15' whick at 404.2'-404.35' with ostrocods
			Limestone 0.2' thick at 405.7'-405.9' with ostrocods
			Limestone 0.15' thick at 410.0'-410.15' with ostrocods
			Limestone 0.6' thick at 410.7'-411.3' Dirty
413.3'	434.6'		Brown to gray lean oil shale with and without carbonate parts have intermixed
			ostrocods and larger fossils of snails and bivalves. Splits with larger fossils
			marked by black "X" on core. Massive limestone >0.1' thick noted. Silty in
			lower 5'.
	sinking		
	ngth was tal casi		
242'			Limestone 0.2' thick at 417.4'-417.6'
			Diamond bit changed at 432.1'
434.6'	452.9'		Fine white to gray calcite cemented quartz sandstone, mixed with shale in places
			also Interbedded. Shaley segments are calcitic, with ostrocods and carbonized
			plant remains. Larger fossils common in parts.

				-							

FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION
452.9'	454.6'		Massive shale (claystone), dark gray and relatively soft and brittle largely
			without carbonate with many slickensides. May be fault gouge.
454.6'	458.1'		Gray to dark-gray calcitic shale
458.1'	466.1'		Light-gray silty clayey limestone or calcite rich dirty siltstone. Fossils
			uncommon.
466.1'	467.71		Gray to brown and black calcitic shale, thinly bedded with siderite (?) nodules.
			No oil smell.
467.7	475.1'		Medium-grained gray to white well-sorted moderately well-rounded quartz
			sandstone. Massive with calcite and silica cement, soft in upper 1' where leache
			Some parts water saturated. Less well sorted in lower 2'.
			By 470' water loss rate down the drill hole had Increased to about
			15 ft. ³ hr. ⁻¹ .
475.1'	491.3'		Calcite-rich claystone, clayey siltstone, and fine-grained poorly sorted
			sandstone, light gray to gray, interbedded with poorly defined horizons on a
			scale of about 1'. Fossils or calcitic nodules common. Lowest 0.5' is very
	Special Control of the Assertation Special Control		dark brown non-calcitic shale.

FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION
491.4'	495.8		Sandstone, medium to very coarse grained, poorly sorted with high angle bedding
			dips, possibly cross bedding. Tan to light gray with calcite and silicla cement.
			Parts are water saturated. Lowermost 2' mixed and bedded with shale and
			carbonaceous material.
			Completence Continued de Continue de continue de la
495.8'	505.1'		Shale gray to dark brown, silty and largely calcitic. Siderite nodule at 496.9'.
.,,,,,,			Fossiliferous units with bivalve shells at 497.2'-497.4', 0.2' thick.
			499.3'-500.6', 1.3' thick
			From an outgroup stones of about 46%
			At the second the last about a second to see the second again to be a second again.
505.1'	507 41		Sandstone, medium grained light gray, massive, well sorted with calcite cement.
303.1	307.4		
507.41	557.91		Light-gray calcareous claystone with sandy units interbedded on a scale of about
307.4	,,,,,		a foot. Fossils common. Dark-brown to gray and light-gray calcitic shale and
			claystone from 525.9' to 533.6', 7.7' thick.
			Sandstone unit, white to light gray, interbedded with minor shale, fine
			grained with calcite cement. 535.0'-542.5', 7.5' thick.
			gramma week and the second sec
			W/19.57 _ 0.5%* shifek
			At 558.3', the 3" casing was advanced to 248' and additional pipe added on top
			to remedy casing sinking beyond seals.
C INCOME AND DESCRIPTION OF THE PARTY OF THE			
	A CAMPAGE AND ADDRESS OF THE PARTY OF		

FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION
557.9'	575.4'		Gray shale, calcitic, medium to thinly bedded with some turbation. Snails and
			bivalve fossils common, ostrocods intermixed and abundant.
			service and subservices plant to the subservice of the subservice
575.4'	605.5'		Calcitic gray to light-gray claystone, shale, siltstone, and poorly sorted
			sandstone interbedded and mixed. Fossiliferous with ostrocods and larger
			fossils.
			After a four-day break, water remained in the hole to a depth of about 120',
			from an original depth of about 40'.
			At ~450' depth the hole had caved in and had to be reamed upon reinsertion of the drill pipe to the hole bottom at 602.1'.
			Light-gray to white fine-grained moderately-sorted calcite cemented sandstone
			interbedded with calcitic clayey siltstone or mudstone.
			At 602.1'-604.0', 1.9' thick.
			by ~615' water loss rate down the drill hole has increased to ~20 ft. 3 hr1.
			Fine-grained poorly sorted sandstone, gray with calcite cement, from 604.95'-
			605.5', 0.55' thick.

Coretors 18-8 (Constance)

FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION	
605.5'	630.0'		Gray to dark-gray calcitic shale, several zones	
			gray to black and smell faintly of oil. Thinly bedded with little turk	ation.
			ostrocods and other fossils common particularly below 611.7'.	
			Due to the 3½" casing sinking below its seals, it was advanced to 251'	and a 5'
			section added on top.	
		-	TERROR TO THE PROPERTY OF THE	
			Noncalcareous gray claystone at 617.4'-617.9', 0.5' thick.	
	8 2 2			
		7 In 60		
			PATEUR DE LE LE DE	
			282828282828282828282828282828282828	
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Samples from the U.S. Geological Survey's Corchole 78-8 drilled in sec. 22, T. 1 N., R. 100 W., Rio Blanco County, Colorado

								Special .
7.0			be inte	Yield o	i prod	The second secon		Specific
De	pth	· Continue specie	METAILE	percent		Gal p	er ton	gravity
From	To	Oi1	Water	Spent	loss +	0132/		of nil at
				21102 2 2	1088	011-	Water	60°/60° F
20.0	0-21.0	1.2	5.2	92.4	1.2	3.2a	12.5	020
21.0)-22.0	1.1	3.7	94.3	.9	2.9a	8.9	.920
22.0	-23.0	1.4	5.5	92.0	1.1	3.6a	13.2	.920
23.0	-24.0	1.9	5.0	92.0	1.1	4.8a	12.0	.920
24.0	-25.0	.7	5.5	92.9	.9	1.9a	13.2	.920
25.0	-26.0	.6	5.5	92.4	1.5	1.6a	13.2	. 920
26.0	-27.0	1.9	5.2	91.7	1.2	4.9a	12.5	.920
	-28.0	2.3	5.0	91.6	1.1	6.2	12.0	.886
28.0	-29.0	2.3	4.5	91.9	1.3	6.1	10.8	.894
	-30.0	1.7	6.0	91.0	1.3	4.5a	14.4	.920
	-31.0	5.4	4.4	88.4	1.8	14.2	10.5	.909
	-32.0	7.6	4.0	85.7	2.7	19.9	9.6	.915
	-33.0	7.7	3.2	85.3	3.8	20.2	7.7	
	-34.0	4.8	2.9	90.6	1.7	12.6	7.0	.920
	-35.0	5.1	3.6	88.7	2.6	13.6	8.6	.909
	-36.0	4.9	3.9	89.3	1.9	13.2	9.3	.904
	-37.0	3.0	2.7	93.2	1.1	8.1		. 896
	-38.0	4.0	3.0	90.7	2.3	10.7	6.5 7.2	. 887
	-39.0	1.9	3.6	93.2	1.3			.897
	-40.0	2.2	3.4	93.1	1.3	5.1a	8.6	.920
	-41.0	2.3	3.2	93.0	1.5	5.8	8.1	.389
	-42.0	2.5	3.6	92.4	1.5	6.3	7.7	.885
	-43.0	2.7	3.8	92.1		6.9	8.6	.878
	-44.0	2.4	3.6	92.5	1.4	7.3	9.1	.878
	-45.0	1.8	3.6		1.5	6.6	8.6	.886
	-46.0			93.4	1.2	4.8a	8.6	.920
		2.5	3.3	92.7	1.5	5.8	7.9	.883
46.0-		2.7	3.4	92.5	1.4	7.4	8.1	.877
47.0-		3.1	3.1	92.3	1.5	8.3	7.4	. 884
48.0-		3.2	3.6	91.4	1.8	8.8	8.6	. 885
49.0-		5.1	3.9	88.9	2.1	13.8	9.3	.892
50.0-		3.2	3.7	91.5	1.6	8.7	8.9	.891
51.0-		6.9	3.4	87.4	2.3	18.2	8.1	.907
52.0-		4.3	5.0	88.8	1.9	11.4	12.0	.896
53.0-		3.7	4.0	90.6	1.7	10.1	9.6	.880
54.0-		3.4	3.7	90.7	2.2	9.3	8.9	. 381
55.0-		3.1	3.8	91.6	1.5	8.5	9.1	. 876
56.0-		3.2	3.6	91.6	1.6	8.8	8.6	.883
57.0-		5.8	3.5	88.6	2.1	15.5	8.4	.897
58.0-		6.2	4.3	87.3	2.2	16.6	10.3	.898
59.0-		5.9	3.7	88.5	1.9	15.7	8.9	.891
60.0-		4.6	5.5	87.9	2.0	12.4	13.2	.886
61.0-		8.4	4.0	84.4	3.2	22.2	9.6	.901
62.0-		7.8	3.5	86.3	2.4	20.5	8.4	.914
63.0-		5.9	3.9	88.2	2.0	15.6	9.3	.909
64.0-	65.0	5.0	2.9	89.5	2.6	13.3	7.0	.900

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Semples from the U.S. Geological Survey's Corehole 78-8 (Continued)

				- Conti	and also		
		Vainte	Yield	of pro:	duct		Specific
Depth	-	Weight	percent		Gal p	er ton	gravity
Fron To	011	Water	Spent	loss	oi1 ¹ /	Water.	of oil at
							60.19U. E
65.0-66.0	8.8	3.7	85.0	2.5	23.1	8.9	012
66.0-67.0	8.6	3.0	86.0	2.4	22.7	7.2	.912
67.0-68.0	11.9	3.9	80.9	3.3	31.5	9.3	.910
68.0-69.0	11.6	4.0	81.2	3.2	30.7	9.6	.907
69.0-70.0	8.0	3.5	86.0	2.5	21.0	8.4	.909
70.0-71.0	6.5	3.5	88.1	1.9	17.4	8.4	.907
71.0-72.0	7.8	3.8	86.0	2.4	20.6	9.1	.894
72.0-73.0	11.2	3.5	82.1	3.2	29.7	8.4	.902
73.0-74.0	8.8	3.9	84.0	3.3	22.9	9.3	.906
74.0-75.0	4.4	3.9	90.3	1.4	11.9	9.3	.915
75.0-76.0	3.9	3.7	91.2	1.2	10.6	8.9	. 890
76.0-77.0	4.6	3.0	91.0	1.4	12.4	7.2	. 882
77.0-78.0	4.6	3.2	91.1	1.1	12.3	7.7	. \$85
78.0-79.0	4.7	3.7	90.2	1.4	12.8	8.9	.888
79.0-80.0	7.6	2.9	87.0	2.5	20.0	7.0	. 890
80.0-81.0	4.9	3.8	89.0	2.3	13.0	9.1	.906
81.0-82.0	4.0	4.3	89.8	1.9	10.8	10.3	.904
82.0-83.0	3.7	3.0	91.1	2.2	9.9	7.2	.895
83.0-84.0	5.0	3.5	90.0	1.5	13.5	8.4	.889
84.0-85.0	4.0	3.6	91.0	1.4	10.8	8.6	.888
85.0-86.0	2.0	4.0	91.3	2.7	5.6		.882
86.0-87.0	1.5	3.3	94.6	.5	4.3a	9.6	.872
87.0-88.0	2.2	3.7	93.0	1.1	6.0	7.9	.920
88.0-89.0	3.1	3.7	91.7	1.5		8.9	.871
89.0-90.0	4.1	3.1	91.5	1.2	8.5	8.9	.878
90.0-91.0	5.6	3.0	89.6	1.8	11.2	7.4	. 890
91.0-92.0	7.8	3.2	86.5		14.7	7.2	.915
92.0-93.0	4.4	1.7	92.8	2.5	20.4	7.7	.918
93.0-94.0	6.9	2.8	88.1	1.1	11.4	4.1	.919
94.0-95.0	4.9	3.1		2.2	18.2	6.7	.914
95.0-96.0	4.1	3.1	90.7	1.3	13.1	7.4	.895
96.0-97.0	2.7	3.3	91.6	1.2	11.0	7.4	.889
97.0-98.0	4.2	3.1	91.2		7.3	7.9	.896
98.0-99.0	6.2	3.0	88.9	1.5	11.0	7.4	.906
99.0-100.0	11.0	2.9		1.9	16.4	7.2	.910
100.0-101.0	10.8	4.0	82.6	3.5	28.9	7.0	.916
101.0-102.0	13.3	3.5	82.0	3.2	28.7	9.6	.901
102.0-103.0	12.3	3.7	79.5	3.7	35.1	8.4	.904
103.0-104.0			80.3	3.7	32.7	8.9	.901
104.0-105.0	6.8	3.7	87.3	2.2	17.8	8.9	.916
105.0-106.0		3.7	82.1	3.1	29.1	8.9	.915
106.0-107.0	8.8	3.8	85.0	2.4	22.9	9.1	.918
107.0-108.0	6.1	3.7	88.2	2.0	16.2	8.9	.897
108.0-109.0	5.2	3.3	89.5		14.2	7.9	.884
109.0-110.0	8.4	2.9	85.7	3.0	22.3	7.0	. 899
107.0-110.0	8.4	2.7	86.7	2.2	22.4	6.5	.896

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Bemples from the U.S. Geological Survey's Corehole 78-8 (Continued)

	Yaeld of product											
	-	Weight	Percent	of pro			Specific					
Depth		Meakitt	Spent		Gal	per ton	gravity					
From: To	011	Water	shale	loss	013-	/ Water.	of oil at					
						MALEZ.	60°/60° F					
110.0-111.0	8.0	2.3	87.7	2.0	21.3	5.5	0.895					
111.0-112.0	7.8	2.1	87.4	2.7	20.6	5.0	.905					
112.0-113.0	7.4	3.2	86.9	2.5	19.7	7.7	.902					
113.0-114.0	8.7	3.8	85.0	2.5	23.3	9.1	.895					
114.0-115.0	8.3	3.8	85.2	2.7	22.1	9.1	.900					
115.0-116.0	11.8	3.3	81.3	3.6	31.4	7.9	.900					
116.0-117.0	8.5	3.7	85.1	2.7	23.0	8.9	.891					
117.0-118.0	6.5	4.0	87.3	2.2	17.7	9.6	.882					
118.0-119.0	1.9	3.5	92.9	1.7	4.9a	8.4	.920					
119.0-120.0	2.5	2.7	93.6	1.2	6.8	6.5	.879					
120.0-121.0	3.4	3.0	92.4	1.2	9.4	7.2	.883					
121.0-122.0	1.3	3.9	93.8	1.0	3.3a	9.3	.920					
122.0-123.0	2.7	3.2	92.9	1.2	7.3	7.7	.887					
123.0-124.0	6.8	2.7	88.2	2.3	17.9	6.5	.909					
124.0-125.0	7.4	1.6	88.4	2.6	19.7	3.8						
125.0-126.0	11.8	3.0	81.9	3.3	30.9	7.2	.905					
126.0-127.0	6.6	3.5	87.2	2.7	17.7	8.4						
127.0-128.0	4.6	3.5	89.0	2.9	12.6	8.4	.889					
128.0-129.0	4.7	3.0	90.3	2.0	12.5	7.2	. 884					
129.0-130.0	2.0	3.5	92.8	1.7	5.1a	8.4	. 894					
130.0-131.0	2.7	3.2	92.1	2.0	7.2		. 920					
131.0-132.0	4.5	3.2	89.6	1.7	14.3	7.7	.908					
132.0-133.0	4.8	3.0	90.9	1.3	12.7	7.7	.915					
133.0-134.0	6.4	3.5	87.8	2.3	16.9	7.2	.912					
134.0-135.0	3.1	2.7	92.9	1.3		8.4	.909					
135.0-136.0	2.4	2.9	92.8		8.4	6.5	.880					
136.0-137.0	1.6	3.4	93.9	1.9	6.6	7.0	.873					
137.0-138.0	2.3	3.6	92.9	1.1	4.2a	8.1	.920					
138.0-139.0	1.3	4.3	93.4	1.2	6.3	8.6	.883					
139.0-140.0	1.0	4.8	92.5	1.0	3.4a	10.3	.920					
140.0-141.0	1.5	4.0	93.7	1.7	2.6a 3.9a	11.5	. 920					
141.0-142.0	2.9	3.7	92.2	1.2	8.0	9.6	.920					
142.0-143.0	1.0	3.8	94.2	1.0	2.8a	8.9	.881					
143.0-144.0	1.2	3.7	94.0	1.1	3.1a	9.1	.920					
144.0-145.0	4.8	2.9	91.2		12.8	8.9	.920					
145.0-146.0	11.0	3.0	82.9		29.0	7.0	.909					
146.0-147.0	12.3	3.5	80.4		32.4	7.2	.906					
147.0-148.0	10.3	3.3	83.0			8.4	.912					
148.0-149.0	6.5	3.6	87.9		26.6	7.9	.925					
149.0-150.0	5.4	3.6	89.2			8.6	.901					
150.0-151.0	3.8	3.4	91.0		14.6	8.6	.881					
151.0-152.0	3.8	3.2	90.1		10.4	8.1	.877					
152.0-153.0	3.6	3.6	90.1		10.5	7.7	. 879					
153.0-154.0	3.4	4.0	91.5		10.0	8.6	. 866					
	3.0	3.5	91.3		9.4	9.6	.863					
133.0	3.0	3.3	90.6	2.9	8.3	8.4	.871					

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Samples from the U.S. Geological Survey's Corehole 78-8 (Continued)

		Yield of product										
		Weight	percent		Specific							
Depth			Spent	Gas -		er ton	gravity					
From To	011	Water	shale	loss	011-1	Water.	of oil at					
255 0 454 0						MALEL.	60.160. E					
155.0-156.0	1.0	4.9	93.0	1.1	2.5a	11.7	. 920					
156.0-157.0	1.2	4.5	93.2	1.1	3.1a	10.8						
157.0-158.0	1.6	4.5	92.6	1.3	4.2a	10.8	.920					
158.0-159.0	2.0	3.7	93.3	1.0	5.4	8.9	.920					
159.0-160.0	6.7	3.5	87.5	2.3	17.9	8.4	. 864					
160.0-161.0	5.3	3.5	89.5	1.7	14.1	8.4	.902					
161.0-162.0	4.4	3.5	90.6	1.5	11.9	8.4	.901					
162.0-163.0	5.3	3.6	89.3	1.8	14.3	8.6	.883					
163.0-164.0	4.0	3.5	89.7	2.8	11.1		. 892					
164.0-165.0	1.9	3.4	93.5	1.2		8.4	.874					
165.0-166.0	1.1	2.9	95.2	.8	5.0a	8.1	. 920					
166.0-167.0	. 7	3.0	95.6		2.8a	7.0	-920					
167.0-168.0	1.7	3.2	94.0	.7	1.8a	7.2	.920					
168.0-169.0	1.6	3.1	94.1	1.1	4.6a	7.7	.920					
169.0-170.0	3.2	3.2		1.2	4.2a	7.4	.920					
170.0-171.0	4.6		91.8	1.8	8.7	7.7	.871					
171.0-172.0		2.9	90.7	1.8	12.3	7.0	0.884					
	5.1	3.2	89.4	2.4	13.6	7.4	.898					
172.0-173.0	4.2	2.6	90.9	2.3	11.3	6.2	.892					
173.0-174.0	4.1	2.9	91.4	1.6	11.0	7.0	. 892					
174.0-175.0	4.2	2.9	91.4	1.5	11.2	7.0	.891					
175.0-176.0	4.6	2.8	90.4	2.2	12.3	6.7	.889					
176.0-177.0	4.6	2.8	90.1	2.5	12.5	6.7	.892					
177.0-178.0	4.9	2.8	89.7	2.6	13.1	6.7	. 890					
178.0-179.0	6.0	2.3	88.6	3.1	16.3	5.5	.888					
179.0-180.0	5.7	2.8	89.1	2.4	15.3	6.7	.895					
180.0-181.0	5.2	2.4	90.0	2.4	14.1	5.8	.895					
181.0-182.0	5.1	3.0	88.6	3.3.	13.7	7.2	.894					
182.0-183.0	3.4	3.0	90.5	3.1	9.4	7.2	.882					
183.0-184.0	2.1	2.5	92.6	2.8	5.8	6.0	.866					
184.0-185.0	2.5	2.3	93.2	2.0	6.8	5.5	.864					
185.0-186.0	2.2	2.9	92.3	2.6	6.2	7.2						
186.0-187.0	1.3	2.1	95.0	1.6	3.4a	5.0	. 866					
187.0-188.0	. 8	2.2	94.9	2.1	2.0a		.920					
188.0-189.0	1.0	2.2	95.4	1.4		5.3	.920					
189.0-190.0	1.2	2.4	94.5	1.9	2.7a	5.3	. 920					
190.0-191.0	1.5	2.6	94.0		3.1a	5.8	.920					
191.0-192.0	2.8	2.5		1.9	3.9a	6.2	.920					
192.0-193.0	3.0	2.7	92.6	2.1	7.8	6.0	. 869					
193.0-194.0	3.3	3.2	91.1	3.2	8.2	6.5	.870					
			90.7	2.8	9.1	7.7	.875					
194.0-195.0	6.2	2.9	88.4	2.5	16.8	7.0	. 890					
195.0-196.0	7.5	2.8	86.7	3.0	20.2	6.7	. 895					
196.0-197.0	7.1	2.6	87.9	2.4	19.1	6.2	.888					
197.0-198.0	8.0	3.4	86.5	2.1	21.2	8.1	.900					
198.0-199.0	9.2	3.2	85.3	2.3	24.2	7.7	.908					
199.0-200.0	4.9	3.2	89.1	2.8	13.3	.7.7	.888					

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Semples from the U.S. Geological Survey's Corehole 78-8 (Continued)

		Yield of product										
D1	-	Weight	percent	or proc	The second secon	er ton	Specific					
Depth From To			Spent	£85 +			gravity					
From To	011	Water	shale	loss	0i11/	Water	of oil at 60°/60°					
200.0-201.0	2 /	2.0										
201.0-202.0	2.4	2.9	93.4	1.3	6.5	7.0	0.876					
202.0-203.0	1.2	2.6	95.6	. 6	3.2a	6.2	.920					
	1.5	2.5	94.0	2.0	3.9a	6.0	. 920					
203.0-204.0	2.7	3.3	92.9	1.1	7.2	7.9	.885					
204.0-205.0	7.9	3.1	86.9	2.1	20.7	7.4	.920					
205.0-206.0	10.0	3.7	83.5	2.8	25.8	8.9	.925					
206.0-207.0	4.5	4.0	89.6	1.9	12.0	9.6						
207.0-208.0	2.2	4.3	91.8	1.7	6.1	10.3	.895					
208.0-209.0	1.9	3.7	92.8	1.6	4.8a		.881					
209.0-210.0	.6	2.9	95.3	1.2		8.9	.920					
210.0-211.0	. 7	3.0	95.1		1.6a	7.0	.920					
211.0-212.0	1,0	3.0	93.9	1.2	1.8a	7.2	.920					
212.0-213.0	7.0			2.1	2.6a	7.2	. 920					
213.0-214.0		3.1	87.6	2.3	18.5	7.4	.911					
214.0-215.0	7.7	3.3	86.5	2.5	20.5	7.9	.902					
	5.2	3.6	89.0	2.2	13.9	8.6	.892					
215.0-216.0	5.4	3.6	89.2	1.8	14.4	8.6	. 895					
216.0-217.0	7.1	3.4	87.2	2.3	18.8	8.1	.911					
217.0-218.0	7.8	3.5	86.0	2.7	20.8	8.4	.902					
218.0-219.0	6.8	3.5	87.9	1.8	18.1	8.4						
219.0-220.0	2.9	3.5	91.1	2.5	7.9	8.4	.904					
220.0-221.0	2.1	3.2	92.6	2.1	5.8		.882					
221.0-222.0	2.4	3.7	92.7			7.7	.883					
222.0-223.0	4.6	3.7		1.2	6.5	8.9	.877					
223.0-224.0			89.9	1.8	12.5	8.9	. 884					
224.0-225.0	5.5	3.1	88.9	2.5	14.7	7.4	. 894					
	9.8	2.9	85.5	1.8	25.6	7.0	.921					
225.0-226.0	10.2	3.5	84.3	2.0	26.6	8.4	.916					
226.0-227.0	4.0	3.2	91.1	1.7	10.4	7.7	.914					
227.0-228.0	6.9	3.0	88.7	1.4	18.1	7.2	.915					
228.0-229.0	7.4	3.8	87.2	1.6	19.6	9.1	.908					
229.0-230.0	5.6	3.3	89.7	1.4	14.9	7.9						
230.0-231.0	2.4	3.5	92.9	1.2			.908					
231.0-232.0	2.9	4.0	92.0		6.4	8.4	0.902					
232.0-233.0	4.9	3.2	90.8	1.1	7.6	9.6	.900					
33.0-234.0	5.1			1.1	12.9	7.7	.911					
34.0-235.0		3.6	90.2	1.1	13.4	8.6	.915					
35.0-236.0	7.8	2.7	86.3	3.2	20.4	6.5	.919					
36.0-237.0	8.0	2.7	85.3	4.0	21.1	6.5	.906					
	10.1	2.2	84.5	3.2	26.7	5.3	.909					
37.0-238.0	4.5	2.9	90.6	2.0	12.0	7.0	.905					
38.0-239.0	4.0	2.4	91.4	2.2	10.5	5.8	.906					
239.0-240.0	4.1	2.1	92.7	1.1	10.7	5.0	.917					
240.0-241.0	1.0	1.9	96.3	.8	2.6a	4.6	.920					
241.0-242.0	1.2	2.1	95.8	.9	3.2a	5.0						
242.0-243.0	1.1	2.6	95.5				.920					
243.0-244.0				.8	2.95	6.2	.920					
244.0-245.0	1.1	2.2	96.1	.6	2.9a	5.3	. 920					
243.0	1.1	1.9	96.4	. 6	3.0a	4.6	.920					

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Samples from the U.S. Geological Survey's Corehole 78-8 (Continued)

	-	6-16					
Depair		Weigne	percent	of proc	THE RESERVE AND ADDRESS OF THE PARTY OF THE	er ton	Specific
Depth		Maror	Spent	Gas 4		-1 6011	gravity
From To	011	Water	shale	loss	011-/	Water.	of oil at 60°/60° F
							00 / h() }
245.0-246.0	. 8	2.2	95.3	7 7	2.7	- 0	
246.0-247.0	1.0	2.0	96.2	1.7	2.1a	5.3	.920
247.0-248.0	.7	2.2		.8	2.6a	4.8	.920
248.0-249.0	1.2		96.2	.9	1.9a	5.3	.920
249.0-250.0	.8	1.9	94.8	2.1	3.1a	4.6	.920
250.0-251.0	.9	1.9	96.6	. 7	2.2a	4.6	. 920
251.0-252.0		1.7	96.8	. 6	2.4a	4.1	.920
252.0-253.0	1.2	1.9	96.1	. 8	3.2a	4.6	.920
253.0-254.0	. 4	2.8	96.3	.5	1.0a	6.7	.920
	1.2	2.0	96.4	. 4	3.2a	4.8	.920
254.0-255.0	1.2	2.2	96.0	.6	3.0a	5.3	.920
255.0-256.0	1.1	2.0	95.9	1.0	2.9a	4.8	.920
256.0-257.0	1.5	2.3	95.4	. 8	4.0a	5.5	.920
257.0-258.0	1.5	2.3	94.5	1.7	4.0a	5.5	.920
258.0-259.0	1.3	2.1	96.1	.5	3.4a	5.0	.920
259.0-260.0	1.6	1.9	96.1	. 4	4.1a	4.6	.920
260.0-261.0	0.8	3.0	95.7	0.5	2.1a	7.2	. 920
261.0-262.0	.9	1.7	97.0	.4	2.2a	4.1	. 920
262.0-263.0	1.4	1.5	96.7	. 4	3.7a	3.6	.920
263.0-264.0	. 4	1.9	97.2	.5	1.0a	4.6	.920
264.0-265.0	3.3	1.3	94.4	1.0	9.0	3.1	.873
265.0-266.0	4.7	1.1	92.6	1.6	12.6	2.6	.888
266.0-267.0	3.4	. 6	94.1	1.9	9.1	1.4	.888
267.0-268.0	2.8	2.0	93.7	1.5	7.5	4.8	. 889
268.0-269.0	1.5	2.4	94.8	1.3	4.0a	5.8	.920
269.0-270.0	2.5	2.5	92.9	2.1	6.8	6.0	.900
270.0-271.0	3.0	2.0	93.8	1.2	8.1	4.8	. 883
271.0-272.0	2.9	2.6	93.1	1.4	7.7	6.2	. 894
272.0-273.0	2.7	2.5	92.8	2.0	7.2	6.0	. 896
273.0-274.0	2.2	2.8	93.6	1.4	6.0	6.7	.888
274.0-275.0	5.3	1.9	90.2	2.6	14.1	4.6	.907
275.0-276.0	6.7	2.6	89.2	1.5	17.5	6.2	.910
276.0-277.0	4.6	2.6	91.7	1.1	12.1	6.2	.902
277.0-278.0	6.7	3.2	87.1	3.0	17.4	7.7	.924
278.0-279.0	7.4	3.1	87.4	2.1	19.1	7.4	.930
279.0-280.0	5.5	2.2	90.5	1.8	14.1	5.3	.930
280.0-281.0	3.6	2.3	92.6	1.5	9.3	5.5	.925
281.0-282.0	1.3	3.1	93.9		3.3a	7.4	.920
282.0-283.0	5.7	3.0	89.7		14.6	7.2	.934
283.0-284.0	7.3	2.8	87.5		18.7	6.7	.934
284.0-285.0	5.8	2.5	89.5		15.0	6.0	.931
285.0-286.0	6.6	3.0			16.9	7.2	.931
286.0-287.0	4.3	1.6	92.1	2.0	11.0	3.8	.932
287.0-288.0	1.6	1.8	95.5		4.3a	4.3	.920
288.0-289.0	4.0	2.9	91.9	1.2	10.5	7.0	.922
289.0-290.0	5.9	3.1	89.1	1.9	15.4	7.4	.926

NAME AND ADDRESS OF PERSON AS PARTY AND ADDRESS OF PERSONS ASSESSED.

bearing from the Co. designated assessed automotive or the contract of the con

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OLL-SHALE ASSAYS BY MODIFIED FISCHER RETORT MITHOD

Samples from the U.S. Geological Survey's Corehole 78-8 (Continued)

				Yield	of prod	uct		
Depth		-	Weight	percent		Gal 1	per ton	Specific gravity
From To		011		Spent	Gas +			of oil at
10		011	Water	shale	loss	011-	Water.	60°/60° F
290.0-291.0		5.1	3.4	90.3	1.2	12 2		
291.0-292.0		4.7	2.3	91.9	1.1	13.3	8.1	0.924
292.0-293.0		4.8	3.2	90.8		12.3	5.5	.920
293.0-294.0		4.7	- 2.7	91.4	1.2	12.8	7.7	. 895
294.0-295.0		3.9	4.0	91.4	1.2	12.8	6.5	. 885
295.0-296.0		2.5	3.2		.9	10.8	9.6	.872
		4.2		92.3	2.0	6.7	7.7	.877
296.0-297.0		5.6	3.4	91.3	1.1	11.3	8.1	. 886
297.0-298.0			3.5	89.6	1.3	14.8	8.4	.904
298.0-299.0		3.5	3.6	91.6	1.3	9.5	8.6	.885
299.0-300.0		2.9	3.4	92.5	1.2	8.1	8.1	. 870
300.0-301.0		4.0	2.6	92.1	1.3	10.7	6.2	. 887
301.0-302.0		3.6	2.2	93.0	1.2	9.8	5.3	.887
302.0-303.0		2.4	1.9	94.8	.9	6.6	4.6	. 873
303.0-304.0		2.4	3.9	92.8	.9	6.6	9.3	. 875
304.0-305.0		2.8	4.0	91.5	1.7	7.6	9.6	.882
305.0-306.0		2.4	3.2	93.2	1.2	6.3	7.7	. 890
306.0-307.0		2.0	3.6	93.6	. 8	5.3	8.6	
307.0-308.0		3.6	3.4	91.7	1.3	9.4		. 837
308.0-309.0		5.0	3.7	89.9	1.4		8.1	.913
309.0-310.0		2.8	2.0	94.0		13.2	8.9	.913
310.0-311.0		3.2	3.5	91.6	1.2	7.3	4.8	.932
311.0-312.0		3.4	3.6		1.7	8.4	8.4	.919
		3.1	4.0	91.4	1.6	9.0	8.6	. 894
312.0-313.0		1.0		91.3	1.6	8.5	9.6	. 889
313.0-314.0		2.5	2.0	95.4	1.6	2.7a	4.8	.920
314.0-315.0			4.0	92.1	1.4	6.9	9.6	.878
315.0-316.0		3.7	3.8	91.1	1.4	10.0	9.1	.883
31.6.0-317.0		3.0	3.8	91.2	2.0	8.2	9.1	. 893
317.0-318.0		2.8	3.1	92.7	1.4	7.7	7.4	. 885
318.0-319.0		1.3	1.7	96.1	. 9	3.4a	4.1	.920
319.0-320.0		1.9	2.8	93.9	1.4	4.9a	6.7	.920
320.0-321.0		2.7	2.2	93.9	1.2	7.5	5.3	.878
321.0-322.0		2.1		94.0	1.1	5.6	6.7	. 892
322.0-323.0		3.2	2.3	93.3	1.2	8.5	5.5	.902
323.0-324.0		2.4	3.3	93.1	1.2	6.4	7.9	.893
324.0-325.0	- 1	2.2	3.2	93.5	1.1	5.9	7.7	. 895
325.0-326.0		1.4	2.4	95.5	.7	3.7a	5.8	.920
326.0-327.0		1.2	2.3	96.1	.4	3.2a	5.5	.920
327.0-328.0		3.1	3.6	92.1	1.2	8.3	8.6	.906
328.0-329.0		1.1	3.9	93.9	1.1	2.9a	9.3	
329.0-330.0		1.4	2.8	95.2	.6	3.8a	6.7	. 920
		1.8	2.8	94.9	.5	4.7a		. 920
330.0-331.0		2.6	2.7				6.7	. 920
331.0-332.0				93.8	.9	7.0	6.5	. 882
332.0-333.0		1.8	3.7	93.4	1.1	4.7a	8.9	.920 .
333.0-334.0		1.3	3.4	94.0	1.3	3.3a	8.1	.920
334.0-335.0	* .	1.5	4.5	92.9	1.1	4.0a	10.8	.920

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				290.0-291.0
			. 7.3	

OLL-SHALE ASSAYS BY MODIFIED FISCHER RETORT MITHOD

Samples from the U.S. Geological Survey's Corehole 78-8 (Continued)

Pepth From To
Spent Spent Sab + Spent Sab + Spent Spen
335.0-336.0
335.0-336.0 336.0-337.0 1.4 2.8 94.9 .9 3.7a 6.7 920 337.0-338.0 .6 2.8 95.6 1.0 1.5a 6.7 .920 338.0-339.0 1.3 2.5 95.5 .7 3.5a 6.0 .920 339.0-340.0 2.7 3.1 93.0 1.2 7.2 7.4 891 340.0-341.0 3.2 2.3 93.1 1.4 8.6 5.5 880 341.0-342.0 32.1 1.9 7.0 1.7 6.0 2.6 343.0-344.0 0 34 1.5 97.3 8 .9a 3.6 920 344.0-345.0 331.5 97.7 5 7a 3.6 920 345.0-356.0 34 1.3 97.6 7 98.2 34 1.8a 1.7 920 348.0-349.0 350.0-351.0 2.3 1.9 94.9 94.9 96.2 96.2 96.2 97.7 1.1 1.6a 1.4 920 347.0-348.0 7 7 98.2 34 1.8a 1.7 920 348.0-349.0 99 6 98.0 5 2.3a 1.4 920 349.0-350.0 38 36 350.0-351.0 2.3 1.9 94.9 96.2 36 36 350.0-355.0 3.1 2.4 94.4 1.8 3.8a 5.8 920 353.0-356.0 3.1 2.4 94.4 1.8 3.8a 5.8 920 355.0-356.0 3.1 2.4 93.1 1.4 8.5 886 355.0-356.0 3.1 2.4 93.1 1.4 8.5 886 355.0-356.0 3.1 2.4 93.1 1.4 8.5 8.877 356.0-357.0 2.0 1.3 3.3 94.5 9 3.3a 7.9 9.920 359.0-360.0 3.1 2.4 93.1 1.4 8.5 8.6 886 359.0-359.0 2.0 3.4 93.0 1.6 3.5 94.6 3.3 4.1a 8.4 920 358.0-359.0 2.0 3.4 93.0 1.6 3.5 94.6 3.5 3.1 8.86 369.0 363.0-364.0 1.7 3.0 94.3 1.0 4.4a 7.2 920 363.0-363.0 1.6 2.1 95.4 9 94.2a 5.0 920 363.0-366.0 1.7 3.0 94.3 1.0 4.4a 7.2
336.0-337.0 337.0-338.0 36.0-337.0 338.0-339.0 338.0-339.0 339.0-340.0 32.5 35.0-340.0 32.7 33.1 33.0-340.0 33.1 33.0-340.0 33.1 33.0-340.0 33.1 33.0-340.0 33.1 33.0-340.0 33.1 33.0-340.0 33.1 33.0-340.0 33.1 33.0-340.0 33.1 33.0-340.0 33.1 33.0-340.0 33.1 33.0-340.0 33.1 33.0-340.0 33.1 33.0-340.0 33.1 33.0-340.0 341.0-342.0 341.0-342.0 342.0-343.0 35.0-356.0 31.5 31.5 31.5 31.5 31.5 31.5 31.5 31.5
337.0-338.0 338.0-339.0 1.3 2.5 95.5 7 3.5a 6.0 920 339.0-340.0 2.7 3.1 93.0 1.2 7.2 7.4 891 340.0-341.0 3.2 2.3 93.1 1.4 8.6 5.5 880 341.0-342.0 32 1.1 97.0 1.7 6a 2.6 920 343.0-344.0 3.1 5 2.4 96.2 9 1.2a 5.8 920 344.0-345.0 31.5 97.7 5 7a 3.6 920 345.0-356.0 3 1.5 97.7 1.1 1.6a 1.4 920 347.0-348.0 37 7 7 98.2 4 1.8a 1.7 920 349.0-350.0 38 6 98.2 4 2.0a 1.4 920 349.0-350.0 38 6 98.2 4 2.0a 1.4 920 349.0-350.0 38 36 98.2 4 2.0a 36 351.0-352.0 36 352.0-353.0 31.4 2.4 94.4 1.8 3.8a 5.8 920 355.0-356.0 3.1 2.4 93.1 1.4 8.5 5.8 881 351.0-355.0 3.4 2.5 93.0 1.1 8.9 6.0 909 352.0-353.0 3.4 2.5 93.0 1.1 8.9 6.0 909 352.0-353.0 3.4 2.5 93.0 1.1 8.9 6.0 909 352.0-353.0 3.4 2.5 93.0 1.1 8.9 6.0 909 352.0-355.0 3.1 2.4 93.1 1.4 8.5 5.8 877 356.0-357.0 2.0 1.3 3.3 94.5 93.3 3.1 886 357.0-358.0 1.6 3.5 94.6 3 3.1 3.8 86 357.0-358.0 3.1 2.4 93.1 1.4 8.5 5.8 877 366.0-357.0 2.0 1.3 95.9 8 5.3 3.1 886 357.0-358.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3
338.0-339.0 339.0-340.0 2.7 3.1 93.0 1.2 7.2 7.4 891 340.0-341.0 3.2 2.3 93.1 1.4 8.6 5.5 880 341.0-342.0 32 1.1 97.0 1.7 6a 2.6 920 343.0-344.0 3.5 2.4 96.2 91.2a 5.8 920 344.0-345.0 3.1.5 97.7 3.5 7a 3.6 920 344.0-345.0 3.1.5 97.7 5.7 3.6 920 345.0-356.0 41.3 97.6 79.2 347.0-348.0 37 77 98.2 41.8a 1.7 920 349.0-350.0 38 69 88.6 98.2 42.0a 1.4 920 340.0-351.0 32.3 1.9 94.9 94.9 95.2 34.0-355.0 34.0-355.0 34.0-355.0 34.0-355.0 35.0-356.0 34.0-355.0 35.0-356.0 34.0-355.0 35.0-356.0 34.0-355.0 35.0-356.0 34.0-355.0 35.0-356.0 34.0-355.0 35.0-356.0 35.0-356.0 36.0-357.0 37 38.0-360.0 38.6 98.2 48.0-349.0 99.9 90.9 9
339.0-340.0 339.0-340.0 3.2 2.3 93.1 1.4 8.6 5.5 880 341.0-342.0 2.1.1 97.0 1.7 6a 2.6 920 342.0-343.0 5.2,4 96.2 9 1.2a 5.8 920 343.0-344.0 34.0-345.0 3.1.5 97.7 5.7a 3.6 920 345.0-356.0 3.1.5 97.7 1.1 1.6a 1.4 920 347.0-348.0 7 7 98.2 4 1.8a 1.7 920 348.0-349.0 9 6 98.0 5 2.3a 1.4 920 349.0-350.0 38 6 98.0 5 2.3a 1.4 920 349.0-350.0 350.0-351.0 2.3 1.9 94.9 0.9 6 98.0 352.0-353.0 3.4 2.5 93.0 31.1 8.9 6.0 909 352.0-353.0 3.4 2.4 94.4 1.8 3.8a 5.8 920 355.0-356.0 3.1 2.4 94.4 1.8 3.8a 5.8 920 355.0-356.0 3.1 2.4 93.1 1.4 8.5 5.8 877 356.0-357.0 2.0 1.3 3.3 94.5 9 3.3a 7.9 920 355.0-358.0 3.1 2.4 93.1 1.4 8.5 5.8 877 356.0-357.0 2.0 1.3 3.3 94.5 9 3.3a 7.9 920 355.0-358.0 3.1 886 357.0-358.0 3.1 2.4 93.1 1.4 8.5 5.8 877 356.0-357.0 2.0 1.3 3.5 94.6 3.3 4.1a 8.4 920 355.0-356.0 3.1 2.4 93.0 1.6 5.6 8.1 878 359.0-360.0 3.0 3.3 92.1 1.6 8.0 7.9 886 360.0-361.0 3.5 3.2 91.5 1.8 9,7 7.7 877 361.0-362.0 4.9 2.2 90.4 2.5 13.1 5.3 899 362.0-363.0 1.6 2.6 2.7 2.0 96.6 2.7 2.0 96.4 2.5 3.1 3.1 3.899 362.0-363.0 3.1 3.1 3.0 94.2a 5.0 920 363.0-364.0 1.7 3.0 94.3 1.0 94.4a 7.2
340.0-341.0 3.2 2.3 93.1 1.4 8.6 5.5 880 341.0-342.0 322.1 1 97.0 1.7 6a 2.6 920 342.0-343.0 3.5 2.4 96.2 9 1.2a 5.8 920 343.0-344.0 34.0-345.0 31.5 97.7 3.6 3.6 920 344.0-345.0 31.5 97.7 3.6 3.6 920 345.0-356.0 31.5 97.7 1.1 1.6a 1.4 920 347.0-348.0 37 37 98.2 4 1.8a 1.7 920 348.0-349.0 39 6 98.0 5 2.3a 1.4 920 349.0-350.0 38 8 6 98.2 4 2.0a 1.4 920 349.0-350.0 350.0-351.0 2.3 1.9 94.9 0.9 6.2 4.6 881 351.0-352.0 3.4 2.5 93.0 1.1 8.9 6.0 909 352.0-353.0 1.4 2.4 94.4 1.8 3.8a 5.8 920 354.0-355.0 3.1 2.4 94.4 1.8 3.8a 5.8 920 355.0-356.0 3.1 2.4 93.1 1.4 8.5 5.8 877 356.0-357.0 2.0 1.3 3.3 94.5 93.1 1.4 8.5 5.8 877 356.0-359.0 2.0 3.4 93.0 1.6 3.5 94.6 3 3.1 886 357.0-358.0 3.6 3.7 9.920 363.0-364.0 3.5 3.0 3.1 3.4 9.20 9.20 9.4 9.6 9.6 9.6 9.7 9.7 9.8 9.8 9.8 9.8 9.8 9.8 9.8 9.8 9.8 9.8
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343.0-344.0 .4 1.5 97.3 .8 .9a 3.6 .920 344.0-345.0 .3 1.5 97.7 .5 .7a 3.6 .920 345.0-356.0 .4 1.3 97.6 .7 .9a 3.1 .920 346.0-347.0 .6 .6 .97.7 1.1 1.6a 1.4 .920 347.0-348.0 .7 .7 .98.2 .4 1.8a 1.7 .920 348.0-349.0 .9 .6 .98.0 .5 2.3a 1.4 .920 349.0-350.0 .8 .6 .98.2 .4 2.0a 1.4 .920 350.0-351.0 2.3 1.9 .94.9 0.9 6.2 4.6 .881 351.0-352.0 3.4 2.5 93.0 1.1 8.9 6.0 .900 352.0-353.0 1.4 2.4 .94.4 1.8 3.8a 5.8 .920 354.0-355.0 3.3 3.9 .9 .9 .9 .9 .9 .9 .9 3
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345.0-356.0 .4 1.3 97.6 .7 .9a 3.1 .920 346.0-347.0 .6 .6 97.7 1.1 1.6a 1.4 .920 347.0-348.0 .7 .7 98.2 .4 1.8a 1.7 .920 348.0-349.0 .9 .6 98.0 .5 2.3a 1.4 .920 349.0-350.0 .8 .6 98.2 .4 2.0a 1.4 .920 350.0-351.0 2.3 1.9 94.9 0.9 6.2 4.6 .881 351.0-352.0 3.4 2.5 93.0 1.1 8.9 6.0 .909 352.0-353.0 1.4 2.4 94.4 1.8 3.8a 5.8 .920 353.0-354.0 .7 2.0 96.6 .7 1.7a 4.8 .920 355.0-356.0 3.1 2.4 93.1 1.4 8.5 5.8 .877 356.0-357.0 2.0 1.3 95.9 .8 5.3 3.1 .886 357.0-358.0 1.6
346.0-347.0 .6 .6 97.7 1.1 1.6a 1.4 .920 347.0-348.0 .7 .7 98.2 .4 1.8a 1.7 .920 348.0-349.0 .9 .6 98.0 .5 2.3a 1.4 .920 349.0-350.0 .8 .6 98.2 .4 2.0a 1.4 .920 350.0-351.0 2.3 1.9 94.9 0.9 6.2 4.6 .881 351.0-352.0 3.4 2.5 93.0 1.1 8.9 6.0 .909 352.0-353.0 1.4 2.4 94.4 1.8 3.8a 5.8 .920 353.0-354.0 .7 2.0 96.6 .7 1.7a 4.8 .920 354.0-355.0 1.3 3.3 94.5 .9 3.3a 7.9 .920 355.0-356.0 3.1 2.4 93.1 1.4 8.5 5.8 .877 356.0-357.0 2.0 1.3 95.9 .8 5.3 3.1 .886 357.0-358.0 1.6 </td
347.0-348.0 .7 .7 98.2 .4 1.8a 1.7 .920 348.0-349.0 .9 .6 98.0 .5 2.3a 1.4 .920 349.0-350.0 .8 .6 98.2 .4 2.0a 1.4 .920 350.0-351.0 2.3 1.9 94.9 0.9 6.2 4.6 .881 351.0-352.0 3.4 2.5 93.0 1.1 8.9 6.0 .909 352.0-353.0 1.4 2.4 94.4 1.8 3.8a 5.8 .920 353.0-354.0 .7 2.0 96.6 .7 1.7a 4.8 .920 354.0-355.0 1.3 3.3 94.5 .9 3.3a 7.9 .920 355.0-356.0 3.1 2.4 93.1 1.4 8.5 5.8 .877 356.0-357.0 2.0 1.3 95.9 .8 5.3 3.1 .886 357.0-358.0 1.6 3.5 94.6 .3 4.1a 8.4 .920 358.0-359.0 2.0<
348.0-349.0 .9 .6 98.0 .5 2.3a 1.4 .920 349.0-350.0 .8 .6 98.2 .4 2.0a 1.4 .920 350.0-351.0 2.3 1.9 94.9 0.9 6.2 4.6 .881 351.0-352.0 3.4 2.5 93.0 1.1 8.9 6.0 .909 352.0-353.0 1.4 2.4 94.4 1.8 3.8a 5.8 .920 353.0-354.0 .7 2.0 96.6 .7 1.7a 4.8 .920 354.0-355.0 1.3 3.3 94.5 .9 3.3a 7.9 .920 355.0-356.0 3.1 2.4 93.1 1.4 8.5 5.8 .877 356.0-357.0 2.0 1.3 95.9 .8 5.3 3.1 .886 357.0-358.0 1.6 3.5 94.6 .3 4.1a 8.4 .920 358.0-359.0 2.0 3.4 93.0 1.6 8.6 8.1 .878 359.0-360.0 3.
349.0-350.0 .8 .6 98.2 .4 2.0a 1.4 .920 350.0-351.0 2.3 1.9 94.9 0.9 6.2 4.6 .881 351.0-352.0 3.4 2.5 93.0 1.1 8.9 6.0 .909 352.0-353.0 1.4 2.4 94.4 1.8 3.8a 5.8 .920 353.0-354.0 .7 2.0 96.6 .7 1.7a 4.8 .920 354.0-355.0 1.3 3.3 94.5 .9 3.3a 7.9 .920 355.0-356.0 3.1 2.4 93.1 1.4 8.5 5.8 .877 356.0-357.0 2.0 1.3 95.9 .8 5.3 3.1 .886 357.0-358.0 1.6 3.5 94.6 .3 4.1a 8.4 .920 358.0-359.0 2.0 3.4 93.0 1.6 5.6 8.1 .878 359.0-360.0 3.0 3.3 92.1 1.6 8.0 7.9 .886 360.0-361.0
350.0-351.0 2.3 1.9 94.9 0.9 6.2 4.6 .881 351.0-352.0 3.4 2.5 93.0 1.1 8.9 6.0 .909 352.0-353.0 1.4 2.4 94.4 1.8 3.8a 5.8 .920 353.0-354.0 .7 2.0 96.6 .7 1.7a 4.8 .920 354.0-355.0 1.3 3.3 94.5 .9 3.3a 7.9 .920 355.0-356.0 3.1 2.4 93.1 1.4 8.5 5.8 .877 356.0-357.0 2.0 1.3 95.9 .8 5.3 3.1 .886 357.0-358.0 1.6 3.5 94.6 .3 4.1a 8.4 .920 358.0-359.0 2.0 3.4 93.0 1.6 5.6 8.1 .878 359.0-360.0 3.0 3.3 92.1 1.6 8.0 7.9 .886 360.0-361.0 3.5 3.2 91.5 1.8 9.7 7.7 .877 361.0-362.0 <t< td=""></t<>
351.0-352.0 3.4 2.5 93.0 1.1 8.9 6.0 .909 352.0-353.0 1.4 2.4 94.4 1.8 3.8a 5.8 .920 353.0-354.0 .7 2.0 96.6 .7 1.7a 4.8 .920 354.0-355.0 1.3 3.3 94.5 .9 3.3a 7.9 .920 355.0-356.0 3.1 2.4 93.1 1.4 8.5 5.8 .877 356.0-357.0 2.0 1.3 95.9 .8 5.3 3.1 .886 357.0-358.0 1.6 3.5 94.6 .3 4.1a 8.4 .920 358.0-359.0 2.0 3.4 93.0 1.6 5.6 8.1 .878 359.0-360.0 3.0 3.3 92.1 1.6 8.0 7.9 .886 360.0-361.0 3.5 3.2 91.5 1.8 9.7 7.7 .877 361.0-362.0 4.9 2.2 90.4 2.5 13.1 5.3 .899 362.0-363.0 <
352.0-353.0 1.4 2.4 94.4 1.8 3.8a 5.8 .920 353.0-354.0 .7 2.0 96.6 .7 1.7a 4.8 .920 354.0-355.0 1.3 3.3 94.5 .9 3.3a 7.9 .920 355.0-356.0 3.1 2.4 93.1 1.4 8.5 5.8 .877 356.0-357.0 2.0 1.3 95.9 .8 5.3 3.1 .886 357.0-358.0 1.6 3.5 94.6 .3 4.1a 8.4 .920 358.0-359.0 2.0 3.4 93.0 1.6 5.6 8.1 .878 359.0-360.0 3.0 3.3 92.1 1.6 8.0 7.9 .886 360.0-361.0 3.5 3.2 91.5 1.8 9.7 7.7 .877 361.0-362.0 4.9 2.2 90.4 2.5 13.1 5.3 .899 362.0-363.0 1.6 2.1 95.4 .9 4.2a 5.0 .920 364.0 1.7
353.0-354.0 .7 2.0 96.6 .7 1.7a 4.8 .920 354.0-355.0 1.3 3.3 94.5 .9 3.3a 7.9 .920 355.0-356.0 3.1 2.4 93.1 1.4 8.5 5.8 .877 356.0-357.0 2.0 1.3 95.9 .8 5.3 3.1 .886 357.0-358.0 1.6 3.5 94.6 .3 4.1a 8.4 .920 358.0-359.0 2.0 3.4 93.0 1.6 5.6 8.1 .878 359.0-360.0 3.0 3.3 92.1 1.6 8.0 7.9 .886 360.0-361.0 3.5 3.2 91.5 1.8 9.7 7.7 .877 361.0-362.0 4.9 2.2 90.4 2.5 13.1 5.3 .899 362.0-363.0 1.6 2.1 95.4 .9 4.2a 5.0 .920 363.0-364.0 1.7 3.0 94.3 1.0 4.4a 7.2 .920
354.0-355.0 1.3 3.3 94.5 .9 3.3a 7.9 .920 355.0-356.0 3.1 2.4 93.1 1.4 8.5 5.8 .877 356.0-357.0 2.0 1.3 95.9 .8 5.3 3.1 .886 357.0-358.0 1.6 3.5 94.6 .3 4.1a 8.4 .920 358.0-359.0 2.0 3.4 93.0 1.6 5.6 8.1 .878 359.0-360.0 3.0 3.3 92.1 1.6 8.0 7.9 .886 360.0-361.0 3.5 3.2 91.5 1.8 9.7 7.7 .877 361.0-362.0 4.9 2.2 90.4 2.5 13.1 5.3 .899 362.0-363.0 1.6 2.1 95.4 .9 4.2a 5.0 .920 363.0-364.0 1.7 3.0 94.3 1.0 4.4a 7.2 .920
355.0-356.0 3.1 2.4 93.1 1.4 8.5 5.8 .877 356.0-357.0 2.0 1.3 95.9 .8 5.3 3.1 .886 357.0-358.0 1.6 3.5 94.6 .3 4.1a 8.4 .920 358.0-359.0 2.0 3.4 93.0 1.6 5.6 8.1 .878 359.0-360.0 3.0 3.3 92.1 1.6 8.0 7.9 .886 360.0-361.0 3.5 3.2 91.5 1.8 9.7 7.7 .877 361.0-362.0 4.9 2.2 90.4 2.5 13.1 5.3 .899 362.0-363.0 1.6 2.1 95.4 .9 4.2a 5.0 .920 363.0-364.0 1.7 3.0 94.3 1.0 4.4a 7.2 .920
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357.0-358.0 1.6 3.5 94.6 .3 4.1a 8.4 .920 358.0-359.0 2.0 3.4 93.0 1.6 5.6 8.1 .878 359.0-360.0 3.0 3.3 92.1 1.6 8.0 7.9 .886 360.0-361.0 3.5 3.2 91.5 1.8 9.7 7.7 .877 361.0-362.0 4.9 2.2 90.4 2.5 13.1 5.3 .899 362.0-363.0 1.6 2.1 95.4 .9 4.2a 5.0 .920 363.0-364.0 1.7 3.0 94.3 1.0 4.4a 7.2 .920
358.0-359.0 2.0 3.4 93.0 1.6 5.6 8.1 .878 359.0-360.0 3.0 3.3 92.1 1.6 8.0 7.9 .886 360.0-361.0 3.5 3.2 91.5 1.8 9.7 7.7 .877 361.0-362.0 4.9 2.2 90.4 2.5 13.1 5.3 .899 362.0-363.0 1.6 2.1 95.4 .9 4.2a 5.0 .920 363.0-364.0 1.7 3.0 94.3 1.0 4.4a 7.2 .920
359.0-360.0 3.0 3.3 92.1 1.6 8.0 7.9 .886 360.0-361.0 3.5 3.2 91.5 1.8 9.7 7.7 .877 361.0-362.0 4.9 2.2 90.4 2.5 13.1 5.3 .899 362.0-363.0 1.6 2.1 95.4 .9 4.2a 5.0 .920 363.0-364.0 1.7 3.0 94.3 1.0 4.4a 7.2 .920
360.0-361.0 3.5 3.2 91.5 1.8 9.7 7.7 361.0-362.0 4.9 2.2 90.4 2.5 13.1 5.3 899 362.0-363.0 1.6 2.1 95.4 9 4.2a 5.0 920 363.0-364.0 1.7 3.0 94.3 1.0 4.4a 7.2 920
361.0-362.0 4.9 2.2 90.4 2.5 13.1 5.3 .899 362.0-363.0 1.6 2.1 95.4 .9 4.2a 5.0 .920 363.0-364.0 1.7 3.0 94.3 1.0 4.4a 7.2 .920
362.0-363.0 1.6 2.1 95.4 .9 4.2a 5.0 .920 363.0-364.0 1.7 3.0 94.3 1.0 4.4a 7.2 .920
363.0-364.0 1.7 3.0 94.3 1.0 4.4a 7.2 .920
36/ 0-365 0
365 0-366 0
366 0.367 0
267 0 262 0
260 0 260 0
360 0 370 0
270 0 271 0
370.0-371.0 .6 2.4 96.6 .4 1.7a 5.8 .920
371.0-372.0 1.1 2.6 95.8 .5 2.9a 6.2 .920
372.0-373.0 1.3 2.4 95.0 1.3 3.5a 5.8 .920
373.0-374.0 1.7 2.3 95.3 .7 4.5a 5.5 .920
374.0-375.0 .7 .6 98.1 .6 1.8a 1.4 .920
375.0-376.0 1.0 2.6 95.8 .6 2.5a 6.2 .920
376.0-377.0 1.4 2.3 95.3 1.0 3.6a 5.5 .920
377.0-378.0 1.0 2.4 96.1 .5 2.6a 5.8 .920
378.0-379.0 .9 2.5 96.0 .6 2.4a 6.0 .920
379.0-380.0 1.3 2.9 95.1 .7 3.3a 7.0 .920

THE PERSON NAMED IN COLUMN OF STREET PARTY OF PERSONS ASSESSED.

Samples from the U.S. September Sample's Contents.

OIL-SHALE ASSAYS BY MODIFIED FISCHER RETORT METHOD Samples from the U.S. Geological Survey's Corehole

78-8	(Continued)	
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	-		Yield	of prod	uct		
Depth	-	Weight	percent			Specific	
rom To	011	Water	Spent shale	Cas +	Oi 1 2/	Water.	gravity of oil at 60°/60°
380.0-381.0	2.9	2.6	93.4				
381.0-382.0	1.6	.8	96.5	1.1	7.7	6.2	0.911
382.0-383.0	1.5	. 8		1.1	4.2a	1.9	. 920
383.0-384.0	2.5	1.4	96.0	7	3.9a	4.3	.920
384.0-385.0	3.3		95.0	1.1	6.5	3.4	.916
385.0-386.0	2.7	2.9	92.3	1.5	8.8	7.0	.898
386.0-387.0		3.2	92.7	1.4	7.4	7.7	.874
387.0-388.0	3.2	3.2	92.1	1.5	8.9	7.7	.874
388.0-389.0	1.9	2.1	94.9	1.1	4.9a	5.0	.920
389.0-390.0	1.5	1.5	95.5	1.5	3.9a	3.6	.920
390.0-391.0	3.9	2.9	91.0	2.2	10.4	7.0	.904
391.0-392.0	1.4	2.2	95.1	1.4	3.5a	5.3	.920
392.0-393.0	2.1	2.8	92.7	2.4	5.7a	6.7	.890
393.0-394.0	. 9	.9	97.2	1.0	2.4a	2.2	.920
	2.4	3.2	92.7	1.7	6.4	7.7	.882
394.0-395.0	2.9	3.4	91.9	1.8	7.6	8.1	.899
395.0-396.0	2.9	2.5	92.9	1.7	7.6	6.0	.907
396.0-397.0	3.1	2.7	92.2	2.0	8.0	6.5	.921
397.0-398.0	3.5	2.6	92.0	1.9	9.2	6.2	
98.0-399.0	3.1	2.6	92.5	1.8	8.1	6.2	.921
199.0-400.0	2.8	1.4	94.4	1.4	7.3	3.4	.907

[&]quot;a"-indicates specific gravity estimated as 0.92.

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The Continue Service Services

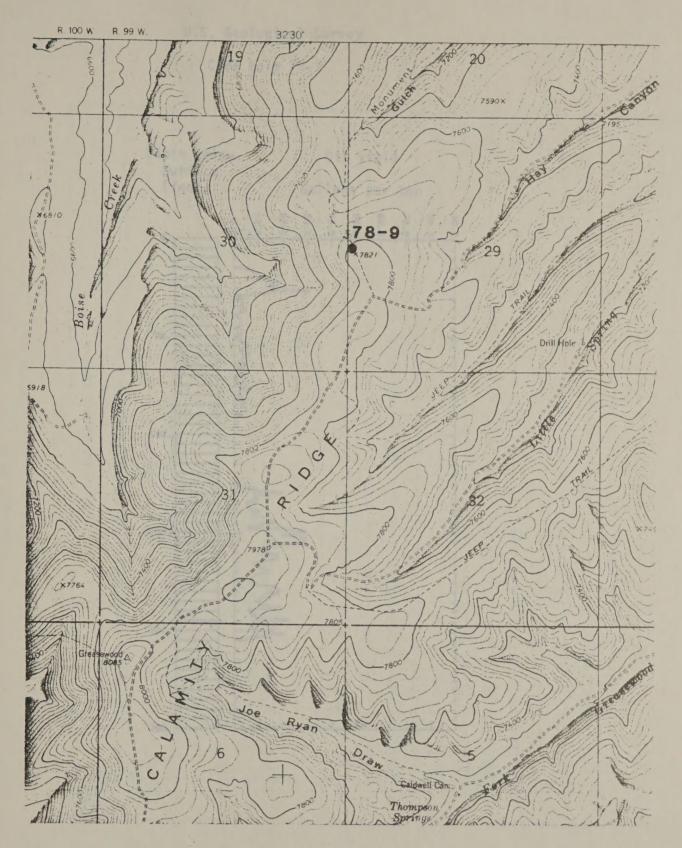


Figure 10.--Map showing location of core hole 78-9. Base from Calamity Ridge Quadrangle (1962). Scale 1:24,000.

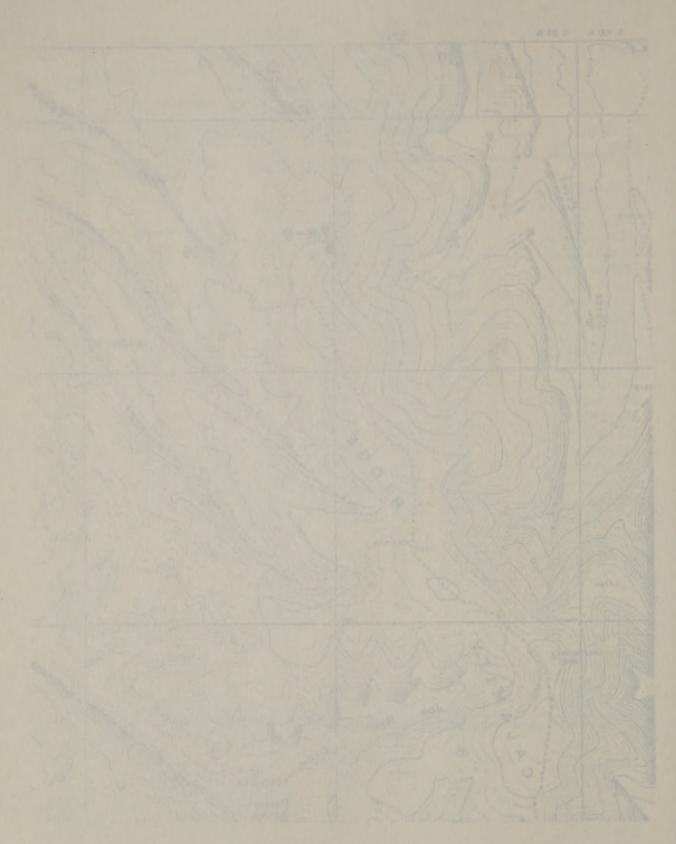
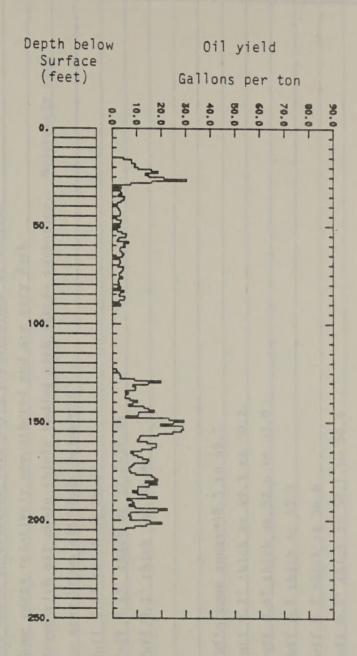


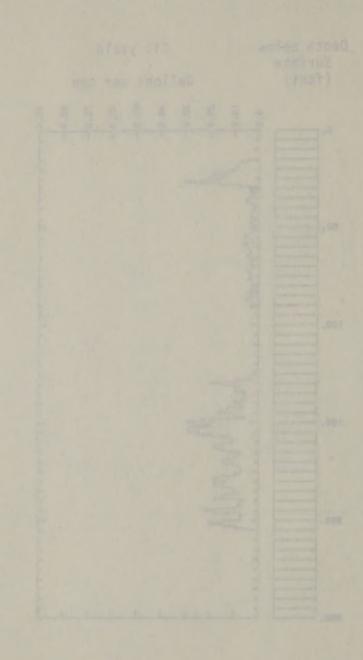
Figure 10 -- Map showing location of core hole 78-9. Base from Calconty Kidge Owadrangle (1962). Scale 1:24.000.

U.S. Geological Survey

Core hole 78-9



Carrie Tachpores, 2.0



FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION
15.0	91.9		Oll shale interbedded with tuff, bleached and weathered.
			Some parts relatively unweathered and are very dark
			Brown rich oil shale thinly bedded with little turbation. Moderately rich
			to gray brown oil shale below 50'
			Tuff 0.1' thick at 28.7'
			Tuff 0.15' thick at 32.7-32.85
			Tuff 0.1' thick at 36.8
			Tuffaceous zone 48.5 to 49.5
			Tuff 0.7' thick at 49.5 to 50.2
			Tuff 0.4' thick at 52.6 to 53.0
			Tuff 0.1 thick at 53.9
			Tuff 0.2 thick at 56.6
			Tuff 0.5' thick at 58.1 to 58.6
			Tuff 0.2 thick at 65.7' - 65.9'
			Oxidized leached zone with numerous open pits
			0.3' thick at 65.9' - 66.2
			Tuff_0.1 thick at 67.6' with minor shale
			Tuff 0.1' thick at 86.2
			Tuff 0.3' thick at 90.8'-91.1'

					,							

	FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION
	91.9	121.7		Tuffaceous zone, numerous thick and thin tuffs
				turbated and interlayered with some dark brown
				Oil shale. Tuffs are gray to dark gray. 380 percent tuff
	121.7	128.9		Brown to tan lean oil shale thinly interbedded and
				in parts turbated with thin tuffs. 650 percent tuff
130		*		At 127.15', 0.5' tuff with abundant solution cavities
0	128.9	134.4		Dark gray brown to black oil shale thinly interbedded
				with thin tuffs
	134.4	141.5		Brown to tan lean oil shale with abundant thinly interhedded tan tuff.
	141-5	204.9		Similar to interval 128.9 - 134.4'
				Tuff 0.15' thick at 143.6 - 142.75'
				Tan to brown oil shale with tuff 145.9' -147.0
				Tan to brown oil shale with tuff 158.3 - 160.6'
				Tuff 0.1' thick at 164.4'
				Tan to dark brown oil shale with tan thinly interbedded tuff. 166.0-169.4
				and 171.5 - 177.9'

FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION	
			Brown to dark gray brown oil shale interbedded with tan tuff.	-
			182.5 - 187.5'	
			and 188.9 - 204.9	
		-	,	
			THE PARTY OF THE P	
	access to making the displacement with a fill party.			
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OIL-SHALE ASSAYS BY MODIFIED FISCHER RETORT METHOD

Samples from the U.S. Geological Survey's Corchole 78-9 drilled in sec. 29, T. 2.N., R. 99 W., Rio Blanco County, Colorado

Dep	th		Weight	percent	of produ	NAME AND ADDRESS OF TAXABLE PARTY.	er ton	Specific gravity
				Spent	Gus +			of oil at
From	To	Oil	Water	shale	1065	011	Water	60°/60° F
15 16 17 18 19	16 17 18 19 20			93.8 94.6 93.9 93.2 92.6	2.8 1.1 1.2 1.4 1.7	4.6	4.0 3.0 4.5 4.2 5.5	.920 * .923 .923 .921 .916
20 21 22 23 24	21 22 23 24 25			92.6 90.5 87.4 88.9 87.8	1.4 1.9 2.7 2.2 2.5	10.6 16.0 18.7 13.5 14.9	4.7 3.6 6.6 9.2 9.5	.905 .905 .906 .911
25 26 27 28 29	26 27 28 29 30			85.5 83.2 88.9 92.2 94.9	2.9 3.1 2.3 1.8 1.6	21.2 30.4 16.1 7.5 N.D.	8.0 4.8 6.3 7.5 8.3	•933 •925 •923 •924
30 31 32 33 34	31 32 33 34 35			92.5 94.2 93.7 95.2 96.0	2.2 1.9 1.4 0.8 0.9	3.7 TRACE 3.3 3.9 2.5	9.3 9.3 8.7 6.0 5.2	.920 * .920 * .920 * .920 * .920 *
35 36 37 38 39	36 37 38 39 40			95.8 95.7 96.2 96.3 96.4	1.0 1.1 1.0 1.5 1.5	5.0 4.7 3.6 2.1 0.3	3.3 3.3 3.3 4.6	.920 * .922 .920 * .920 * .920 *
40 41 42 43 44	41 42 43 44 45			95.9 95.6 96.3 96.5 97.5	1.5 1.8 1.6 1.4	2.1 2.7 3.1 3.3 3.1	4.3 3.7 2.3 2.0 2.2	.920 * .920 * .920 * .920 *

DIL-SHAIL ASSAYS BY MODERN PROPER STATES TIME-110

Samples from the D.S. Coolegant Survey - Conclude van divilled to

Oll-Shalf ASSAYS BY MODIFIED FISCHER RETORT METHOD Semples from the U.S. Geological Survey's Corehole 78-9 (Continued)

			Theld of product								
			Weight	percent		The second secon	er ton	Specific gravity			
From	70	011	Water	Spent	loss			of oil at			
45 46 47 48 49	46 -47 48 49 50			97.6 97.6 97.0 96.9 98.5	0.7	0.5 1.7 3.6 3.3 0.7	3.5 3.6 2.4 1.9	.920 * .920 * .920 * .920 *			
50 51 52 53 54	51 52 53 54 55			97.9 96.9 96.4 96.2 95.2	Q.1 1.8 1.3 1.6	3.1 0.6 2.1 3.9 5.8	2.1 2.6 2.4 1.7 2.4	.920 * .920 * .920 * .920 *			
55 56 57 58 59	56 57 58 59 60			96.7 98.0 98.0 95.9 95.5	0.2 0.1 0.6 0.7	5.4 2.6 2.0 6.7	2.4 2.5 3.4 2.3 4.7	.920 * .920 * .920 * .917 .920 *			
60 61 62 63 64	61 62 63 64 65			95.6 97.0 97.2 95.9 95.8	0.3 0.3 0.6 0.3 0.9	5.2 3.2 3.0 3.8 4.7	L.1 2.4 2.4 4.4 3.6	.920 * .920 * .920 * .920 * .920 *			
65 66 67 68 69	66 67 68 69 70			94.3 95.4 95.1 95.5 95.7	0.8 1.2 1.3 1.3	4.0 TRACE 3.0 3.4 2.8	7.9 8.2 5.8 4.5 4.4	.920 * .920 * .920 * .920 *			
70 71 72 73 74	71 72 73 74 75			96.1 95.4 95.1 96.2 95.6	0.9 1.0 1.0 0.9 1.1	2.3 4.6 4.3 3.6 2.8	5.0 4.4 5.2 3.6 5.4	.920 * .920 * .920 * .920 *			
75 76 77 78 79	76 77 78 79 80			97.2 96.8 97.4 97.0 96.5	0.1 0.1 0.3 0.7	2.9 4.2 2.5 2.3 2.8	4.2 4.3 4.7 4.5 4.4	.920 * .920 * .920 * .920 * .920 *			

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OIL-SHALF ASSAYS BY MODIFIED FISCHER RETORT MITHOD

Samples from the U.S. Geological Survey's Corehole

78-9 (Continued)

					70-3				
	Depth		-			of procu	cı		Specific
			-	Weight	percent		Cas) p.	T EDT.	gravity
Prom	To		0:1	Water	Spent	Cas +	Oil	Water.	of oil at 60°/60° F
80 81 82 83 84	81 82 83 84 85				95.8 96.0 96.5 95.7 96.6	0.3 0.3 0.6 1.0 0.7	2.2 3.L TRACE 4.7 3.1	7.1 5.8 6.9 3.5 3.6	.920 * .920 * .920 * .920 * .920 *
85. 86. 87. 88.	86 87 88 89				96.5 96.5 95.7 96.8 97.3	0.5 0.1 1.3 1.2 0.9	2.7 5.1 4.8 2.7 TRACE	4.7 3.5 2.9 2.4 4.3	.920 * .920 * .920 * .920 * .920 *
90 91 96 101 106	91 95 100 105 110				96.7 97.2 98.8 97.9 98.3	1.1 1.4 0.1 0.6 0.6	3.4 TRACE N.D. N.D.	2.3 3.3 4.2 3.6 2.6	.920 * .920 *
111 116 120 123 124	115 120 122 124 125				98.4 97.7 96.4 96.2 97.0	0.5 0.4 1.2 1.2 0.8	N.D. N.D. N.D. 1.5	2.6 4.5 5.7 4.9 3.5	.920 * .920 *
125 126 127 128 129	126 127 128 129 130				97.4 96.4 96.5 94.2 87.9	0.6 1.6 0.9 1.0	2.7 3.2 3.0 9.0	2.3 1.8 3.6 3.2 6.6	.920 * .920 * .920 * .920 * .922 .928
130 131 132 133 134	131 132 133 134 135				90.4 93.6 93.7 94.3 95.3	2.2 1.4 1.3 0.6 0.8	14.5 8.1 9.4 9.2 5.1	4.4 4.6 3.3 3.6 4.7	.914 .912 .913 .921 .915
135 136 137 138 139	136 137 138 139 140				96.0 96.2 95.7 95.5 93.4	0.5 0.8 1.3 0.9 1.7	6.4 5.1 5.0 7.0 10.2	2.4 2.4 2.3 2.4	.912 .915 .920 * .916 .909

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OIL-SHALF ASSAYS BY MODIFIED FISCHER RETORT MITHOD Samples from the U.S. Geological Survey's Corehole 78-9 (Continued)

		-	Theld of product							
			Weight	percent		Cal p	7 201.	Specific gravity		
From	To	011	Water	Spent	Gas +	013-1/	Water.	of oil at		
140 141 142 143 144	141 142 143 144 145			94.8 96.0 91.6 89.9 90.2	1.1 0.6 1.5 1.9	8.2 6.4 12.8 14.7 17.0	2.5 2.4 4.7 5.8 3.5	.915 .930 .920 .934 .913		
145 146 147 148 149	146 147 148 149 150			93.2 93.5 9L.8 85.6 84.6	1.5 1.5 1.3 3.1 2.8	.10.5 10.4 5.2 23.0 29.1	3.1 2.3 4.6 5.7 3.5	.920 .921 .908 .927 .909		
150 151 152 153 154	151 152 153 154 155			86.5 86.9 84.4 84.7 85.1	2.5 2.7 2.8 2.3 2.4	24.8 19.4 28.6 28.9 28.0	3.6 7.2 4.8 4.8 4.2	.918 .920 .908 .910		
155 156 157 158 159	156 157 158 159 160			85.2 88.7 92.4 94.2 93.9	3.4 2.2 0.9 0.7 1.3	24.6 18.6 11.1 10.7 10.0	4.7 4.8 5.8 2.4 2.4	.918 .915 .922 .921		
160 161 162 163 164	161 162 163 164 165			91.3 88.5 88.4 89.1 91.5	2.0 2.7 2.6 2.2 1.8	14.1 17.9 17.8 16.0 11.7	3.1 4.9 5.2 5.9 5.1	.911 .915 .922 .930 .937		
165 166 167 168 169	166 167 168 169 170			95.0 95.3 94.2 93.0 90.9	0.7	7.3 8.4 10.2 12.2 14.8	3.5 2.3 2.4 2.4 4.8	.920 * .924 .916 .913 .914		
170 171 172 173 174	171 172 173 174 175			90.8 94.1 95.2 96.1 95.9	1.3 0.8 0.9 0.3 0.7	14.2 8.7 7.7 6.7 6.7	5.8 4.1 2.4 2.5 1.7	.929 .927 .911 .923 .933		

OIL-SHALF ASSAYS BY MODITIED FISCHER RETORT MITHOD

Semples from the U.S. Geological Survey's Corehole

78-9 (Continued)

		-		Yaeld c	of proc	uci		5
			Weignit	percent	, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		per ton	Specific gravity
Prom .	To	011	Water	Spent shale	Gas 4	Oil	Water.	of oil at 60°/60° F
175 176 177 178 179	176 177 173 179 180			95.5 94.4 90.9 90.5 89.3	0.7 1.0 2.0 1.4 1.8	7.3 9.4 16.0 17.2 18.4	2.4 2.4 3.5 4.6	.921 .911 .915 .926 .910
180 181 182 183 184	181 182 183 184 185			91.4 89.9 90.9 93.7 94.0	1.4 1.6 1.9 1.5 1.1	13.3 18.2 14.9 10.2 10.4	4.7 3.6 3.5 2.5 2.4	.934 .910 .917 .894 .886
185 186 187 188 189	186 187 188 189			94.6 94.8 93.0 89.3 96.1	1.3 0.4 0.8 1.3 0.6	8.1 10.3 14.0 18.2 5.8	2.4 2.2 2.1 5.8 2.7	.912 .902 .901 .914
190 191 192 193 194	191 192 193 194 195			95.3 94.5 94.5 94.5 87.4	1.0 1.2 1.8 1.1 2.3	8.0 8.8 6.7 9.2 22.3	1.7 2.3 3.0 2.3 4.3	.902 .913 .908 .913 .916
195 196 197 198 199	196 197 198 199 200			89.3 95.3 95.3 94.8 94.4	2.1 0.9 0.9 1.0 1.5	18.5 7.2 6.5 7.6 7.1	3.6 2.5 3.1 3.1 3.3	.920 .917 .908 .910 .924
200- 201 202 203 204	201 202 203 204 204.9			90.3 86.8 91.7 93.7 94.0	1.9 2.9 1.5 1.3 1.9	15.3 20.1 13.8 8.9 5.3	4.7 6.1 3.5 3.8 4.9	.922 .925 .937 .923 .932

^{*} Assumed Specific Gravity

Manager from the U.S. Spiriter Statement in comments and some and analysis

Assumed Specific Gravity

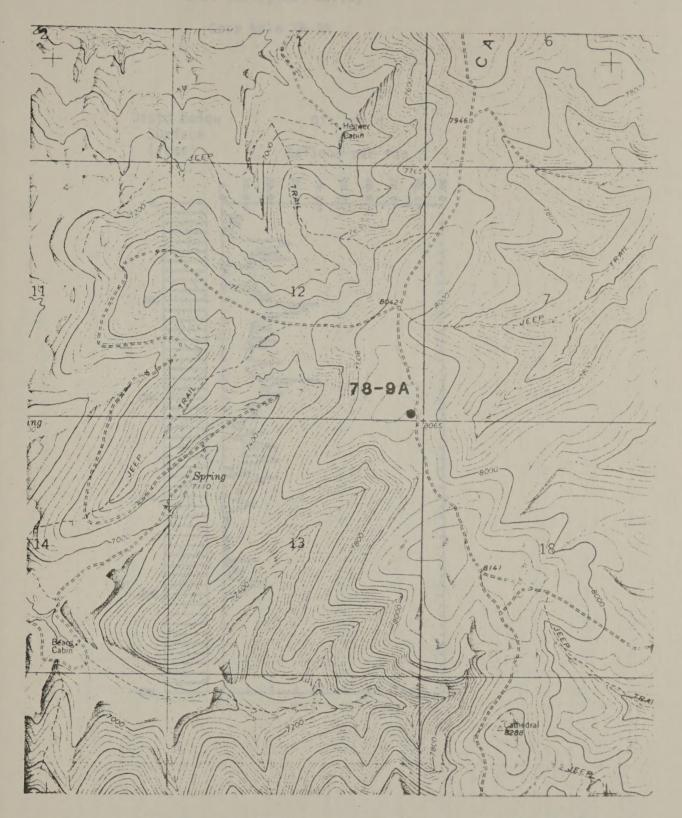


Figure 11.--Map showing location of core hole 78-9A. Base from Calamity Ridge Quadrangle (1962). Scale 1:24,000.

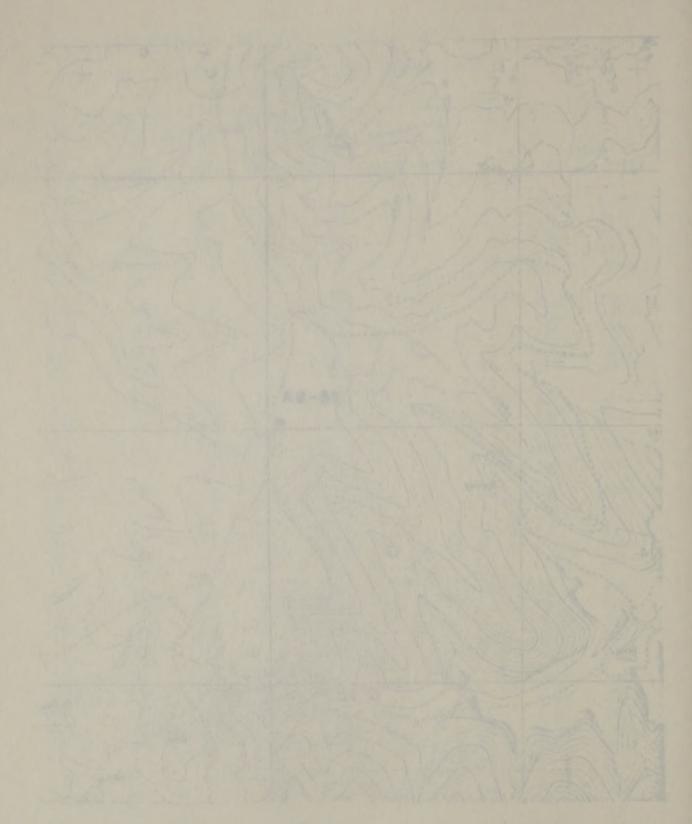
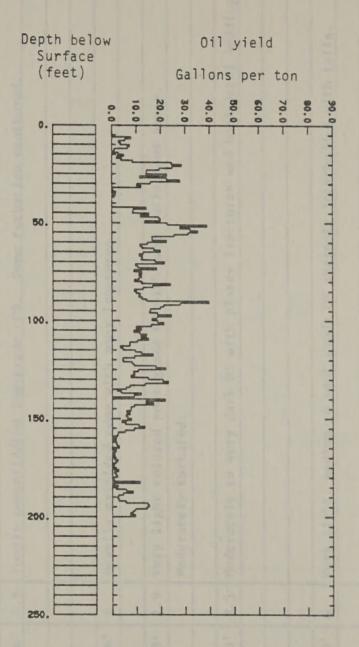


Figure 11. -- Map showing location of core hole 18-9A. Bero from (when.cy 610go Ouadrangle (1962). Scale 1:24:000.

U.S. Geological Survey

Core hole 78-9A



U.S. Sanlagical Survey Core note 32-sa

Corehole 78-9A Logged by Steven Ihnen

FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION	
6'	12.6'	6.6	Poorly consolidated low-grade OS, Some turbation weathered.	
12.6'	16.6'	4	Heavily oxidized zone with many fractures	
16.6'	18.5'	1.9	Very light colored poor-grade OS with some tuffaceous areas. Moderately turbated.	
18.5'	21.0'	3.5	Moderately to very dark OS with platey fractures and horizontal bedding	
21.0'	27.0'	6	Very light, medium to poor grade OS sparsely interhedded with tuffs.	
27.0'	29.6'	2.6	Medium brown mildy turbated medium grade OS.	
29.61	31.0'	1.4	Oxidation zone.	
31.0'	32.0'	1	Similar to 21'-27' above.	
32.0'	33.5'	1.5	Oxidation zone.	

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	NESS	
37.0'	3.5	Medium brown, poor to fair grade OS turbated tuff at 35.2' (0.3' thick)
43.0'	6	Oxidized shale
47.4	4.4	Light, poor to medium grade OS
61.0'	24.6	Mixed light to medium, fair to poor-grade OS tuff at 52.6'.
61.5	1.2	Oxidation/tuff zone
65.0'	3.5	Dark fairly rich OS
81.0'	16	Light poor grade OS
82.5	1.5	Tuffaceous zone ->50% tuffs in beds
88 '	5.5	Same as 65-81 above
93	5	Somewhat darker, finely bedded poor-grade shale
20		Mixed light to medium brown, poor to fair grade shales thinly interbedded with tuffs. Some occurrence of salt.
	47.4' 61.0' 61.5 65.0' 81.0' 82.5'	47.4' 4.4 61.0' 24.6 61.5 1.2 65.0' 3.5 81.0' 16 82.5' 1.5 88' 5.5 93' 5

FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION
120'	120.4	.4	Tuff zone.
120.4'	131.4'	11	Same as 82.5-88 above.
131.4'	133.0'	2.6	Darker, vertically fractured material.
133.0'	138.5'	5.5	Very light poor OS.
138.5'	140.4	1.9	Major tuff zone oxidation in fracture.
140.4'	142.0'	1.6	Darker mixed OS.
142.0'	161.6'	19.6	Very light very poor grade OS.
161.6'	161.9'	0.3	Very dark banded segment.
161.9'	164.5'	2.6	Similar to 142-161 above.
164.5'	167.5'	3.0	Siltstone?
167.5'	193.6		Similar to 142-161 above interspersed w/higher grade OS in small bands.
			Fairly tuffaceous below -187.
	-		

	-	

FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION		
193.61	196.0	2.4	Dark-brown fairly rich OS heavily fractured.		
196.0	200.0		Light-brown low-grade OS.		
	·				
			ENAMED RESERVED BY BURNING STREET		
				I TO A REPORT OF	200
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OIL-SHALE ASSAYS BY MODIFIED PISCHER RETORT METHOD

Samples from the U.S. Geological Survey's Corchole 78-9A drilled in sec. 12, T. 1 N., R. 100 W.Rio Blanco County, Lororado

	***************************************		Yield	DÍ DECL	fuer.		
Depth		WELVILL	percent	31 1100	The second secon		Specific
51.0-11.0			Spent	Caus 4		er ton	ETAVITY
From To	Oil	Water	shale	loss	0112/	Ness	of oil at
					012	Water	60.160. E
(070					200		
6.0-7.0	3.0	2.8	91.2	3.0	7.8	6.7	0.934
7.0-8.0 8.0-9.0	2.1	3.0	93.4	1.5	5.4	7.2	.934
9.0-10.0	1.1	3.6	94.0	1.3	2.8a	8.6	
10.0-11.0	1.4	2.2	95.0	1.4	3.6a	5.3	
11.0-12.0	2.8	2.3	93.4	1.5	7.3	5.5	.926
12.0-13.0	2.4	2.0	94.4	1.2	6.4	4.8	.921
	.4	4.5	94.1	1.0	1.la	10.8	
13.0-14.0	.3	1.6	97.3	. 8	. 8a	3.8	
14.0-15.0	1.0	1.5	96.2	1.3	2.7a	3.6	
15.0-16.0	1.9	1.3	95.7	1.1	4.9a	3.1	
16.0-17.0	.8	1.4	96.8	1.0	2.0a	3.4	
17.0-18.0	1.5	.8	96.9	.8	3.9a	1.9	
18.0-19.0	3.2	1.3	94.2	1.3	8.5	3.1	.919
19.0-20.0	9.5	2.6	85.4	2.5	24.5	6.2	.932
20.0-21.0	11.0	3.7	81.9	3.4	28.6	8.9	.924
21.0-22.0	9.5	2.1	85.6	2.8	24.7	5.0	.918
22.0-23.0	7.4	2.1	88.3	2.2	19.4	5.0	.914
23.0-24.0	5.4	1.8	90.7	2.1	14.2	4.3	.913
24.0-25.0	5.3	1.7	91.5	1.5	14.0	4.1	.912
25.0-26.0	8.7	2.1	86.8	2.4	22.6	5.0	.926
26.0-27.0	4.4	2.1	92.0	1.5	11.4	5.0	.915
27.0-28.0	8.6	2.4	86.3	2.7	22.5	5.8	.917
28.0-29.0	10.7	2.1	84.4	2.8	27.9	5.0	.916
29.0-30.0	6.1	2.3	89.7	1.9	15.8	5.5	.924
30.0-31.0 31.0-32.0	3.9	1.0	93.6	1.5	10.2	2.4	.906
32.0-33.0	.0	1.0	93.3	1.2	11.9	2.4	.903
33.0-34.0	.1	1.9	96.4	1.3	Trace	7.2	
34.0-35.0	.6	1.1	97.8	.5	.3a 1.6a	4.6 2.6	
35.0-36.0	.6	1.0	97.9	.5	1.5a		
36.0-37.0	0.4	0.9	98.2	0.5	1.0a	2.4	
37.0-38.0	.0	2.5	97.2	. 3	No oil	5.9	
38.0-39.0	.0	3.1	96.6	. 3	No oil	7.3	
39.0-40.0	.0	2.6	97.1	. 3	No oil	6.2	
40.0-41.0	.0	2.8	96.8	.4	No oil	6.6	
41.0-42.0	.0	3.6	96.0	.4	No oil	8.7	
42.0-43.0	5.4	1.9	90.7	2.0	14.1	4.6	0.911
43.0-44.0	3.3	2.0	93.0		8.7	4.8	.916
44.0-45.0	3.2	1.4	94.2	1.2	8.5	3.4	.912
45.0-46.0	5.8	1.4	90.6		15.2	3.4	.911
46.0-47.0	4.4	1.5	92.6	1.5	11.7	3.6	.913
47.0-48.0	7.4	2.3	88.3	2.0	19.3	5.5	.919
48.0-49.0	7.7	2.5	87.4	2.4	19.9	6.0	.931
40.0 47.0							

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Samples from the U.S. Geologics Survey's Corehole 78-9A (Continued)

			78-9A	(Cont.	inued)		
		Waters	Yield	of pro	duct		Specialist
Depth	-	Weight	The second second	AND DESCRIPTION OF THE PERSON NAMED IN	GE]	per ton	Specific gravity
From To	011	Water	Speni	loss	+	1	of oil a
					013	Water.	60.160.
49.0-50.0	5.2	1.7	92.0	1.1	13.5	4.1	.919
50.0-51.0	8.6	1.6	87.6	2.2	22.7	3.8	.906
51.0-52.0	14.7	1.5	80.0	3.8	38.9	3.6	.907
52.0-53.0	10.6	2.2	84.6	2.6	27.8	5.3	.914
53.0-54.0	12.3	2.4	82.3	3.0	32.1	5.8	.919
54.0-55.0	13.5	2.1	80.9	3.5	35.1	5.0	.920
55.0-56.0	11.9	2.5	82.2	3.4	31.2	6.0	.913
56.0-57.0	. 10.7	2.5	85.1	2.7	25.4	6.0	
57.0-58.0	6.3	1.7	90.1	1.9	16.4		.917
58.0-59.0	6.2	1.3	90.7	1.8	16.4	4.1	.922
59.0-60.0	8.5	2.6	86.3	2.6		3.1	.909
60.0-61.0	5.6	2.4	90.1		22.3	6.2	.912
.61.0-62.0	4.4	2.0	92.1	1.9	14.5	5.8	.930
62.0-63.0	4.8	1.3		1.5	11.4	4.8	.933
63.0-64.0	6.6		92.3	1.6	12.3	3.1	.926
64.0-65.0	7.6	1.3	90.5	1.6	17.2	3.1	.916
65.0-66.0		2.1	88.2	2.1	19.8	5.0	.925
66.0-67.0	4.9	1.6	91.9 93.2	1.6	12.7	3.8	.928
67.0-68.0	4.8	1.4	92.4	1.4	11.1	2.6	0.929
68.0-69.0	4.6	1.3		1.4	12.4	3.4	.932
69.0-70.0	6.8	1.3	92.9	1.2	12.0	3.1	.924
70.0-71.0	8.2	1.8	90.3	1.6	17.7	3.1	.915
71.0-72.0	3.6	1.8	88.1	1.9	21.5	4.3	.917
72.0-73.0	4.0		92.5	2.1	9.6	4.3	.915
73.0-74.0	6.9	1.2	93.5	1.3	10.6	2.9	.898
74.0-75.0		2.0	89.0	2.1	18.3	4.8	.910
75.0-76.0	3.4	1.2	94.1	1.3	9.0	2.9	.922
76.0-77.0	4.7	1.4	92.3	1.6	12.3	3.4	.920
	4.2	1.4	92.2	2.2	11.0	3.4	.922
77.0-78.0	4.7	1.7	92.1	1.5	12.1	4.1	-920
78.0-79.0	4.2	1.3	92.4	2.1	11.0	3.1	.920
79.0-80.0	3.5	1.6	93.2	1.7	9.2	3.8	.922
80.0-81.0	4.7	1.9	91.9	1.5	12.2	4.6	.916
81.0-82.0	9.3	2.5	85.0	3.2	23.9	6.0	.930
82.0-83.0	6.4	1.6	90.4	1.6	16.7	3.8	.925
83.0-84.0	4.9	1.8	91.9	1.4	12.7	4.3	.922
84.0-85.0	3.5	2.4	92.9		9.1	5.8	.925
85.0-86.0	3.8	1.5	93.2	1.5	9.9	3.6	.925
86.0-87.0	4.4	1.5	94.4	1.7	11.5	3.6	
87.0-88.0	4.2	1.6	92.8	1.4	11.0	3.8	.923
88.0-89.0	4.7	1.6	92.1	1.6	12.3		.915
89.0-90.0	5.4	1.7	91.1	1.8	14.2	3.8	.912
90.0-91.0	14.9	1.9	79.3	3.9	39.7	4.1	.909
91.0-92.0	10.5	1.5	85.4	2.6		4.6	.900
92.0-93.0	7.9	1.2	89.0		27.9	3.6	.905
93.0-94.0	7.3	1.2	89.4	1.9	21.1	2.9	.893
94.0-95.0	6.0	1.0	91.2		19.7	2.9	.894
95.0-96.0	5.8	1.2		1.8	15.7	2.4	.911
2310 3010	3.0	1.4	91.1	1.9	15.3	2.9	.911

NAME OF TAXABLE PERSONS ASSURED IN COLUMN 2 ASSURED

Searches from the United Seasons of Seasons

Samples from the U.S. Geological Survey's Corehole 78-9A(Continued)

	See and	Weight	11619	of pro	cuci		Street
Depth	-	mergint		-	Ga]	per ton	Specific
Frem To	012		Spent	Gas	+		gravity
	01:	Water	shale	loss	011	Water	of oil a 60°/60°
96.0-97.0	7.1	0.0	00.0				00 /60
97.0-98.0		0.9	89.8	2.2		2.2	0.920
98.0-99.0	9.1	1.5	87.3	2.1	24.2	3.6	.904
99.0-100.0	7.0	1.5	89.6	1.9	18.5	3.6	.910
	6.2	1.4	90.9	1.5	16.4	3.4	.909
100.0-101.0	7.1	1.6	89.5	1.8	18.7	3.8	.909
101.0-102.0	8.0	1.7	88.1	2.2	21.1	4.1	.910
102.0-103.0	6.2	1.5	90.2	2.1	16.0	3.6	.921
103.0-104.0	3.8	1.7	93.4	1.1	9.8	4.1	
104.0-105.0	4.6	1.3	92.8	1.3	12.0	3.1	.926
105.0-106.0	3.4	1.3	94.3	1.0	8.8		.928
106.0-107.0	4.4	1.5	92.7	1.4		3.1	.926
107.0-108.0	5.4	1.6	91.6		11.4	3.6	.923
108.0-109.0	4.5			1.4	14.1	3.8	.920
109.0-110.0	5.8	2.1	91.9	1.5	11.8	5.0	.919
110.0-111.0		2.2	90.7	1.3	14.9	5.3	.934
111.0-112.0	4.0	2.0	92.8	1.2	10.3	4.8	.929
	2.7	1.6	94.9	. 8	7.1	3.8	.924
112.0-113.0	2.8	2.0	94.3	.9	7.3	4.8	.920
113.0-114.0	1.3	2.0	96.2	.5	3.4a	4.8	.,,,,
114.0-115.0	1.7	1.5	96.1	.7	4.4a	3.6	
115.0-116.0	3.6	1.9	93.2	1.3	9.5	4.6	000
116.0-117.0	4.5	2.0	92.2	1.3	12.0		.909
117.0-118.0	6.3	1.5	90.8	1.4	16.8	4.8	.904
118.0-119.0	3.4	1.8	93.7			3.6	.904
119.0-120.0	1.7	3.0	94.2	1.1	9.1	4.3	.898
120.0-121.0	1.7	3.4		1.1	4.4a	7.2	
121.0-122.0	3.0		93.7	1.2	4.5a	8.1	
122.0-123.0	3.4	2.1	93.8	1.1	8.1	5.0	.905
23.0-124.0	6.9	2.2	93.2	1.2	8.9	5.3	.922
24.0-125.0		2.0	89.5	1.6	17.9	4.8	.923
25.0-126.0	8.4	1.5	88.4	1.7	21.9	3.6	.914
26.0-127.0	4.1	1.4	93.2	1.3	10.6	3.4	.921
27.0-128.0	3.3	1.2	94.2	1.3	8.7	2.9	.919
28.0-129.0	3.4	1.1	94.3	1.2	9.1	2.6	.905
29.0-130.0	2.9	2.1	93.9	1.1	7.7	5.0	.901
	5.7	1.7	90.2	2.4	14.8	4.1	.916
30.0-131.0	7.9	1.6	88.4	2.1	20.8	3.8	.911
31.0-132.0	8.8	1.8	87.4	2.0	22.9	4.3	.925
32.0-133.0	5.2	1.7	91.4	1.7	13.5	4.1	.921
33.0-134.0	2.8	2.0	94.3	.9	7.3	4.8	.920
34.0-135.0	2.2	1.9	95.1	. 8	5.7	4.6	.920
35.0-136.0	. 8	2.0	96.7	.5	2.1a	4.8	. 720
36.0-137.0	1.4	1.3	96.8	.5	3.7a	3.1	
37.0-138.0	4.5	1.7	92.6				036
38.0-139.0	3.4			1.2	11.9	4.1	.916
39.0-140.0			92.7		8.9	5.8	.916
40.0-141.0	.3				.7a	10.5	4893
41.0-142.0	8.3		88.0	1.9		4.3	.917
			92.7		13.7	1.9	.916
42.0-143.0	6.5	1.3	90.4	1.8	17.0	3.1	.913

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OIL-SHALE ASSAYS BY MODILIED FISCHER RETORT MITHOD

Samples from the U.S. Geological Survey's Corehole 78-9A (Continued)

	-		/8-9A		inued)		
	-		Yzeld	of pro	cuct		S. Commercial Commerci
Depth	-	Weight	percen	1	Ge 1	per ton	Specific gravity
From To	011	Water	Spent	Gas	4	1/	of oil at
184-0-187.0		2 3 3	BUIET.E.	loss	013-	Water	60°/60° F
143.0-144.0	3.5	1.5					
144.0-145.0	3.0	1.5	93.8	1.2	9.0	3.6	.924
145.0-146.0	2.9	1.5	94.5	1.0	7.7	3.6	.924
146.0-147.0	2.3	2.0	93.9	1.1	7.6	5.0	.924
147.0-148.0	2.8	2.0	95.0	. 7	5.9	4.8	.927
148.0-149.0	2.2	1.8	94.3	.9	7.2	4.8	.925
149.0-150.0	2.4	1.6	95.3	. 7	5.7	4.3	.919
150.0-151.0	3.0	1.4	95.2	. 8	6.3	3.8	.923
151.0-152.0	1.5	2.5	94.3	1.3	7.8	3.4	.921
152.0-153.0	2.1	2.0	95.3	.6	4.0a	6.0	
153.0-154.0	4.2	2.4	91.6	.6	5.5	4.8	.920
154.0-155.0	5.1	2.7	90.3	1.8	10.9	5.8	.924
155.0-156.0	3.4	2.7	92.2	1.9	13.3	6.5	.923
156.0-157.0	2.0	2.8	93.9	1.3	9.0	6.5	.921
157.0-158.0	.9	2.7	95.7	.7	2.4a	6.7	0.910
158.0-159.0	. 8	3.9	94.7	.6	2.2a	6.5 9.3	
159.0-160.0	. 3	5.0	94.0	. 7	.8a	12.0	
160.0-161.0	. 6	4.2	94.7	. 5	1.6a	10.1	
161.0-162.0	. 2	4.1	95.2	.5	.6a	9.8	
162.0-163.0	. 6	3.2	95.6	.6	1.7a	7.7	
163.0-164.0	. 8	2.9	95.0	1.3	2.0a	7.0	
164.0-165.0	1.1	1.2	97.0	. 7	2.8a	2.9	
165.0-166.0	. 2	.9	98.4	.5	.4a	2.2	
166.0-167.0	. 6	1.4	97.3	. 7	1.5a	3.4	
167.0-168.0	. 3	1.3	97.8	. 6	.8a	3.1	
168.0-169.0	. 4	1.5	97.6	. 5	.9a	3.6	
169.0-170.0	-4	1.5	97.5	.6	1.0a	3.6	
170.0-171.0	. 4	1.6	97.1	.9	1.1a	3.8	
171.0-172.0	. 8	1.7	96.4	1.1	2.2a	4.1	
172.0-173.0	.5		97.0	. 5	1.4a	4.8	
173.0-174.0	. 3	1.7	97.1	.9	70	4.1	
174.0-175.0	. 2	1.5	97.7	. 6	. 5a	3.6	
175.0-176.0	.3	2.5		. 7	.9a	6.0	
176.0-177.0	1.0	2.3	96.0	. 7	2.5a	5.5	
177.0-178.0	.4		96.3	1.0	1.0a	5.5	
178.0-179.0	.6		95.8	1.0	1.5a	6.2	
179.0-180.0	. 8		95.3	1.0	2.1a	7.0	
180.0-181.0	. 2		96.3		.6a	6.5	
181.0-182.0	. 3		95.4	.9	.7a	8.1	
182.0-183.0	4.2		91.6		11.3	5.8	.893
183.0-184.0	. 3		95.2		.7a	8.6	
184.0-185.0	.9		6.7		2.4a	3.6	
185.0-186.0	.6	.9 9	7.6	. 9	1.5a	2.2	

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			Total .	
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OIL-SHALE ASSAYS BY MODITIED FISCHER RETORT MITHOD

Samples from the U.S. Geological Survey's Corehole 78-9A (Continued)

		Vadana	Yzeld (of produ	ici		50
Depth		Weight	-		Gel pe	T ton	Specific
From. 70	011	Water	Spent	Cas +	0111/	Water.	of oil a 60°/60°
186.0-187.0 187.0-188.0 188.0-189.0 189.0-190.0 190.0-191.0	2.2 3.2 1.7 1.0	0.8 .9 .7 .7	95.8 94.5 96.5 97.4 97.4	1.2 1.4 1.1 .9	5.8 8.4 4.4a 2.5a 2.2a	1.9 2.2 1.7 1.7	0.912
192.0-193.0 193.0-194.0 194.0-195.0 195.0-196.0 196.0-197.0 197.0-198.0 198.0-199.0	1.0 2.1 5.5 5.8 5.4 3.6 3.2 2.8 3.5	.8 1.0 1.2 1.4 1.7 1.5 .9 1.0	97.2 95.7 91.3 90.6 90.9 93.3 94.1 94.8 94.0	1.0 1.2 2.0 2.2 2.0 1.6 1.8 1.4	2.7a 5.6 14.5 15.1 14.1 9.3 8.4 7.4 9.3	1.9 2.4 2.9 3.4 4.1 3.6 2.2 2.4 2.4	.919 .913 .920 .914 .912 .912 .911

^{1/ &}quot;a"--indicates specific gravity estimated as 0.92.

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complex from the U.S. (antiques) turney's Carefully

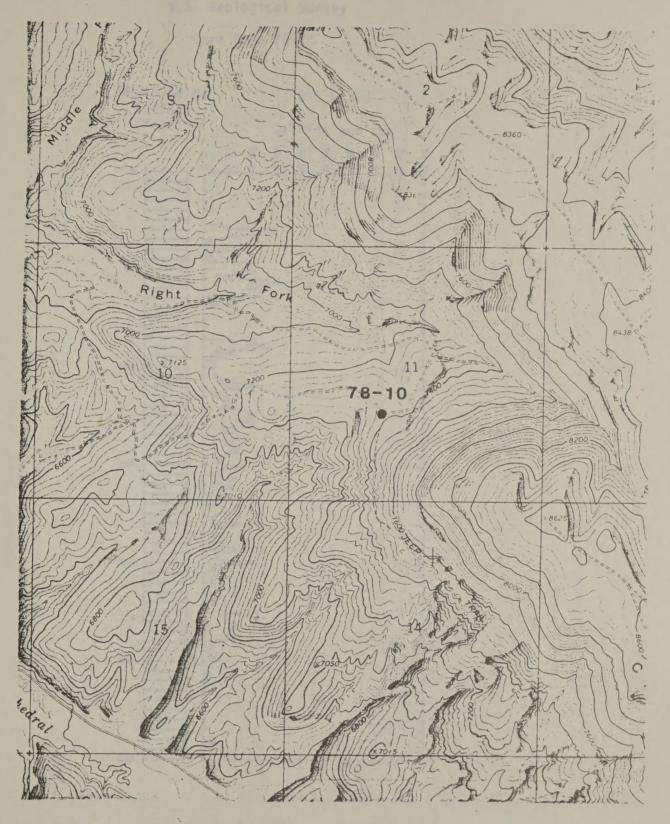


Figure 12.--Map showing location of core hole 78-10. Base from Black Cabin Gulch Quadrangle (1964). Scale 1:24,000.

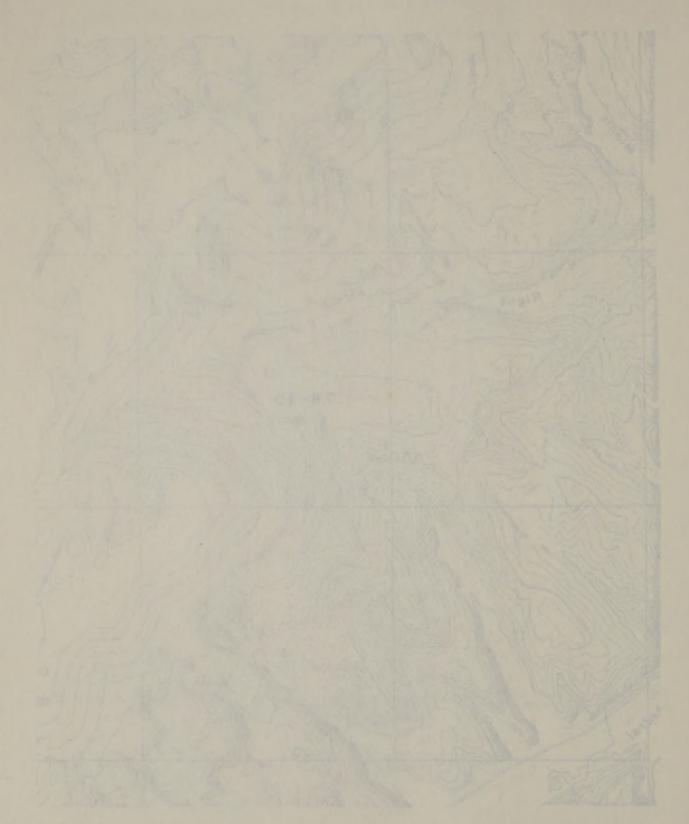
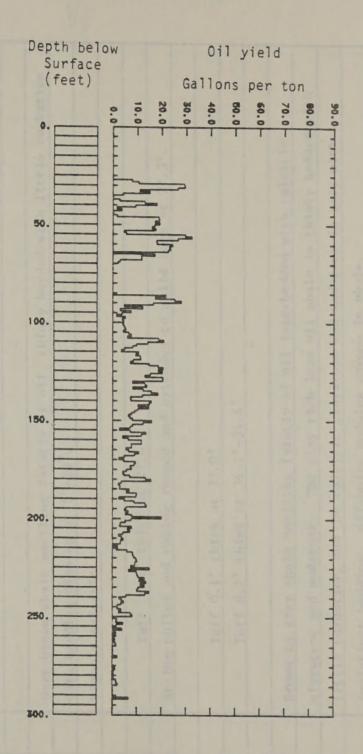
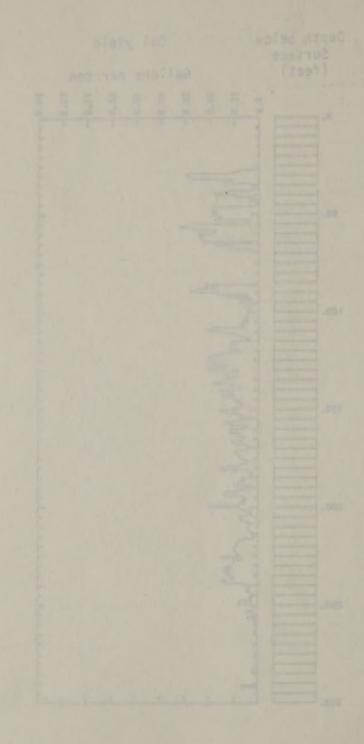


Figure 12.--Map showing location of core loly 26-10. Each fire Drack Canth. Gulen Quadrangle (1964). Scale 1:24,600

U.S. Geological Survey

Core hole 78-10





FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION
20.0'	27.3'		Loose slope debris, discarded
			become and the control of the contro
27.3'	34.9'		Dark-brown shale smelling faintly of oil, thinly bedded with little turbation
			with bedding dipping at 5°-20°.
			Sightly calcitic.
			THE RESERVE THE PROPERTY OF TH
			Tuff 0.1' thick at 27.6'
			String pulled and casing reamed and extended to solid rock at 27.3'.
			Character and the state of the
			Tuff 0.1' thick at 32.0'
			Tuff 0.2' thick at 34.2'-34.4'
34.91	104.4'		Brown to gray shale smelling faintly of oil interbedded with calcitic
			claystone and mudstone. The clay rich lean oil shale is thinly bedded with
			little turbation, and the calcitic claystone and mudstone is gray with
			indistinct bedding. Glisonite nodules common in shale.
			AND THE RESERVE OF THE REAL PROPERTY OF THE REAL PR
			Claystone 34.9'-38.3', 3.4' thick
			Mudstone 42.6'-45.5', 2.9' thick with shale chips
			Tuff (Dolomite?) 0.7' thick at 54.0'-54.7' with minor shale
			Tuff 0.1' thick at 57.6'
			the contract of the contract o
			New Addition of the annual Columns of the Columns o

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FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION
			Dolomite 0.2' thick at 62.2'-62.4', with shale and ostrocods. Mudstone with
			minor shale and abundant shale chips from 68.2'-85.0-, 17.8' thick. Gray and
			calcitic, poorly bedded with some thinly bedded to highly turbated shale.
			Tuff 0.2' thick at 83.2'-83.4'
			Tuff 0.1' thick at 85.0'
			Moderately rich oil shale 85.1'-91.3', 6.2' thick
			Claystone, 92.3'-97.0', 4.7' thick, thinly bedded
			PRODUCT SOLD STORES OF STORES
			- Polit Will think or to be
104.4"	121.2'		Brown to gray lean oil shale thinly and horizontally bedded, calcareous.
			Abundant scattered and bedded ostrocods.
			per ruson limitable Call remak of Dalar
			Ostrocod limestone 0.3' thick at 108.2'-108.5'
			Ostrocod limestone 1.0' thick at 109.2'-110.2' oil saturated.
			Ostrocod limestone 0.6' thick at 110.9'-111.5'
			Ostrocod limestone 0.1' thick at 115.3'
			Brittle, Massive limestone 0.2' thick at 121.0'-121.2'
121.2'	257.3'		Dark brown to gray moderately lean to lean oil shale, thinly bedded with
-			little turbation. Mainly noncalcareous with some light-colored calcilic

Countrale 78-10 (Continued)

FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION
			Calcitic light colored shale 128.4'-129.3', 0.9' thick
			Calcitic light colored shale 132.8'-133.5', 0.7' thick
			Bivalve fossils or mud flakes 0.1' thick at 135.5'
			Tuff 0.1' thick at 140.4'
			Tuff 0.1' thick at 145.3'
			Ostrocods dolomite 0.2' thick at 150.9'-151.1'
			Ostrocods dolomite 0.5' thick at 153.5'-154.0'
			Tuffaceous zone 1.7' thick at 157.6'-159.3' ~50% shale
			Tuff 0.2' thick at 160.4'-160.6'
			Tuff 0.1' thick at 161.3'
			Tuff 0.1' thick at 161.8'
			Ostrocod limestone 0.3' thick at 162.3'-162.6'
			Ostrocod limestone 0.1' thick at 163.9'
			Ostrocod limestone 0.1' thick at 164.7'
			Tuff 0.1' thick at 168.0'
			Limestone 0.1' thick at 170.8' Stromatolites?
			Limestone 0.1' thick at ~171.7'
			Dolomite 0.4' thick at 175.05'-175.45'
			Ostrocod limestone 0.3' thick at 176.7'-177.0' turbated
			Ostrocod limestone 0.3' thick at 180.7'-181.0' oil stained
	e abbillionity and the commenced service		Dolomite 0.2' thick at 187.8'-188.0' with minor shale
			Limestone 0.1' thick at 188.5' stromatolites?
			Limestone 0.2' thick at 189.3'-189.5'
	THE WASHINGTON TO SHE WASHINGT		Ostrocod Ilmestone 0.2' thick at 194.0'-194.2'

FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION
			Limestone 0.2' thick at 194.4'-194.6'
			Dolomite 0.1' thick at 198.9'
			Dolomite 0.1' thick at 200.1'
			Dolomite 0.2' thick at 200.8'-201.0'
			Dolomite 0.1' thick at 202.6'
			Limestone 0.6' thick at 203.2'-203.8' with minor shale
			Ostrocod limestone 0.1' thick at 210.7'
			Ostrocod limestone 0.3' thick at 212.3'-212.6'
			Ostrocod limestone 0.2' thick at 215.4'-215.6'
			Dark brown moderately lean oil shale 216.2'- thick, with abundant
			lighter colored beds and stromatolites.
			Dolomite 0.1' thick at 217.9' stromatolites
			Dolomite 0.1' thick at 224.7'
			Dolomite 0.3' thick at 224.8'-225.1' stromatolites
			Dolomite 0.4' thick at 226.7'-227.1' ostrocods
			Dolomite 0.5' thick at 228.5'-229.0' ostrocods with minor shale
		-	Limestone 0.1' thick at 223.6' oil stairs, ostrocods
			Limestone 0.2' thick at 223.8'-224.0' oil stained, ostrocods
		-	
257.3'	271.0'		Gray to brown poorly bedded calcareous claystone with abundant bivalve fossils.

FROM	то	THICK- NESS				LITHOLOGIC DE	SCRIPTION		
271.0	297.5'		Mudsto	ne, siltsto	ne, and dirty	poorly sort	ed sandstone	, gray and la	rgely
Bottom	of hole		calcit	ic, interbe	dded on a sca	le of about	2'.		
			Lime	stone, dolo	mite, lean ol	l shale, and	tuff were of	ten calcitic	and
			text	urally quit	e stmilar and	may be some	what confused	in this log.	
			Slick	kensides co	mmonly ranged	from horizon	ntal to 60° a	nd were rarel	y curved.
			Stria	ations were	usually para	llel to the o	din and rarel	y parallel to	strike.
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			P 12 14						
	-								
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- Company						angantus estimatibus de la companya	The second secon		

DIL-SHALE ASSAYS BY HODIFIED FISCHER RETORT METHOD

Samples from the U.S. Geological Survey's Corehele 78-10drilled in sec. 11, T. 3 S., R. 100 W., Rio Blanco County, Lolorado

		a management					
		-	Yield :	i produ	ict		Spanis
Dep	th		Weight percent		Gol pe	r ton	Specific gravity
From	To	0i1	Spent	Cas +			of oil at
1.0111	10	011	Water shale	1055	011	Water	60°/60° F
27	28		91.3	1.5	7.9	10.4	860
28	29		90.0	1.6	10.6	10.8	.869 .885
29	30 '		83.7	2.4	29.2	6.9	.904
30	31		81.5	2.8	29.5	10.9	.906
31	32		81.2	3.0	26.5	13.9	.906
32	33		89.9	2 3	11.0	9.3	.853
32 33 34 35 36	33 34		88.6	2.3	15.1	9.8	.871
34	35 36		93.5	0.7	4.1	10.1	.920*
35	· 36		94.3	0.1	TRACE	13.4	-
30	. 37		93.9	1.3	TRACE	11.5	-
37 38	38		93.5	0.8	2.8	11.1	·920*
38	39 40		90.8	1.5	13.1	6.8	.878
39	41		88.4		18.0	7.5	.886
40	42		93.0 93.9	0.4	9.2	11.5	.853 .920*
			73.7	0.1	1.0		• 720*
42	43		95.5	0.2	3.6	6.9	.920*
43	445		95.6	0.7	TRACE	8.9	-
15	46		9T-8	1.3	1.7	9.2	.920*
74 77 77	47		95.5 88.7	1.5	18.8	6.9	.879
1.7	48					0.0	
47 48	49	•	86.7 88.6	2.5	19.1	9.0	.879
49	50		87.9	2.2	19.2	7.0	.884
50 51	51		89.5	0.9	17.1	8.3	.880
51	52		88.6	2.0	16.0	8.5	.873
52	53		87.7	1.8	17.5	9.9	.882
53	54		91.7	1.4	4.5	12.5'	.920*
52 53 54 55-	53 54 55 56		91.7 93.9 82.4	0.7	17.5 4.5 5.4 29.6	9.9 12.5 8.1 7.5	.920* .920* .895
55-			82.4		29.6	7.5	.895
56	57		80.5	4.1.	32.2	8.3	.890

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Oll-SHALP ASSAYS BY MUDITIED FISCHER RETORT METHOD

Bemples from the U.S. Geological Survey's Corehole

78-10 (Continued)

				Yield o	of procu	c:			
			Weight percent				r ton	Specific gravity	
Prov	Tr	011	Water	Spent	Gas +	013	Water	of oil at 60°/60° F	
57 58 59 60 61	58 59 60 61 62			82.5 87.2 88.1 84.6 85.1	3.4 2.5 2.3 3.2 3.0	26.6 17.8 18.1 24.4 23.1	10.0 8.9 6.8 7.2 7.8	.899 .887 .891 .910	
62 63 64 65 66 67	63 64 65 66 67 68			86.2 85.7 Sample 89.2 91.0 91.9	2.7 2.5 not re 2.2 1.9	23.5 22.6 ceived 17.2 11.6 11.8	5.8 8.2 5.5 6.7 5.5	.896 .893 .888 .877 .891	
68 69 85 86 87	69 70 86 87 88			94.8 95.7 82.6 87.0 88.7	1.2 0.6 2.9 1.7	2.9 2.1 30.7 21.5 17.3	7.0 7.0 7.1 7.9 7.5	.920 * .920 * .901 .889	
88 89 90 91 92	89 90 91 92 93			86.4 83.9 88.5 94.9 91.8	1.9 2.9 1.8 1.1	25.3 27.9 16.5 4.6 12.3	5.3 6.7 8.6 5.3	.900 .895 .893 .920 *	
93 94 95 96 97	94 95 96 97 98			96.1 94.3 96.1 96.7 95.0	0.5	3.0 7.4 3.7 1.6 5.1	5.4 5.0 5.1 5.6	.920 * .887 .920 * .920 *	
98 99 100 101 102	99 100 101 102 103			95.9 95.6 95.2 95.6 94.8	0.6 0.4 0.6 0.3	3.8 4.4 4.0 4.4 4.9	4.9 5.5 6.5 5.7 5.7	.920 * .920 * .920 * .920 *	
103 104 105 106 107	104 105 106 107 108			95.0 95.2 94.2 94.1 95.2	0.55	5.3 4.3 6.5 7.5 6.0	6.2 6.5 6.1 5.2 4.7	.897 .920 * .879 .862 .857	

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OIL-SHALP ASSAYS BY MODIFIED FISCHER RETORT METHOD Semples from the U.S. Geological Survey's Corehole 78-10 (Continued)

			Yzeld	ol procu	51		65-116	
		Weign	t percent		The second second	er ton	Specific	
From	epth To	Oil Wate	Spent shale	Cas +	Oil	Water.	of oil at 60°/60° F	
108 109 110 111 112	109 110 111 112 -113		91.5 90.5 91.1 93.8 93.2	1.3 1.1 1.8 1.0	18.8 20.8 14.3 9.7 8.1	1.1 0.8 4.6 3.4 6.7	.871 .920 * .865 .920 *	
113 114 115 116 117	114 -115 -116 117 118		94.5 95.3 92.4 92.9 91.7	1.0 0.7 1.7 1.0	4.8 3.5 10.6 9.4 11.2	6.5 6.2 4.9 6.5 7.1	.920 * .920 * .868 .867 .885	
118 119 120 121 122	119 120 121 122 ·123		92.2 92.8 93.3 90.7 89.1	0.7 1.0 0.6 0.9	11.4 8.3 7.2 14.9 18.6	6.7 7.5 8.3 6.9 6.8	.888 .886 .869 .894	
123 124 125 126 127	124 125 126 127 128		88.2 88.9 87.4 89.5 89.6	1.0 1.1 2.1 1.7	20.5 18.6 20.2 15.3 13.2	7.4 7.1 6.7 6.9 9.1	.901 .904 .921 .924	
128 129 130 131 132	129 130 131 132 133		88.4 88.1 92.7 90.4 91.8	1.5 1.9 1.0 1.3	20.4 20.4 8.1 13.2 13.9	5.7 4.9 7.9 7.9	.910 .924 .900 .918	
133 134 135 136 137	134 135 136 137 138		92.8 90.9 90.3 88.7 90.6	1.2 1.2 1.5 1.3	8.2 12.5 15.8 18.4 12.1	7.3 7.5 5.8 8.1 9.4	.874 .902 .882 .862 .865	
138 139 140 141- 142	139 140 141 142 143		93.1 91.2 87.6 89.0 90.2	0.7 1.2 1.7 1.7	7.2 7.4 15.7 14.9	8.6 11.7 11.8 9.2 11.1	.866 .859 .889 .887	

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OIL-SHALF ASSAYS BY MODIFIED FISCHER RETORT METHOD

Samples from the U.S. Geological Survey's Corehole

78-10 (Continued)

Benches from the S.C. Carlogical Survey's Crystall-

		-	Yield of product							
		Weight			or proc:		or tor.	Specific		
Prov	pth To	0:1		Spent	Gas +	1000		pravity of oil at		
		0.1	Water	shale	loss	Oil	Water.	60°/60° F		
143 144 145 146 147	144 145 146 147 148			89.6 91.0 90.5 91.3 92.3	1.7 1.8 1.3 1.0	14.7 10.1 8.9 7.6 6.4	8.0 8.3 11.8 11.9 9.9	.882 .881 .861 .875 .888		
148 149 150 151 152	149 150 151 152 153			91.8 90.8 89.3 91.0 92.5	1.6 1.9 1.1 1.1	7.0 8.0 15.8 12.4 8.0	9.5 10.4 8.4 7.7 8.5	.878 .886 .909 .907 .885		
153 154 155 156 157	154 155 156 157 158			94.5 92.5 92.0 88.9 91.0	0.6 0.9 1.0 1.6	7.0 2.8 7.1 13.6 11.7	5.5 13.3 10.8 11.0 8.0	.880 .920 * .864 .865 .884		
158 159 160 161 162	159 160 161 162 163			95.5 93.8 91.7 90.9 93.2	0.8 1.1 1.3 1.6 1.2	4.1 6.3 11.7 11.7 7.5	5.2 6.9 6.4 7.7 6.8	.920 * .866 .878 .880 .881		
163 164 165 166 167	164 165 166 167 168			92.4 94.3 92.8 90.0 92.1	1.0 0.8 1.4 1.4	7.7 5.5 6.5 10.7 8.9	9.2 6.7 8.4 11.2 8.7	.883 .920 * .858 .864 .892		
168 169 170 171 172	169 170 171 172 173			93.3 94.6 93.1 92.2 90.5	1.0 1.5 1.2 1.1	4.7 2.6 4.5 9.3 8.7	9.8 7.0 9.7 7.9 11.3	.857 .920 * .920 * .863 .868		
173 174 175 176 177	174 175 176 177 178			90.6 91.4 95.1 95.2 94.0	1.4 0.3 1.0 0.8 1.0	7.1 7.6 5.6 4.1 4.5	13.2 13.3 4.0 5.9 8.0	.851 .856 .920 * .920 *		

NAMED AND POST OFFICE ASSESSMENT OF PARTY ASSESSMENT

Charleson of an enter fangacion of the six south and post

WINDSHOOT MANNER BY PROPERTIES VISCHER RETORT NETHOD

Samples from the U.S. Reological Survey's Corehole 78-10 (Continued)

		Section 180	BECOME TO	Yield c	of procu	161		
Don	Depth		Weigns	percent		Cas) p	Specific gravity	
2707	70	011	Water	Speni	Loss	013	Water	of oil at
178 179 180 181 182	179 180 181 182 183	011	Water	93.1 89.8 90.1 93.6 94.0	1.0 1.4 1.4 1.1	7.0 13.4 15.6 3.5 2.3	8.1 9.2 6.7 9.5 9.2	.876 .886 .882 .920 *
183 184 185 186 187	184 185 186 187 188			93.0 93.3 92.2 93.3 89.9	1.2 0.7 1.1 1.0 1.8	3.0 2.9 6.7 5.6 9.8	11.1 11.8 10.3 8.8 11.4	.920 * .920 * .882 .868 .875
188 189 190 191 192	189 190 191 192 193			91.3 96.7 94.5 93.7 90.7	1.5 Ø.1 Ø.1 0.2 1.2	9.5 2.6 4.8 8.8 13.3	8.8 6.7 8.8 7.2 7.7	.887 .920 * .920 * .864 .876
193 194 195 196 197	194 195 196 197 198			89.9 94.9 92.2 91.9 90.4	1.5 0.9 1.3 1.0 2.5	13.8 5.5 4.8 6.3 5.3	8.3 5.3 11.1 11.5 12.3	.883 .877 .920 * .864 .888
198 199 200 201 202	199 200 201 202 203			92.2 84.8 93.0 92.4 93.9	1.3 2.4 1.5 1.1	7.8 19.9 7.5 5.2 3.2	8.6 13.2 6.5 11.0 8.9	.879 .876 .897 .885
203 204 205 206 207	204 205 206 207 208			96.4 92.1 93.5 92.6 93.9	0.8 1.8 1.4 1.4	2.8 7.8 6.1 7.0 4.2	3.9 7.6 6.9 8.1 8.3	.920 * .899 .881 .920 *
208 - 209 210 211 212 213	209 210 211 212 213 214			94.2 92.6 95.0 94.2 95.2 91.6	1.2 2.0 1.4 1.9 1.6	2.4 3.6 4.3 3.3 3.2	8.9 9.5 4.5 6.3 4.8	.920 * .920 * .920 * .920 * .920 *

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OLL-SHALE ASSAYS BY MODIFIED FISCHER RETORT MITHOD

Samples from the U.S. Geological Survey's Corehole 78-10 (Continued)

			/8-10	(Contin	insq)		
			Yield	of proc	uct		
Depth		Weignit	percent		The second second second	er ton	Specific
From To	011	Water	Spent shale	Cas +	011	Water	gravity of oil at 60°/60° F
							. 00 \u0010- E
214-215 215-216 216-217 217-218 218-219				.3 .5 .8 .8	2.1 1.6 6.0 8.2 8.3	9.0 6.9 7.2 6.9 5.8	.910 .910 .910 .921
219-220 220-221 221-222 222-223 223-224				1.3 .9 .6 .7	8.8 9.6 10.0 9.2 9.1	9.5 7.1 7.5 10.7 10.2	.925 .922 .900 .869
224-225 225-226 226-227 227-228 228-229				1.8 1.5 .3 .9	7.5 15.1 6.6 9.8 10.1	5.7 8.9 6.9 11.4 6.2	.910 .902 .890 .888 .890
229-230 230-231 231-232 232-233 233-234				1.4 1.9 1.7 2.3 1.8	10.5 13.1 10.9 13.7 11.4	9.5 10.4 9.0 8.4 6.0	.908 .930 .912 .899
234-235 235-236 236-237 237-238 238-239				2.1 1.7 1.6 2.0 1.7	13.0 10.4 9.9 14.9 13.3	8.6 5.5 5.4 7.8 7.1	.900 .893 .896 .887
239-240 240-241 241-242 242-243 243-244				1.2 .8 .0 .0	5.5 2.7 3.6 4.6 3.4	9.7 7.9 6.4 7.1 7.2	.910 .910 .910 .910

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OLL-SHALE ASSAYS BY MODIFIED FISCHER RETORT MITHOD Samples from the U.S. Geological Survey's Corehole

78-10 (Continued)

	-	Yield of product												
		Weignt	percent	or brode	Gul pe		Specific							
Depth			Spent	Cas 4	Od. Pi	ET EON	gravity							
From To	0	11 Water	shale	loss	011	Water.	of oil at 60°/60° F							
244-245				1.4	2.0	8.3	.910							
245-246 246-247				1.2	1.9	9.3	.910							
247-248				1.1	2.5	10.0	.910							
248-249				.9	7.4	9.5	.910							
249-250				1.2	8.0	6.5	.910							
250-251 251-252	*			.7	0.0	7.9	***********							
252-253				.8	1.8	8.3	.910							
253-254				.6	4.3	5.8	.910 .910							
254-255				.0	1.5	6.2	.910							
255-256				.3	0.2	4.9	.910							
256-257 257-258				.5	3.9	3.8	.910							
258-259				1.0	0.8	6.2	.910 .910							
259-260				.1	0.1	5.4	.910							
260-261				.2	0.3	5.1	.910							
261-262 262-263				.5	1.0	8.0	.910							
263-264				.0	0.2	8.5	.910							
2000223					1.1	6.0	.910							
264-265 265-266				1.9	1.4	7.6	.910							
266-267				.0	0.1	7.0	.910							
267-268				.5	0.2	6.0 5.8	.910							
268-269				1.9	0.1	8.0	.910							
269-270				.9	0.2	7.2	.910							
270-271				. 9	1.9	8.6	.910							
271-272 272-273				.1	0.0	7.8								
273-274				.1	0.0	2.9								
				. 3	0.0	4.0								

NAME OF TAXABLE PARTY OF THE OWNER, NAME OF TAXABLE PARTY OF TAXABLE PARTY.

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OIL-SHALE ASSAYS BY MODIFIED FISCHER RETORT MITHOD Samples from the U.S. Geological Survey's Corehole 78-10 (Continued)

Danes		Weight	percent	of prod	The second second second	per ton	Specific
Pepth From To	011	Water	Spent	Gas + loss	011	Water.	of oil at 60°/60° F
274-275 275-276 276-277 277-278 279-280				1.0 1.2 .3 1.0 2.6	0.0 0.0 1.1 0.5 0.5	4.3 5.1 2.4 3.5 4.2	.910
280-281 281-282 282-283 283-284 284-285				3.1 3.2 1.1 0.0	0.4 0.1 1.5 1.6 2.1	4.8 5.5 3.6 4.3 4.0	.910 .910 .910 .910
285-286 286-287 287-288 288-289 289-290				.3 .7 .7 2.1 1.1	0.0 0.1 .1 .2	6.1 5.7 5.7 7.2 8.1	.910 .910 .910 .910
290-291 291-292 292-293 293-294 294-295				1.0 1.4 0.0 0.0	.5 6.6 .1 .1	10.5 1.6 8.8 7.9 1.6	.910 .910 .910 .910
295-296 296-297				1.0	.1	1.1	.910 .910

*Assumed specific gravity

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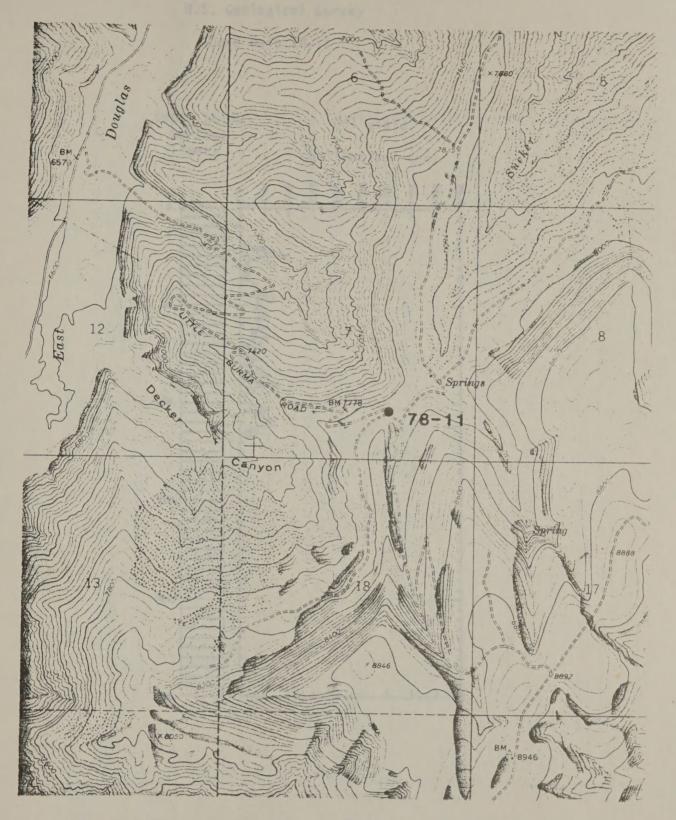


Figure 13.--Map showing location of core hole 78-11. Base from Brushy Point Quadrangle (1964). Scale 1:24,000.

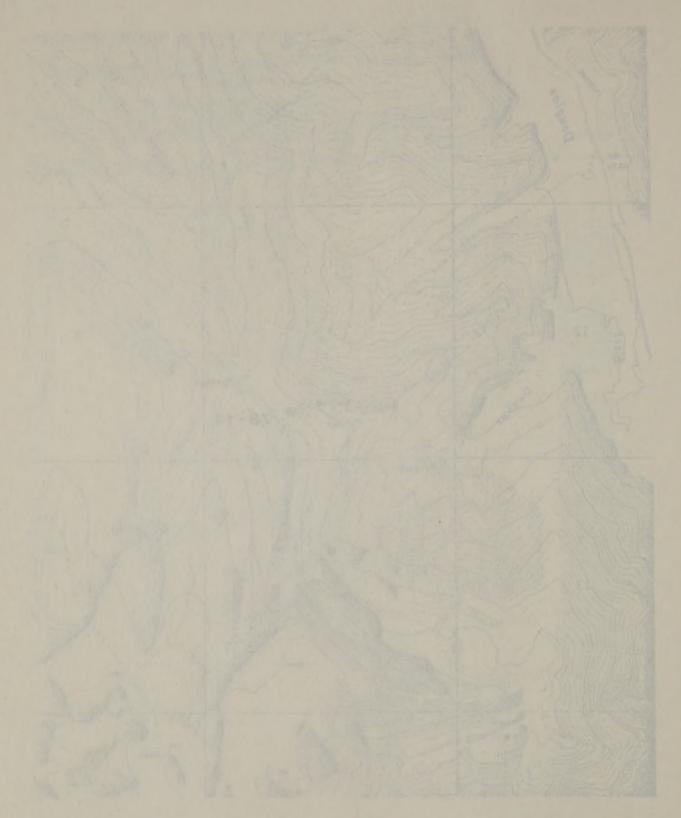
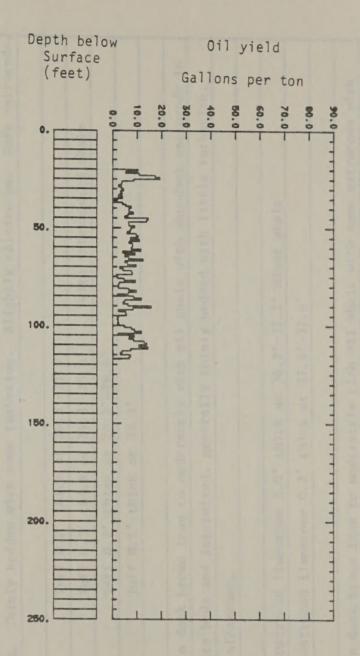


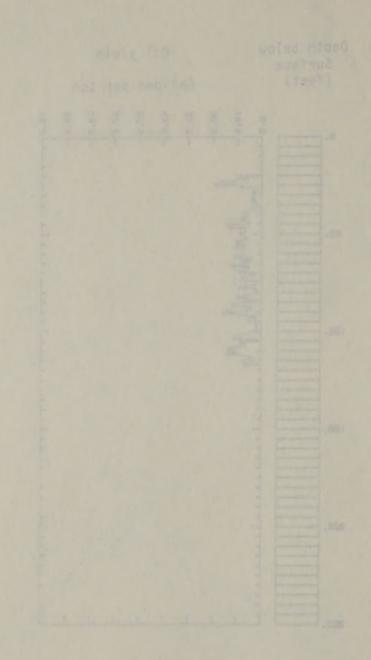
Figure 13. -- Map shinking location of core hole 70-15. Hade From Sci. of tornic Quadrangle (1964). Scale 1924. NOU

U.S. Geological Survey

Core hole 78-11



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FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION
20.0'	35.9'		Dark-brown to gray very lean oil shale, abundant clay, shrinks and cracks on
			drying. Thinly bedded with some turbation. Slightly calcareous. Rare ostrocods.
			Tuff 0.2' thick at 20.8'-21.0'
			Tuff 0.3' thick at 25.3'-25.6' with interbedded shale
			Tuff 0.2' thick at 28.2'-28.4'
			Tuff 0.1' thick at 33.3'
			A Delication of the Control of the C
35.9'	45.1'		Gray to dark brown lean to moderately rich oil shale with abundant ostrocods in
			descrete beds and intermixed, generally thinly bedded with little turbation.
			Very calcareous.
			Ostrocod limestone 1.0' thick at 36.2'-37.2' minor shale
			Ostrocod limestone 0.2' thick at 37.4'-37.6'
			Delinates operated that the late of the la
45.1'	101.5'		Gray to dark brown lean to moderately rich oil shale with some ostrocods with
			Impure or dolomitic limestone beds, thinly bedded with little turbation.
			Slickensides common. Generally calcareous. Stromatolites and conglomeritic
			textures common in dolomites.
			Dolomite (?) 0.4' thick at 46.1'-46.5' with minor shale ostrocods
			Dolomite (?) 0.2' thick at 46.8'-47.0' with minor shale ostrocods
			Deliver of the second of the s

Constitute 19-15

Lagged by Kure Hollocher

FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION
			Dolomite 0.3' thick at 82.5'-82.8'
			Dolomite oolites (pisoliths?) and ostrocods with calcite
			cement 0.4' thick at 86.3'-86.7'
			Dolomite 0.2' thick at 90.9'-91.1'
1416			Dolomite 0.2' thick at 91.2'-91.4' with minor shale
			Dolomite 0.1' thick at 94.0'
			Dolomite w/Stromatolites 0.3' thick at 97.0'-97.3' with minor shale
			Dolomite 0.15' thick at 97.5'-97.65' with minor shale
			Dolomite w/Stromatolites (?) 0.4' thick at 100.6'-101.0' with minor shale
			Dolomite w/Stromatolites 0.1' thick at 101.2' with minor shale
01.5'	117.4'		Similar to preceeding interval 45.1' to 101.5', but oil shale is dark gray and
			brown to nearly black and rich. Smells of H ₂ S as well as oil. Calcareous.
			Dolomite, stromatolites 0.4' thick at 101.7'-101.1' with minor shale
			Dolomite, stromatolites 0.1' thick at 103.6' with minor shale
			Dolomite, stromatolites 0.4' thick at 104.0'-104.4' auto conglomerate
			Dolomite, stromatolites (?) 0.1' thick at 104.8' auto conglomerate
			Dolomite 0.2' thick at 107.0'-107.2'
			Dolomite 0.2' thick at 109.7'-109.9'

Coretole 18-11 (Conttoued)

FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION
117.4'	153.0'		Gray calcareous claystone, mudstone, and dirty sandstone irregularly inter-
			bedded to massive. Some of the mudstones are fossiliferous and parts of the
			sandstones show crossbedding and brown oil staining.
153.0'	193.3'		Sandstone, moderately well sorted with calcite cement, medium grain size with
13313			thick indistinct bedding. Largely water saturated with dark brown oil staining.
			Thickly interbedded with calcareous claystone and mudstone some beds are oozing
			a brown thick oil
			Below about 170' the drilling water has been producing droplets of brown oil
			and smells strongly of oil
			Sandstone, largely oil saturated 9.4' thick at 153.0'-162.4'
			Sandstone, largely oil saturated 2.2' thick at 169.8'-172.0'
			Sandstone, largely oil saturated 17.5' thick at 173.3'-190.8'
193.3'	201 61		Thinly bedded to massive gray mudstone and claystone with minor sand.
	of hole		Calcareous with a fossiliferous unit at 201.1'-201.4', 0.3' thick.
DOLLOW	or note		
			Bottom of Hole

Cocepule 18-15 (Continued

FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION
			The dolomites were distinguished on the basis of texture and reaction to
			dilute HCl in comparison to pure calcite. Such beds occurred in shales which
			were both calcitic and noncalcitic. The texture of some tuffs or lean marlstone
			may well be the same as some dolomite and may be confused. Slickenside attitude
			varied widely but were mainly between about 10° and 50° from the horizontal
			with striations oriented down dip.
			CARL CAR
		4 00 00	

Colepsie 18-17 (Courrence)

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Samples from the U.S. Geological Survey's Corchole 78-11 drilled in sec. 7, T. 4 S., R. 100 W., Rio Blanco County, Colorado

			Yield c	i prod	wet		
Depth		Weight	percent	11100			Specific
			Spent	Gas +	THE RESERVE	er ton	gravity
Eron To	Oi1	Water	shale	loss	013-1/	Water	of nil at
20 0 21 2			9111			Marei	60°/60° F
20.0-21.0	3.9	4.7	89.6	1.8	10.4	11.3	0.905
21.0-22.0	2.0	7.0	89.3	1.7	5.3	16.8	.905
22.0-23.0	4.1	7.0	86.4	2.5	10.9	16.8	.910
23.0-24.0	6.6	5.7	85.0	2.7	17.3	13.7	.923
24.0-25.0	7.2	5.5	84.3	3.0	19.2	13.2	
25.0-26.0	3.2	3.4	91.3	2.1	8.5	8.1	.906
26.0-27.0	1.4	4.0	93.2	1.4	3.7a	9.6	.907
27.0-28.0	1.4	4.2	93.3	1.1	3.6a		
28.0-29.0	.9	3.0	95.0	1.1	2.3a	10.1	
29.0-30.0	1.4	3.0	94.4	1.2	3.6a	7.2	
30.0-31.0	1.7	3.1	94.2	1.0		7.2	
31.0-32.0	1.2	3.9	93.8	1.1	4.42	7.4	
32.0-33.0	1.5	4.5	92.8	1.2	3.2a	9.3	
33.0-34.0	.8	4.0	94.3		3.8a	10.8	
34.0-35.0	1.5	4.6	92.4	. 9	2.2a	9.6	
35.0-36.0	.7	3.5	94.3	1.5	4.0a	11.0	
36.0-37.0	. 2	1.5	97.8	1.5	1.9a	8.4	
37.0-38.0	1.5	2.9		. 5	.6a	3.6	
38.0-39.0	2.0		94.8	. 8	4.0a	7.0	
39.0-40.0		3.5	93.4	1.1	5.4	8.4	.873
40.0-41.0	2.8	3.0	93.0	1.2	7.6	7.2	.872
41.0-42.0	2.4	3.7	92.2	1.7	6.6	8.9	. 884
42.0-43.0	2.5	4.5	91.5	1.5	6.7	10.8	. 886
	3.1	4.1	91.4	1.4	8.4	9.8	. 889
43.0-44.0	2.3	3.8	92.7	1.2	6.2	9.1	.883
44.0-45.0	1.9	4.5	92.0	1.6	5. Na	10.8	
45.0-46.0	5.5	6.0	86.5	2.0	14.5	14.4	.905
46.0-47.0	5.2	2.9	90.0	1.9	13.8	7.0	.911
47.0-48.0	2.4	4.0	92.4	1.2	6.4	9.6	.903
48.0-49.0	2.5	3.1	93.3	1.1	6.6	7.4	.900
49.0-50.0	3.2	3.1	92.4	1.2	8.9	7.4	. 878
50.0-51.0		2.3		1.2	7.4	5.5	0.867
51.0-52.0	2.6	4.6	91.5	1.3	7.1	11.0	.868
52.0-53.0	2.1	4.0	92.5	1.4	5.9	9.6	. 865
53.0-54.0	3.5	4.4	90.7	1.4	9.6	10.5	.881
54.0-55.0	3.9	3.5	91.3	1.3	10.4	8.4	.888
55.0-56.0	2.6	3.8	92.3	1.3	7.3	9.1	.862
56.0-57.0	4.0	4.0	89.7	2.3	10.9	9.6	. 872
57.0-58.0	2.4	2.7	94.0	. 9	6.6	6.5	.879
58.0-59.0	2.9	6.0	89.3	1.8	8.0	14.4	. 883
59.0-60.0	3.0	4.0	91.7	1.3	8.1	9.6	.885
60.0-61.0	2.8	4.0	92.1	1.1	7.5	9.6	.887
61.0-62.0	4.4	3.3	91.0	1.3	11.5	7.9	.914
62.0-63.0	1.6	3.9	93.2	1.3	4.1a	9.3	1000
63.0-64.0	3.3	5.0	90.3	1.4	9.1	12.0	. 870
64.0-65.0	1.9	2.6	94.6	.9	4.98	6.2	

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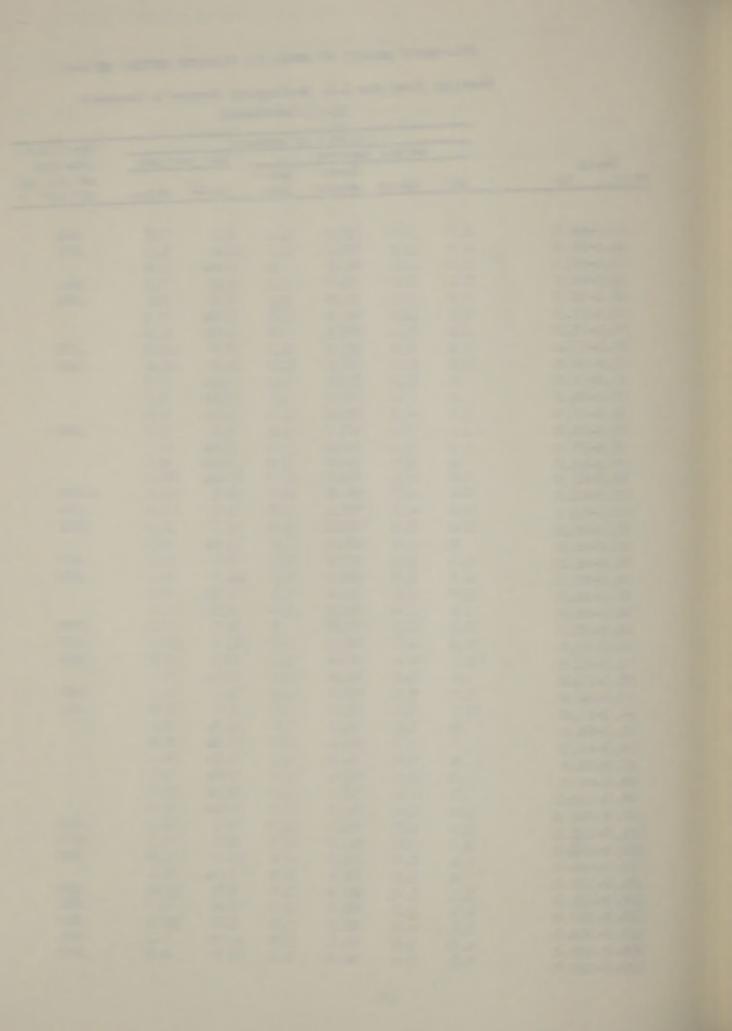
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OIL-SHALE ASSAYS BY MODIFIED FISCHER RETORT MITHOD

Samples from the U.S. Geological Survey's Corehole 78-11 (Continued)

	-	*	Yield		1060)		
		Weight	percent	of proc			Specific
Depth			Spent	Gas 4		er ton	gravity
From To	011	Water	shale	loss	011-	Water.	of oil at
						MALEL.	60°/60° F
65.0-66.0	2.3	2.9	93.6	1.2	6.5	7.0	.866
66.0-67.0	4.5	2.3	92.1	1.1	12.4	5.5	.871
67.0-68.0	1.9	2.4	94.9	.8	4.9a	5.8	.071
68.0-69.0	2.2	2.9	93.7	1.2	6.0	7.0	.864
69.0-70.0	3.5	3.5	91.9	1.1	9.5	8.4	.885
70.0-71.0	1.1	3.0	94.9	1.0	2.9a	7.2	
71.0-72.0	1.6	2.4	95.2	. 8	4.2a	5.8	
72.0-73.0	2.8	4.5	91.5	1.2	7.7	10.8	.873
73.0-74.0	2.9	4.5	90.6	2.0	8.0	10.8	.868
74.0-75.0	.6	2.2	96.6	.6	1.5a	5.3	
75.0-76.0	.8	2.6	95.9	. 7	2.0a	6.2	
76.0-77.0	1.7	4.0	93.0	1.3	4.6a	9.6	
77.0-78.0	3.4	2.1	93.5	1.0	9.2	5.0	.884
78.0-79.0	1.0	3.4	94.6	1.0	2.6a	8.1	
79.0-80.0	. 8	3.5	94.7	1.0	2.2a	8.4	
80.0-81.0	0.9	4.5	93.3	1.3	2.4a	10.8	
81.0-82.0	2.4	4.5	91.8	1.3	6.5	10.8	0.865
82.0-83.0	3.6	4.5	90.1	1.8	9.6	10.8	. 894
83.0-84.0	2.4	3.5	92.3	1.8	6.3	8.4	.902
84.0-85.0	.8	2.8	95.6	.8	2.0a	6.7	0.70
85.0-86.0	3.1	3.6	91.8	1.5	8.6	8.6	.879
86.0-87.0	4.3	3.8	90.4	1.5	11.7	9.1	.883
87.0-88.0	1.9	2.7	94.4	1.0	4.9a	6.5	
88.0-89.0	1.6	3.6	93.3	1.5	4.2a	8.6	0.70
89.0-90.0	2.2	3.0	93.9	.9	6.1	7.2	.878
90.0-91.0	5.8	4.2	88.3	1.7	15.7	10.1	.877
51.0-92.0	3.1	4.4	91.4	1.1	8.3	10.5	. 884
92.0-93.0	2.0	3.1	94.6	1.4	2.3a	7.4	006
93.0-94.0		3.5	93.0	1.5	5.3	8.4	.886
94.0-95.0	2.1	3.7	94.5	1.7	5.6 2.3a	8.9	. 891
95.0-96.0	.9	3.7	94.4		1.8a		
96.0-97.0	.9	3.8	94.2		2.2a	9.1	
97.0-98.0	.8	2.4	95.4		2.0a		
98.0-99.0	.9	4.4	93.1		2.5a		
99.0-100.0	1.8	2.4	94.5	1.3	4.8a		
100.0-101.0	2.9	1.7	94.1	1.3	7.6	4.1	.910
101.0-102.0	3.3	3.9	91.3	1.5	8.9	9.3	.877
102.0-103.0	4.4	2.0	92.0		11.7	4.8	. 895
103.0-104.0	.8	3.8	93.4	2.0	2.1a	9.1	
104.0-105.0	3.2	5.0	89.9	1.9	8.8	12.0	.886
105.0-106.0	2.4	3.2	92.7	1.7	6.6	7.7	.880
106.0-107.0	3.2	4.2	90.7	1.9	8.5	10.1	.905
107.0-108.0	4.8	3.0	90.2	2.0	12.8	7.2	.904
108.0-109.0	. 5.2	3.6	89.0	2.2	13.9	8.6	.902
109.0-110.0					*		



OLL-SHALE ASSAYS BY MODIFIED FISCHER RETORT MITHOD Samples from the U.S. Geological Survey's Corehole 78-11 (Continued)

			Yzeld	of prop	uc:		
Depth		Weight	percent			er ton	Specific
Ртоп То	011	Water	Spent	loss	Qi3-1/		of oil at
110.0-111.0	4.0	3.4	90.8	1.8	10.7	8.1	0.896
111.0-112.0	5.3	2.9	90.1	1.7	14.4	7.0	.882
112.0-113.0	2.7	3.8	91.9	1.6	7.3	9.1	.877
113.0-114.0	1.4	3.5	93.9	1.2	3.7a	8.4	
114.0-115.0	1.2	3.7	93.9	1.2	3.1a	8.9	
115.0-116.0	2.7	3.8	92.0	1.5	7.2	9.1	. 893
116.0-117.0	2.4	3.8	92.3	1.5	6.7	9.1	.876
195.0-196.0	.0	2.9	96.1	1.0	Trace	7.0	
196.0-197.0	.0	3.4	94.8	1.8	No oil	8.1	
197.0-198.0	.0	3.4	95.1	1.5	No oil	8.2	
198.0-199.0	.0	2.7	96.4	.9	No oil	6.5	
199.0-200.0	.0	2.3	95.7	2.0	No oil	5.5	
200.0-201.0	.0	3.5	95.5	1.0	Trace	8.4	

^{1/ &}quot;a"--indicates specific gravity estimated as 0.92.

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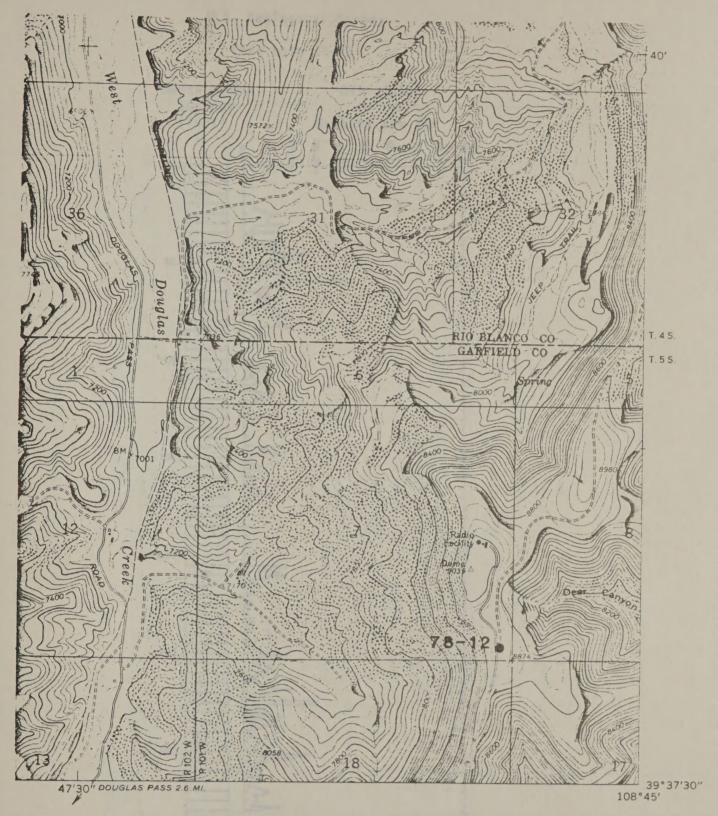


Figure 14.--Map showing location of core hole 78-12. Base from Big Foundation Creek Quadrangle (1964). Scale 1:24,000.

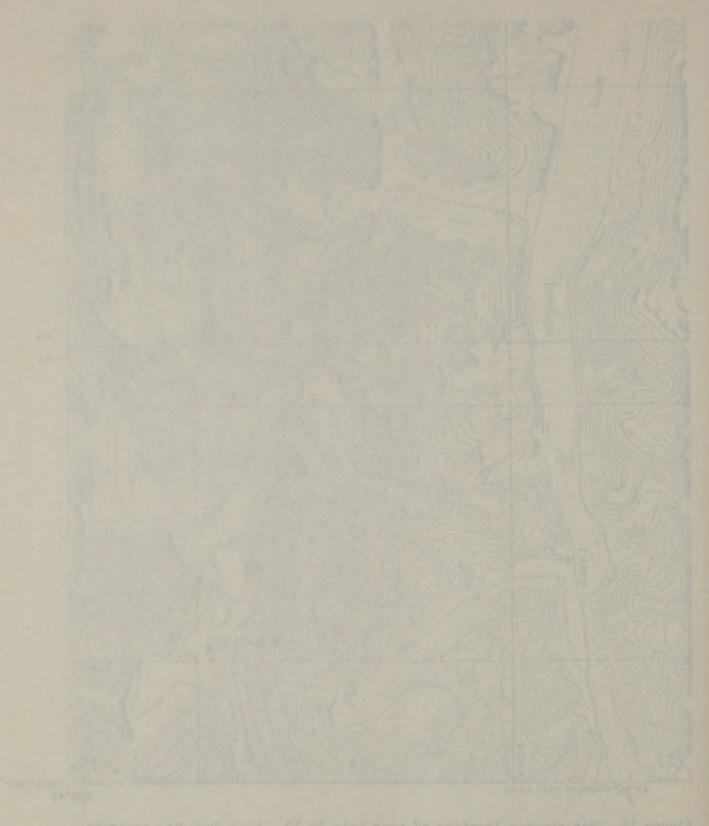
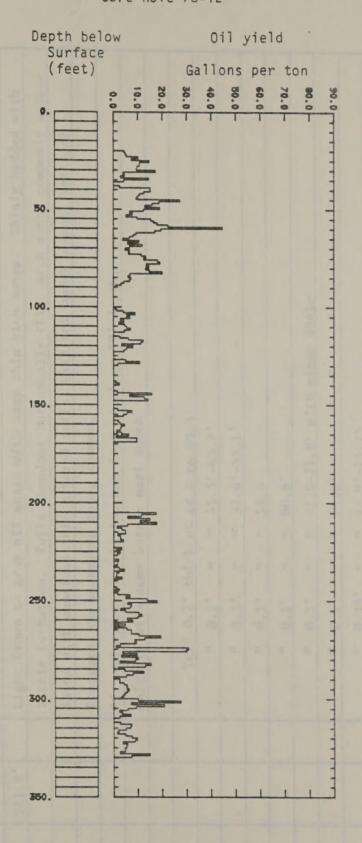


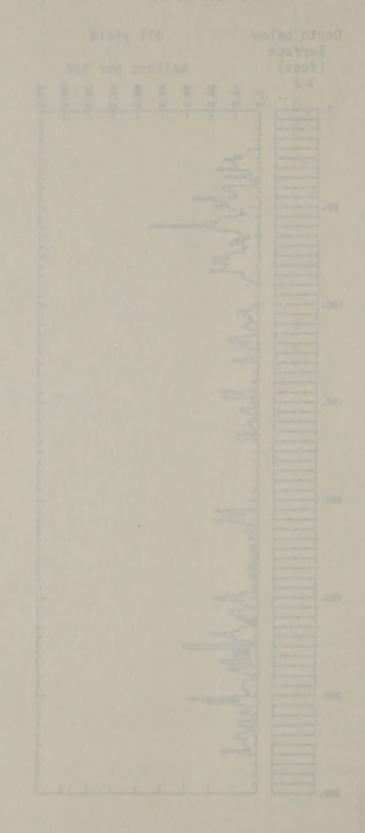
Figure 14.--Map situating location of core hale 78-12. (a.e. from 81g Foundation Creek Quadrangle (1964), Scale 1:24,000;

U.S. Geological Survey

Core hole 78-12



U.S. Tantopical Lawrey



Corehole 73-12
Logged by Kurt Hollocher

FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION
20'	111.8'		Light brown to gray oil shale with many thin rich zones. Thinly bedded with
			little turbation. Tuffs abundant but usually thin. Rich zones commonly assoc-
			iated with numerous thin altered tuffs. Oxidized zones common. Vertical
			fractures on broken-up zones common.
			Air and water circulation was lost at about 50' depth.
			Calcitic with some barren marl zones
			Tuff 0.2' thick at 44.4 to 45.3'
			" 0.2' " 45.5'-45.7'
			" 0.5' " " 52.6'-53.1'
			" 0.1' " 58.0
			" 0.1' " " 60.6'
			" 0.2' " " 71,6-71.8' with minor shale
			" 0.1' " " 74.6' " " "
			" 0.35' " 74.9'-75.25'
			0.3' " " 75.8'-76.1' " " "
			0.2' " 78.4'-78.6' " " "
			" 1.1' " " 81.3'-82.8' " " " "
			" 0.1' " " 90.4' Oxidized
			" 1.4' " " 91.4'-92.8' Oxidized
			" 0,2' " "105,2'-105,4'0xidized
			" 0.25' " "106.05'-106.3 Oxidized
		CO CO COMPANY	" 0.15' " "107.95'-107.1'

Logged by Eust Halloche

FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION
111,8'	205.1'		Brown to gray lean oil shale, thinly bedded with little turbation. Thin tuffs
			very abundant with many thicker tuffs (some siltstone?). Many of the thicker
			tuffs are oxidized. Some layers are grayish green. Not calcareous.
			They have been and the body which came an extended which have the body and the body
			Maly he had also there a mention, religible, Stiller
			Tuff 0.4' thick at 113.0'-113.4' with minor shale
			" 1.5' " "113.9'-115.4' " " "
			0.2' " 117.6'-117.8'
			0.41 " 120.91-121.31 " "
			0.3' " 122.4'-122.7' " " "
			Siltstone 4.3' " "122.7'-127.0' " " "
			Tuff 0.2' " 128.0-128.2' " " "
			Siltstone 3.9' " "131.6'-134.5'
			" 4.2' " "135,7'-139,9' " " "
			Tuff 0.1' " 144.6'
			" 0.4' " "145.0'-145.3'
			Siltstone 4.6' " "146.9-151.5' " " "
			Ostracods 0.05' thick at 151.85'
			Siltstone 3.8' thick at 154.6'-158.4' with minor shale
	1		

FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION
			Siltstone 0.2' thick at 171.2'-171.4'
			" 33.4' thick at 171.7'-205.1' Iron stained
Siltstone 0.2' thick at 171.2'-171.4'			
			Thinly bedded with little turbation, calcitic. Silty
			Bilding and account and distanced oughling 271,80-271,80, 2.80 (bill)
			The state of the s
			Tuff 0.1' thick at 214.0' Turbated
			Intraformational conglomerate 0.1' thick at 218.6'
			Fine sandstone 0.1' thick at 219.7' Turbated
			Fine sandstone 0,2' thick at 219,9'-220,1'
			Siltstone with minor shale 220,2'-223,2', 3.0' thick
			Tuff 0.3' thick at 224,6'-224.9' Turbated
			Tuff 0.2' thick at 231.2'-231.4'
			Siltstone 4.3' thick at 238.9'-243.2' with minor shale
246.9'	330.0'		Gray to brown and dark brown oil shale with common tuff and some silt and
			siltstone, less common than above unit. Some parts calcareous
			Intraformational conglomerate 0.4' thick at 248.6'-249.0;
			Tuff 0.4' thick at 249.3'-249.7' Highly contorted
			Tuff 0.7' thick at 254.5'-25.2' Highly enterted Silty

FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION
			Tuff 0.5' thick at 261.3'-261.8' Highly contorted
			" 0.4' " 262.8'-263.2' Highly contorted
			" 0.15' " " 269.4'-269.55' Highly contorted
			" 0.1' " "269.8' Highly contorted
			Ostracods 0.05' " 270.3' (some ostracods below this bed)
			Highly tuffaceous and disturbed section 271.8'-273.8', 2.0' thick
			Tuff 0.1' thick at 278.3'
			Highly tuffaceous and disturbed section, 280.5'-282.2', 1.7' thick
			Tuff 0.1' thick at 286.6'
			Tuff 0.8' thick at 300.0'-300.8' Highly contorted
			" 0.3' thick at 301.85'-302.15' Highly contorted
			Intraformational conglomerate with ostracods, 302.3'-302.6'
			0.3' thick
			Tuff 0.2' thick at 306.8'-307.0' (Dolomite)
			" 0.2' thick at 308.1'-308.3'
			Ostracod dolomite 0.4' thick at 310.3'-310.7'
			" 0.6' thick at 310.9'-311.5'
			" 0.7' thick at 312.6'-313.3' (contorted) (tuffaceous?)
			" 1,3' thick at 314.3'-315.6' "
			" 0,3' thick at 316.2'-316.5' "
			Stromatolites(?) at 318.7'
			Ostracod dolomite 0.3' thick at 319.6'0319.9'
	A CONTRACTOR OF THE PARTY OF TH		" 0.4' thick at 320.6'-321.0' with stromatolites

FROM	то	THICK- NESS	LITHOLOGIC DESCRIPTION
			Ostracod dolomite 0.3' thick at 322.4'-322.7' with stromtolites?
			" 0.1' thick at 323.5' Nodule
			" 0.2' thick at 324.1'-324.3' contorted
			" 0.8' thick at 326.5'-327.3'
			" 0.5' thick at 328.6'-329.1' stromatolites?
			COMMENTS:
			Vertical fractures are relatively common, but slickensides are absent.
			Much of the material labeled as tuff may in fact be dolomitic marl, dolomite,
			or thin sandstone units, as textures and colors are often very similar.
			No thick sections of rich, dark oil shale were seen, although thin units up to
			+0~3' thick are common throughout the section. Oxidized zones are common
			to a depth of about 200'.
	A		to a major
1			

OIL-SHALE ASSAYS BY MODIFIED FISCHER RETORT METHOD

Samples from the U.S. Geological Survey's Corchole78-12 drilled in sec. 7, T. 5 S., R 101 W., Rio Blanco County, Colorado

		-		Yield o	of produ	C1		
Dep	th		METAIL	percent		The second secon	er ton	Specific
From	To	Oil	Water	Spent	loss +			of oil at
				Sugar	TORE	013	Water	60°/60° F
20 21 22 23 24	21 22 23 24 25		•	94.5 95.2 95.6 94.1 95.0	1.4 0.7 0.3 1.0 0.8	4.4 4.9 5.3 10.2 7.4	5.7 5.3 4.7 2.5 3.4	.920 * .920 * .953 .911 .909
25 26 27 28 29	26 27 28 29 · 30			91.4 93.5 93.2 93.1 93.3	1.4 0.7 0.9 1.3	14.7 10.7 10.6 .9.6 9.5	3.7 4.1 4.6 4.7 4.7	.915 .912 .911 .915
30 . 31 . 32 . 33 . 34	31 32 33 34 35			89.9 96.9 96.3 97.1 92.2	1.6 0.1 0.3 0.3 1.1	17.2 3.9 4.5 2.9 14.5	4.7 4.5 4.1 3.6 2.7	.908 .920 * .920 * .920 *
35 36 37 38 39	36 37 38 39 40			96.2 97.2 97.6 96.0 90.4	0.6 0.1 0.5 0.7 1.8	4.2 0.0 0.0 2.5 15.1	3.9 5.8 4.3 5.4 5.0	.920 * .920 * .920 * .920 * .920 *
40 41 42 43 44	41 42 43 44 45			89.6 91.2 94.1 91.5 92.1	1.6 1.5 0.8 1.4 1.2	15.2 12.6 10.7 10.0 9.4	7.3 6.1 2.7 7.8 7.6	.908 .904 .900 .910
45 46 -47 48 49	46 47 48 49 50			86.8 89.2 90.6 92.3 89.9	1.7 1.9 1.5 0.9	27.3 18.7 15.8 13.0	3.2 4.6 4.6 4.5 3.4	.890 .899 .908 .911

DIL-SHALL ASSESSED OF HOUSEVER STREET, MARKET

samples true the H.S. Goological Europy's Carchalange 19-12 delived on

OIL-SHALP ASSAYS BY MODITIED PISCHER RETORT MITHOD

Samples from the U.S. Geological Survey's Corehole
78-12 (Continued)

		-			CODEID			
		-	Weight	Yield c	of proc			Specific
Dep	th		MESKIII	Spent	E. I	Cal p	er ton	gravity
From	То	0:1	Water	shale	loss	Oil	Water	ec./eu. 2
50 51 52 53 54	51 52 53 54 55			93.1 93.6 92.7 94.0 92.6	0.8 0.4 2.2 1.8 2.2	12.4 6.7 7.8 5.2 9.8	3.3 8.1 5.1 5.2 3.5	.905 .923 .913 .905
55 56 57 58 59	56 57 58 59			90.7 90.3 89.8 89.3 79.1	2.2 2.4 2.6 1.2 2.6	15.4 16.6 18.0 22.4 44.6	2.9 2.6 2.0 2.4 3.7	.913 .900 .902 .912 .903
60 61 62 63 64	61 62 63 64 65			89.8 91.9 92.9 93.1 95.5	1.4 0.9 0.4 1.2 1.2	19.4 17.0 9.3 8.2 6.7	3.5 1.9 7.5 5.9 1.8	.906 .913 .929 .937 .917
65 66 67 68 69	66 67 68 69 70			96.4 89.0 96.2 93.3 93.7	1.1 5.7 0.8 1.4 1.3	3.9 10.6 5.9 11.9 6.7	2.2 3.0 1.8 1.8 5.9	.920 * .919 .907 .916 .925
70 71 72 73 74	71 72 73 74 75			94.6 95.4 94.7 93.0 92.3	2.1 1.4 1.9 2.1 1.9	4.8 6.6 6.2 11.5 13.3	3.6 1.7 2.3 1.2 1.8	.920 * .910 .927 .912 .916
75 76 77 78 79	76 77 78 79 80			92.7 90.1 89.8 92.2 91.6	1.9 2.2 2.2 2.0 2.1	12.5 18.2 19.1 13.5 14.6	1.7 1.8 1.8 1.7	.908 .915 .908 .902
80 81 82 83 84	81 82 83 84 85			91.9 91.5 88.8 94.8 95.3	2.3 2.2 2.8 1.7 1.5	13.3 14.7 20.0 6.8 6.0	1.6 1.8 1.8 2.3 2.2	.907 .903 .911 .924 .935

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Oll-SHALF ASSAYS BY MODITIED FISCHER RETORT METHOD Bemples from the U.S. Geological Survey's Corehole 78-12 (Continued)

		-	1	Yield	of procu				
			Weight	percent		er ton	Specific gravity		
From	To	0:1	Water	Spen: shale		013	Water.	of oil at	
85 86 87 88 89	86 87 89 89 90			96.4 96.4 97.1 96.7 97.7		7.2 6.6 4.3 3.1 1.1	2.3 2.1 2.4 2.7 3.8	.922 .917 .920 * .920 *	
90 91 92 93 94	91 92 93 94 95			98.3 97.8 99.2 98.8 98.4	0.1 0.4 Ø.1 Ø.1	0.0 0.0 N.D. N.D.	4.3 4.3 1.9 3.2 3.5	.920 * .920 *	
95 96 97 98 99	96 97 98 99			97.6 97.4 97.8 97.9 97.5	0.7 0.6 0.7 0.7	0.0 0.0 N.D. 0.0 N.D.	4.0 5.0 3.4 3.5 4.2	.920 * .920 * .920 *	
100 101 102 103- 104-	101 102 103 104 105			96.8 98.3 96.0 93.9 95.7	0.9 0.3 1.1 1.7 1.2	0.0 1.3 4.1 8.9 5.3	5.5 2.2 3.4 2.4 2.5	.920 * .920 * .920 * .915 .920 *	
105 106 107- 108 109	106 107 108 109 110			95.1 97.4 96.3 97.2 96.6	0.9 0.8 1.4 1.1	6.8 2.8 4.3 2.1 4.7	3.4 1.8 1.6 2.2 1.2	.920 * .920 * .920 * .920 * .920 *	
110- 111 112 113- 114	111 112 113 114 115			95.5 94.1 94.5 98.0 99.1	1.6 1.3 0.7 0.1	5.5 7.0 4.4 0.0 0.0	1.8 4.8 7.3 4.7 1.8	.908 .904 .920 * .920 *	
115 116 117 118 119	116 117 118 119 120			96.2 96.7 92.4 93.0 96.6	0.3 0.5 1.5 1.7 0.8	2.6 6.2 12.2 11.3 3.3	5.8 1.1 3.5 2.6 3.3	.920 * .902 .903 .903 .920 *	

Senter from the C.S. Sentegral Survey's Cornect-

OIL-SHALF ASSAYS BY MODITIED FISCHER RETORT MITHOD Samples from the U.S. Geological Survey's Corehole 78-12 (Continued)

				Yzeld	of proc			
D			Weight	percent	or bros			Specific
Prom	To	011	Water	Spent shale	Gas + loss	Oil	Water.	gravity of oil at
120 121 122 123 124	121 122 123 124 125			95.0 95.7 95.9 98.8 98.2	1.2 1.1 0.8 0.7 1.1	8.0 5.4 4.4 0.0 0.0	1.9 2.5 3.8 1.3 1.6	.920 .920 * .920 * .920 * .920 *
125 126 127 128	126 127 128 129	4		98.3 97.9 95.2 92.5	0.8 0.8 1.4 1.4	0.0 0.0 5.0 10.7	2.1 3.0 3.5 4.9	.920 * .920 * .920 *
129 130 131 132 133	130 131 132 133 134			97.6 97.1 96.2 96.4 99.1	0.9 0.6 0.8 0.9	1.8 N.D. N.D.	1.9 5.3 7.1 6.5 5.0	.920 *
134 135 136 137 138	135 136 137 138 139			98.7 98.3 98.0 97.7 97.0	9.1 9.1 9.1 9.1	0.0 0.0 0.0 0.0	5.7 6.5 6.9 7.2 6.7	.920 * .920 * .920 * .920 *
139 140- 141- 142 143	140 141 142 143 144			97.4 95.9 95.0 95.2 97.8	0.1 0.2 0.7 0.4 0.6	2.3 0.0 0.0 0.0	5.0 8.8 10.3 10.5 2.5	.920 * .920 * .920 * .920 *
144 145 146 147 148	145 146 147 148 149			91.3 95.1 91.1 90.2 98.2	1.9 1.4 1.7 2.0 0.7	15.7 6.5 12.6 14.1 N.D.	1.9 2.4 5.8 6.1 2.5	.916 .913 .907 .898
149 150 151 152 153	150 151 152 153 154			98.1 97.4 97.8 97.4 94.1	1.0 1.6 1.5 0.9 1.4	N.D. 0.0 0.0 1.6 7.5	2.2 2.2 1.8 2.4 4.0	•920 * •920 * •920 * •915

Senter from the U.S. Geological Survey a Consult

25 126

OIL-SHALE ASSAYS BY MODITIED FISCHER RETORT MITHOD

Samples from the U.S. Geological Survey's Corehole 78-12 (Continued)

		-		Yield	of proc	uc:		
Des	oth	-	Weight	percent			er ton	Specific
From	To	011	Water	Spent	Gas + loss	013	Water.	gravity of oil at 60°/60° F
154 155 156 157 158	155 156 157 158 159			94.6 96.8 99.1 99.0 97.2	1.3 0.6 0.4 \$\text{\$\text{\$\text{\$0.1}}}\$	5.5 4.0 N.D. 0.0	4.8 2.5 1.2 2.7 4.3	.920 * .920 * .920 *
159 160 161 162 163	160 161 162 163 164			96.4 95.7 95.8 94.6 95.1	0.5	2.7 4.5 3.0 2.7	5.0 4.7 6.4 8.5 9.5	•920 * •920 * •920 * •920 *
164 165 166 167 168	165 166 167 168 169			95.2 95.2 98.3 94.2 93.7	0.4	3.3 6.3 1.1 9.5 9.6	7.7 4.8 1.9 2.8 4.3	•920 * •920 * •920 * •916 •896
169 170 205 206 207	170 171 206 207 208			98.7 97.6 90.0 93.0 92.7	♥.1 0.3 1.7 1.1 1.2	0.0 0.0 17.5 11.4 5.7	3.4 5.1 4.0 3.7 9.3	.920 * .920 * .903 .915
208 209 210 211 212	209 210 211 212 213			91.0 91.5 89.1 96.2 98.3	1.3 1.3 2.2 0.6 0.1	14.9 10.8 17.7 5.6 1.4	4.8 7.6 4.5 2.4 2.3	.912 .911 .919 .920 *
213 214 215 216 217	214 215 216 217 218			97.1 96.7 96.5 98.0 97.8	0.6 0.7 0.6 0.6	3.3 4.7 4.9 1.7 2.7	2.5 1.9 2.6 1.7	.920 * .920 * .920 * .920 *
218 219 220 221 222	219 220 221 222 223			97.3 97.3 98.7 99.2 98.7	0.9 0.4 0.5 0.1	2.9 4.0 0.0 0.0	1.6 1.7 2.0 1.6 1.7	.920 * .920 * .920 * .920 *
250							1.6	-958

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bouples from the F.D. Geological Survey's Coroleste

OIL-SHALE ASSAYS BY MODIFIED FISCHER RETORT MITHOD Samples from the U.S. Geological Survey's Corehole 78-12(Continued)

				Yzeld	of prod	1101		
Dec			Weight	percent			per ton	Specific
From	To To	043		Spent	Gas +		per ton	gravity
	41.	011	Water	shale	loss	Oil	Water	of oil a: 60°/60°
								71117
					1-9			
223	224			97.3	1.0	3.2	1.2	•920 +
224	225			97.8	0.7	1.2	2.6	.920 +
225 226	226			97.4	1.1	2.6	1.2	·920 +
227	227 228			97.4	1.2	1.6	1.9	.920 +
	220			98.2	1.0	0.0	2.0	·920 +
228	229	ar .		99.9	-	37 70	0.7	
229	230			98.2	0.1	N.D. 2.0	0.7	000
230	231			98.8	0.5	1.6	1.1	•920 ÷
231	232			98.6	0.2	1.6	1.2	.920 +
232	233			99.4	<0.1	N.D.	1.3	-
233	234			07.1	. 167			
234	235			97.4	1.1	2.3	1.4	•920 *
235	236			97.4	1.1	4.4	1.9	•920 *
236	237	,		98.0	0.8	1.2	1.9	.920 *
237	238			98.0	1.0	1.1	1.6	.920 *
238	239			07 4		2 1	4.0	000 "
239	240			97.1	1.1	3.4	1.2	•920 *
240	241			99.8	0.1	N.D.	0.2	.920 *
241	242			99.8	0.1	N.D.	0.4	
242	243			99.7	€0.1	N.D.	0.8	
243	2114			98.9		4.4	4.1	000 ×
244	245			97.6	0.1	1.1	1.4	•920 * •920 *
245	246			97.3	0.4	0.0	4.9	.920 *
246 247	247			98.2	0.2	1.6	2.3	.920 *
-41	248			94.8	1.2	6.8	3.6	.896
248	249			95.8	1.1	4.9	2.7	•920 *
249-	250			91.4	1.7	13.8	4.1	. 896
250	251			89.2	2.5	17.9	3.7	.915
251 . 252	252			95.0	1.8	5.7	2.4	.909
-72	253			95.0	1.4	7-4	2.1	.906
253	254			95.4	1.3	6.8	1.7	•912
254	255			97.7	0.7	2.8	1.2	.920 *
255 256	256			95.5	1.0	4.9	3.7	•939
257	257 258			94.2	1.2	10.4	1.8	.908
-)	250			93.6	1.2	11.5	2.1	•908

THE PARTY PROPERTY AND UPON THE STATES LINES-110.

SAMPLE TWO RIS DIN THE PARTY OF PARTY O

				200

OLL-SHALE ASSAYS BY MODILIED FISCHER RETORT MITHOD

Samples from the U.S. Geological Survey's Corehole 78-12 (Continued)

		_		Yield	of produ	r4		
Da	pth		Weignit	percent	o. produ	THE RESERVE AND ADDRESS OF THE PERSON NAMED IN	er ton	Specific
From	То	Oi	1 Water	Spent shale	Gas +			gravity of oil at
			, water	andre	loss	Oil	Water.	60°/60° F
258 259 260 261 262	259 260 261 262 263			94.1 94.1 93.1 98.9 96.6	1.0 0.9 1.4 0.2 0.7	10.0 5.6 7.9 0.0 4.9	2.7 7.0 6.0 2.1 1.9	.901 .915 .900 .920 *
263 264 265 266 267	264 265 266 267 268			98.9 96.2 93.9 93.6 91.8	0.8 1.1 1.3 1.0 1.7	0.0 5.5 7.3 7.3 10.5	0.7 1.3 4.8 6.1 5.7	.920 * .925 .920 * .920 * .927
268 269 270 271 272	269 270 271 272 273			87.6 91.4 93.4 93.1 96.4	2.7 1.8 1.3 1.2 2.0	19.4 12.8 8.6 9.3 2.7	5.8 4.9 4.7 5.1 1.2	.906 .894 .920 * .920 *
273 274 275 276 277 278 279 280 281 282 283	274 275 276 277 278 279 280 281 282 283 284	· .		98.6 82.6 81.3 95.5 91.9 95.8 93.0 94.1 97.1 91.4	0.5 3.7 4.6 1.9 1.8 2.2 1.8 1.3 2.3	1.1 30.8 30.0 3.6 9.7 3.1 10.3 9.0 2.5 15.4 13.1	1.2 5.1 6.6 2.9 5.9 2.9 2.2 1.8 1.4	.920 * .905 .904 .920 * .920 * .920 * .898 .887 .920 * .894
284 285 286 287 288	285 286 287 288 289			98.0 97.0 93.3 93.2 95.1	0.5 0.6 0.8 0.7	1.9 4.5 12.5 8.0 5.3	1.7 1.6 2.8 7.4 6.2	.920 * .920 * .914 .907 .920 *
289 290 291 292 293	290 291 292 293 294			98.1 97.1 96.8 95.3 94.4	0.1 0.1 0.5 1.0	0.0 2.6 2.4 4.4 5.6	4.3 4.9 5.8	.920 * .920 * .920 * .920 *

THE PERSON NAMED IN COLUMN TO PERSON ASSESSMENT OF

Respire from the U.S. Testinging Survey's Engines

				996 .	

OIL-SHALE ASSAYS BY MODILIED FISCHER RETORT MITHOD Samples from the U.S. Geological Survey's Corehole 78-12 (Continued)

			,	Yield c	i procu	~ 1		
			Weight	percont		er tor	Specific	
From				Spent	Gas +	<u>ou.</u> p	c. Lur	pravity of oil at
1 1011	То	011	Water	shale	loss	013	Water	60°/60° ±
294 295 296 297 298	295 296 297 298 299			94.8 93.0 93.0 93.0 95.4	0.4 1.3 1.2 1.1 0.4	5.4 6.4 5.6 4.7 4.0	6.4 7.6 8.7 9.9 6.4	.920 * .920 * .920 * .920 *
299 300 301 302 303	300 301 302 303 304			93.8 94.0 85.2 95.2 86.3	0.5 1.4 2.0 1.2 3.7	3.1 10.1 27.7 7.2 20.9	10.8 1.9 5.4 2.2 5.3	.920 * .911 .910 .907 .901
304 305 306 307 308	305 306 307 308 309			90.1 92.9 96.2 97.2 95.0	3.0 2.8 1.9 0.3	9.3 5.9 2.4 3.6 7.1	8.3 5.0 2.3 2.8	.899 .904 .920 * .920 *
309 310 311 312 313	310 311 312 313 314			98.0 99.7 98.9 97.8 94.5	Q.1 Q.1 0.3 0.6 1.6	2.4 0.0 0.0 2.7 7.4	2.8 1.5 0.9 1.4 2.6	.920 * .920 * .920 * .920 * .920 *
314 315 316 317 318	315 316 317 318 319			95.6 96.7 97.8 98.0 96.3	1.3 0.4 0.6 0.8 1.1	7.0 5.1 2.0 1.5 4.9	1.2 2.2 1.9 1.5	.902 .921 .920 * .920 *
319 320 321 322 323	320 321 322 323 324			95.2 94.1 94.5 96.4 96.4	1.3 1.3 1.3 1.2 0.2	7.5 9.7 8.8 3.7 5.7	1.8 2.1 2.1 2.4 2.7	.904 .911 .913 .920 *
324 325 326 327 328 329	325 326 327 328 329 330			98.1 95.9 98.7 99.2 93.8 96.4	9.1 9.1 9.1 9.1 9.1	5.3 4.8 2.6 14.9 7.4	3.8 8.5 2.0 1.6 2.7 4.8	.920 * .920 * .920 * .920 * .920 * .908

^{*} Assumed specific gravity.

THE PARTY STATES AND SHOOK THE REALISM COMMENTED

Assertes from the E.S. Carrestest Survey's Covennie

			are .		

Assumed opening gravity.

